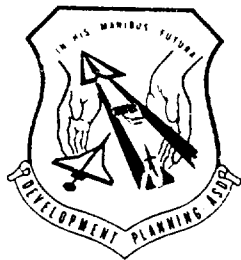


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ASDIR-II
VOLUME II
PROGRAM DESCRIPTION

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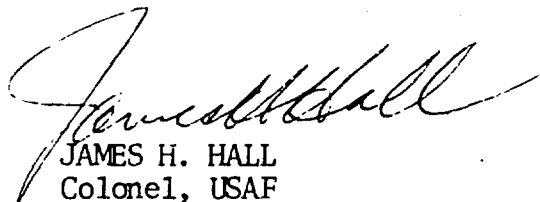
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ASDIR-II PROGRAM DESCRIPTION

INTRODUCTION

This Program Description outlines the structure of ASDIR-II in order to give the users the essential knowledge required for program implementation, use and modification. Simplified structural and flow diagrams of the major programs and short functional descriptions of all programs and subroutines are given to help describe ASDIR. The level of detail presented in this manual is consistent with the availability of reference and documentation material, program difficulty or program impact on overall computational accuracy.

Essentially this manual is written in the same order as the calling sequences in ASDIR, with modification only when structural considerations and clarity dictate.

Please note, this manual is intended as an aid to the user to allow better understanding of each program's function and not as a users manual (see ASDIR-II, Volume I - USERS MANUAL).

GENERAL PROGRAM DESCRIPTION

The Aeronautical Systems Division's InfraRed Signature Prediction Model (ASDIR) is a computer code utilizing the overlay structure shown in figure 1. These overlays are organized into three major functionally modularized computational groupings, figure 2: (1) Hot Parts Analysis; (2) Plume Gas Dynamics; and (3) Signature Prediction. A fourth overlay element establishes the required data initialization and input/output operational capabilities.

This volume is organized in the following functional format:

1. ASDIR 2 - Program Control
2. Data Initialization & I/O
3. Hot Parts Analysis
4. Plume Gas Dynamics
5. Signature Prediction
6. Program Listing in Overlay Form

PROGRAM: ASDIR 2 (Page A-4)

FUNCTION: This program is the main controlling routine of ASDIR (the Aeronautical Systems Division InfraRed Signature Prediction model). ASDIR's prime function is to provide a logical sequence of calls to the functional programs.

INPUT: None

OUTPUT: None

SUBROUTINES: All overlays and data blocks

DESCRIPTION: See figures 1 and 2 and program listing on page A-4.

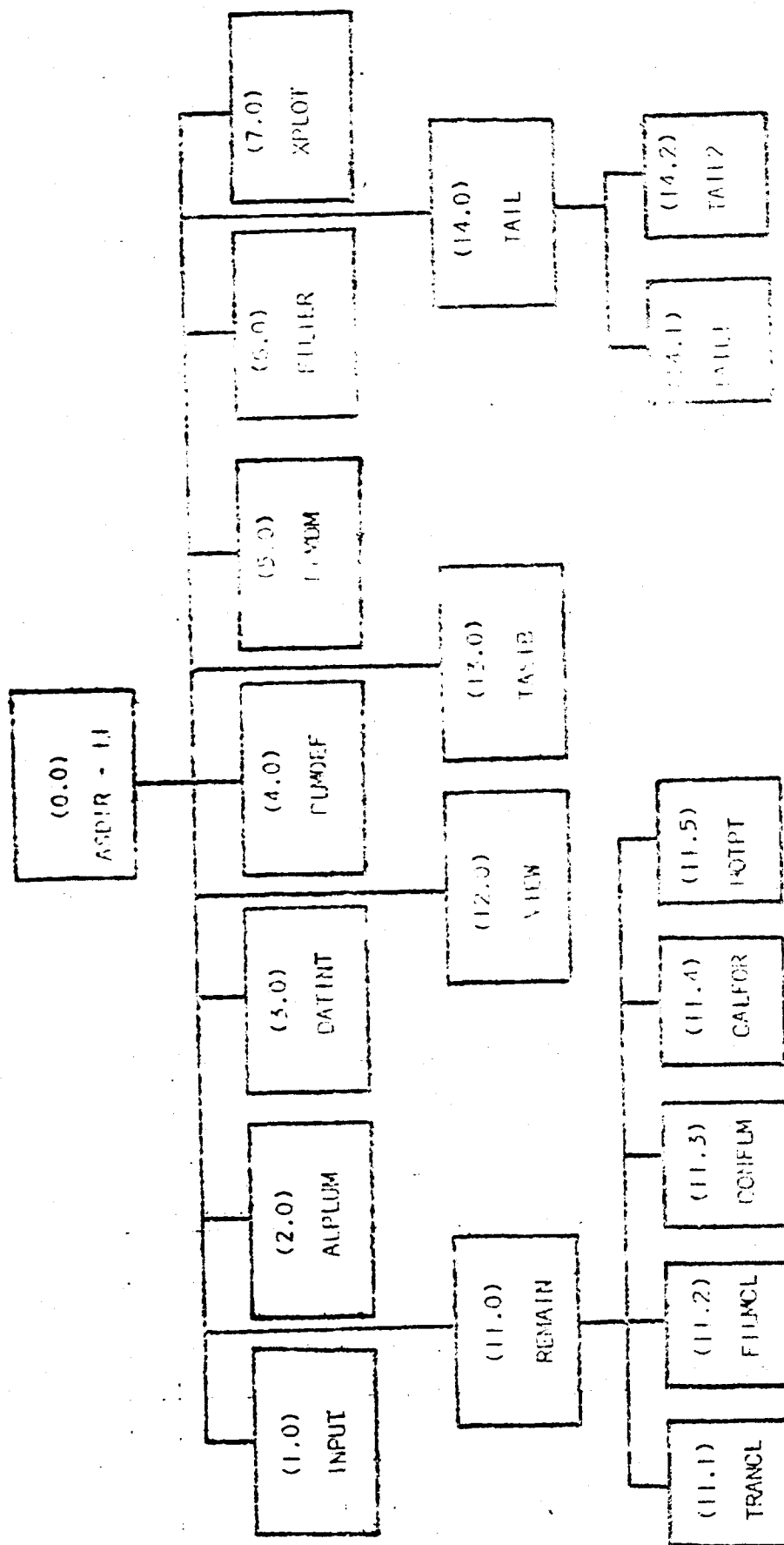


FIGURE 1. ASDIR-II OVERLAY STRUCTURE

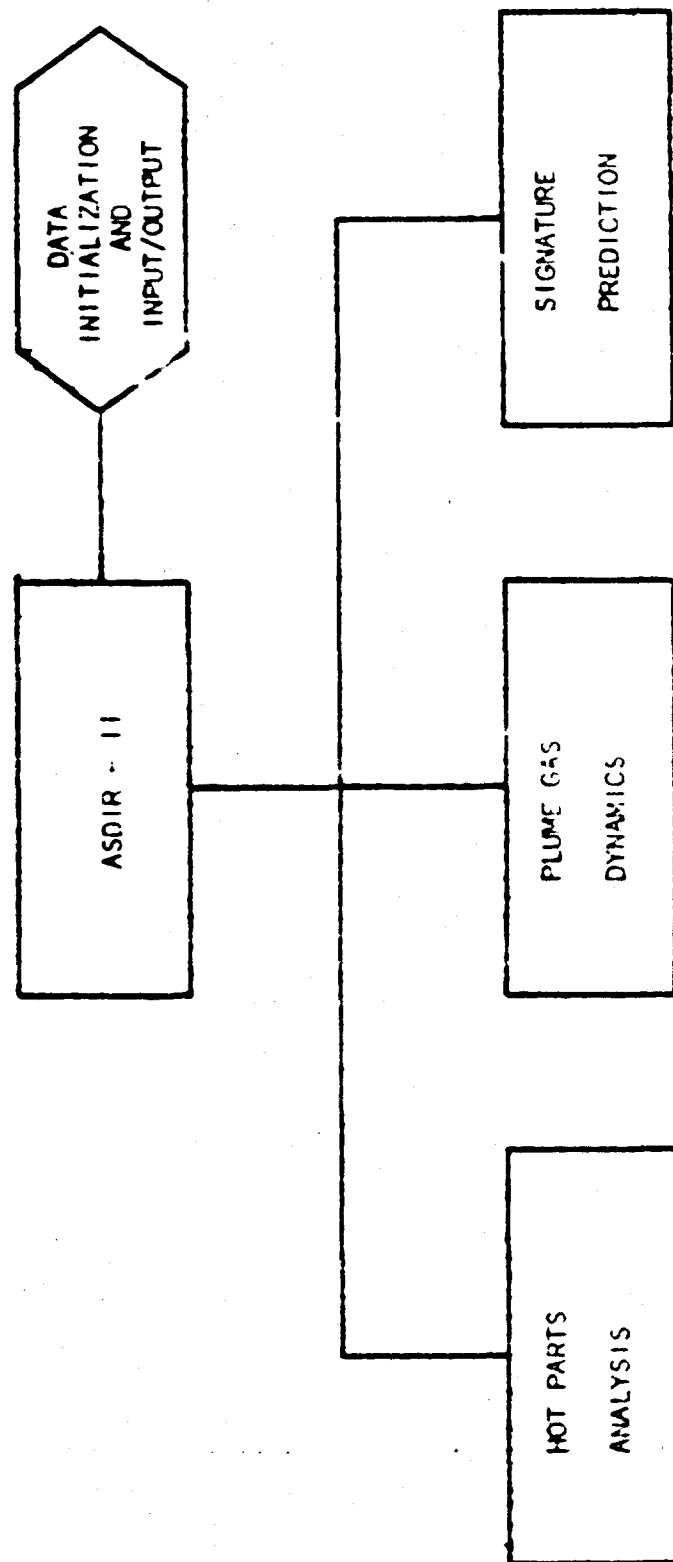


FIGURE 2. ASDIR-II FUNCTIONAL STRUCTURE

PROGRAM: INPUT (Page A-43)

FUNCTION: Provide a vehicle by which the desired calculation parameters, case definition and data initialization can be read into ASDIR.

INPUT: All control and computational variables in the CASE namelist.

OUTPUT: Computationally compatible case and dimensional data.

SUBROUTINES: None

DESCRIPTION: See ASDIR-II Volume I, User's Guide, for complete description of the namelist variables.

PROGRAM: DATINT (Page A-79)

FUNCTION: To initialize the calculation parameters.

INPUT: None

OUTPUT: Initialized calculation parameters

SUBROUTINES: None

DESCRIPTION: This program has been written to initialize the common block data to the default case. See ASDIR-II, Volume I, User's Guide for default options. A secondary function of this program is to allow use of ASDIR on systems in which a zero core initialization is not available.

PROGRAM: FILTER (Page A-106)

FUNCTION: Provides a means of accessing stored filter response data or entering a filter response of the user's choice.

INPUT: Filter number or filter band width and response.

OUTPUT: Filter response.

SUBROUTINES: None

DESCRIPTION: Stored filter responses are in data statements with modification possible through namelist FILT. This program also can be used to initialize the wavenumber calculation intervals.

PROGRAM: XPLOT (Page A-109)

FUNCTION: To provide a means of file manipulation for
either punching or printing spatial signature
data.

INPUT: Calculated spatial signature data.

OUTPUT: Punched or printed spatial data.

SUBROUTINES: None

DESCRIPTION: This program requires the use of a punch file
and an addition file TAPE 8.

PROGRAM: Block Data H2O (Page A-15)

FUNCTION: Data Block for water vapor band parameters.

INPUT: None

OUTPUT: None

SUBROUTINES: None

DESCRIPTION: See References [1, 2, 3]

PROGRAM: Block Data CO2 (Page A-7)

FUNCTION: Data Block for carbon dioxide band parameters.

INPUT: None

OUTPUT: None

SUBROUTINES: None

DESCRIPTION: See References [1, 2, 3]

PROGRAM: SIGNIR

FUNCTION: To calculate the hot parts signature and descriptive parameters required in ASDIR.

INPUT: Engine description, gas properties and case definition (See ASDIR-II, Volume I, User's Manual).

OUTPUT: Primarily the information which is transferred from the SIGNIR link to ASDIR is an equivalent black body area and equivalent black body temperature.

SUBROUTINES: See Figure 3.

DESCRIPTION: With the exception of the modifications required to adapt SIGNIR to the ASDIR format the hot parts calculations are performed with the original LTV/SIGNIR-I computer code. This code was chosen for only one reason; it has proven to be the best available methodology to predict engine hot metals signatures regardless of program size, operating cost or complexity.

The description of the infrared signature prediction program (SIGNIR) is provided by the following discussions which cover a general description of the program, the program computational procedure and the analytical methods utilized in obtaining the solution.

The program SIGNIR is a digital computer program written for the purpose of providing predictions of the hot metal infrared emission from aircraft engine exhaust systems. The program is designed to be applicable to axi-symmetric turbojet, turbofan, or turboshaft engine exhaust systems. It predicts the spectral intensity of the radiant energy emitted from exhaust system hot metal in the wavelength band of from one to 15 microns. In general, the information required by the program is as follows:

- . Exhaust system physical characteristics
- . Engine operating conditions
- . Special surface cooling flow conditions
- . Exhaust system surface properties

The predictions provided by the program for the combination of a selected maximum of 20 engine off-axis angles are:

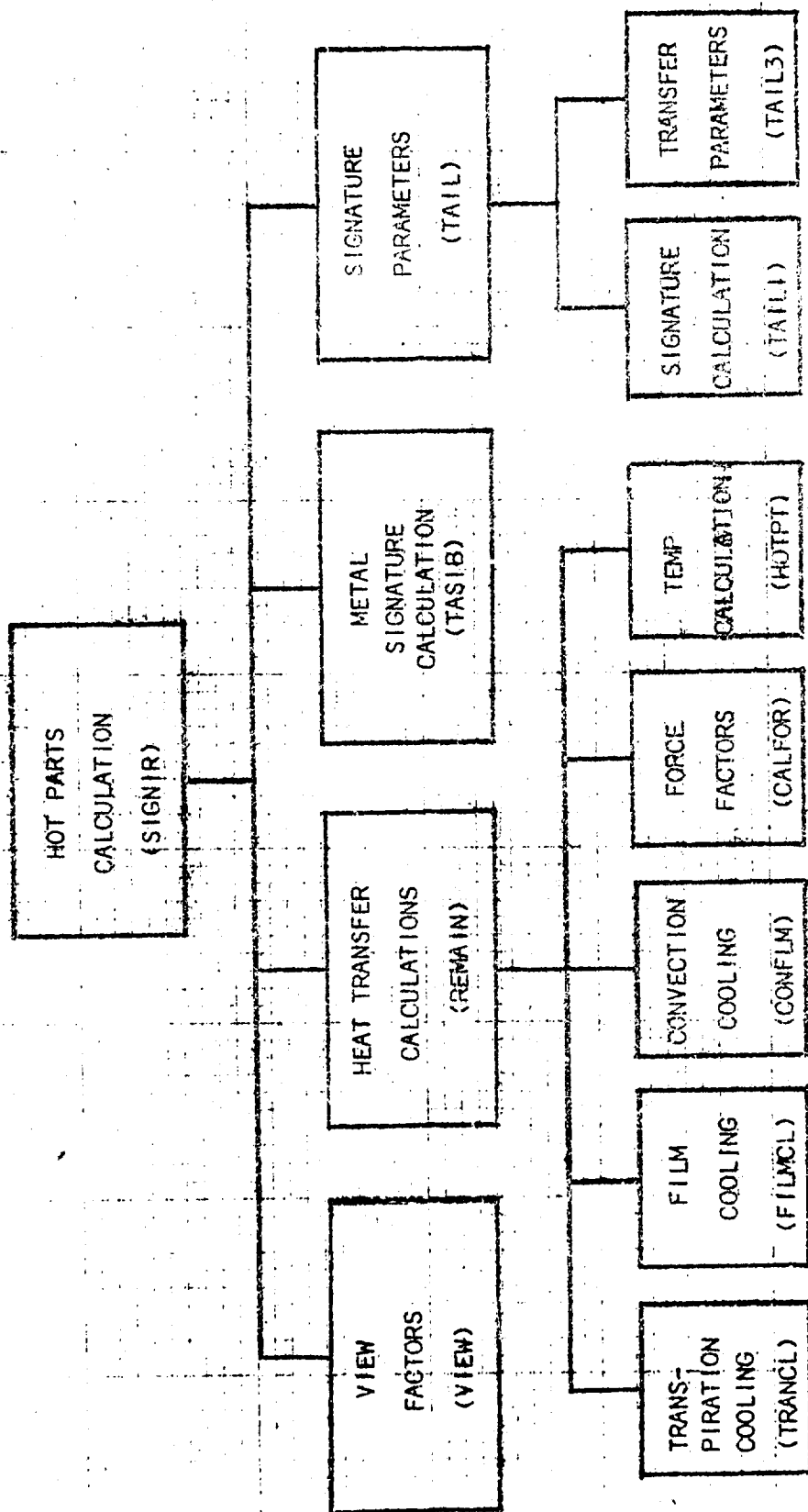


FIGURE 3. HOT PARTS ANALYSES

- . Spectral radiant intensity nonattenuated by the atmosphere
- . Selected radiant intensity bandwidth summations nonattenuated by the atmosphere

Optional exhaust system information which can be requested from the program is:

- . Internal fluid flow properties
- . Surface boundary layer data
- . Internal and external geometric radiation view factors
- . Surface temperature distribution
- . Thrust information

The process of computing the intensity of the infrared energy emitted from aircraft exhaust system hot metal requires a knowledge of the metallic surfaces temperature, emissive properties and their relative physical positioning within the system. From this information, the radiant energy emitted and reflected from the exhaust system to a point in space can be determined. The computational procedure established by this program for the prediction of exhaust system hot metal infrared radiation is shown by major subjects in the general block diagram presented on figure 3.

The input data required by the program provides a physical model (nodal system) of the exhaust system configuration, the properties and conditions of the exhaust gases entering the system, band width and location relative to the exhaust system. The program undertakes a one-dimensional, isentropic, compressible flow analysis which generates the axial distribution of exhaust gas flow conditions and properties within the system. Where two gas streams at different temperatures flow within a single passage, compound flow considerations are utilized. The program adjusts the flow at the nozzle throat to balance with the ambient pressure or a choked condition dependent on the system's entrance flow data.

With the internal flow properties defined, a surface boundary layer analysis is conducted to obtain the coefficients of convection and friction along each surface within the system. This analysis is primarily dependent on the surface's axial static pressure distribution and the upstream boundary layer conditions. An area weighted average coefficient of convection for each of the model's surface nodes (isothermal regions established by the input data) is computed for the system thermal analysis. The axial force on each surface, internal to the system, is computed utilizing both the frictional and pressure-area forces.

Descriptions of the routines associated with SIGNIR are presented in Table 1. Further definitions of the routines can be found in ASDIR-II, Volume III, Reference Documentation or in Reference [4].

The program SIGNIR, other than a few minor programming changes, remains as developed by LTV. The only link between SIGNIR and ASDIR-II is Common Block OUT, containing the following information:

- . Equivalent Black Body Area, CM^2
- . Equivalent Black Body Temperature, deg-K
- . Viewing Aspect Angles, degrees off tail
- . Number of Aspect Angles

TABLE 1
DESCRIPTION OF SIGNIP ROUTINES

<u>ROUTINE NAME</u>	<u>BASIC FUNCTION</u>	<u>PAGE</u>
ARCCOS	Determines the angle, in radians, corresponding to a given cosine value. The angle will be from zero to $\pi/2$ radians.	A-176
ARRAY	Describes in two-dimensional coordinates the inner and outer surfaces of the flow streams using the surface node coordinates.	A-38
AVFR	Averages the cooling wall temperatures for the surface nodes along the cooled portion of the configuration surfaces; prints these averages.	A-118
AVERFS	Determines the average values of the parameters necessary for force factor (pressure area and friction forces) calculations for each surface node along the configuration surfaces.	A-160
AVERHT	Determines and prints the average heat transfer coefficient for each surface node along the configuration surfaces.	A-151
AXAREA	Determines the cross-sectional area of the fluid flow streams as a function of the configuration axial distance.	A-126
BODY	Determines for the internal view factors, if the line of sight between points on two nodes is tangent to a shadowing body.	A-186
CALFOR	Prints the average force factor for each surface node and calculates and prints the total net surface force factor for the configuration.	A-148
CANSEE	Checks, for internal view factors, the visibility between two nodes to determine if shadowing may occur.	A-184
CEDIT	Selects the convection and conduction heat paths from input data and forms the conduction matrix.	A-203
CHECK	Checks the data returned from routine BODY for extraneous solutions.	A-188

TABLE 1 (Cont)

<u>ROUTINE NAME</u>	<u>BASIC FUNCTION</u>	<u>PAGE</u>
CODE	Analyzes the results provided by routine FINDIT to describe the nature of shadowing between two nodes.	A-183
COFLOW	Calculates the compressible flow properties for the flow streams as a function of pressure. Adjusts the flow for cooling or ambient pressure at the exit of the configuration.	A-122
COND	Reads in those values of heat transfer and fluid lump temperatures for nodes whose thermal paths are not connected with the fluid streams.	A-40
CONFLM	Calculates a pressure balance and surface temperatures for a surface cooled by convection-film cooling for either counter or parallel flow. Prints the coolant mass flow rate and pressure.	A-139
CPAGMA	Calculates the specific heat at constant pressure as a function of temperature for routine HEAT and the specific heat ratio as a function of Mach number of routines RIMAIN and HEAT.	A-128
CRODEL	Computes Kroneker Delta for matrix solutions.	A-196
CUBIC	Determines the real roots of a third order equation.	A-178
DINVRT	Computes the matrix inversion and accompanying solution for linear equations.	A-199
DIS	Computes the distance between two given coordinates.	A-215
FEDIT	Selects the radiation view factor data from the input data and forms the radiation matrix.	A-202
FILMCL	Calculates a pressure balance and surface temperatures for a film cooled surface. Prints the coolant mass flow rate and pressure.	A-134

TABLE I (Cont)

<u>ROUTINE NAME</u>	<u>BASIC FUNCTION</u>	<u>PAGE</u>
FINDIT	Locates the axial positions of two nodes with respect to the axial positions of the configurations surfaces.	A-182
FLOWNO	Checks the resulting pressure for surface cooling against the static pressure along the cooled surface. Prints a warning diagnostic for areas of no cooling flow.	A-119
GATHER	Combines data from routines AXAREA and COFLOW to form the compressible flow properties for the configuration flow streams.	A-127
HEAT	Calculates the initial conditions necessary for the boundary layer calculations.	A-153
HEATTR	Calculates the convection heat transfer coefficient.	A-159
HOTPT	Routine to control the calculation of surface boundary layers and heat transfer coefficients.	A-149
MATPOS	Checks to ensure that all the elements for convection and radiation matrices are positive.	A-197
MATSYM	Completes the matrices for the convection heat paths and the radiation view factor area product.	A-198
MINV	Inverts the "Script F" matrix.	A-222
ORDER	Arranges two-dimensional coordinate arrays into increasing order according to a selected variable.	A-39
PICMAX	Determines the maximum value of an array of up to twenty numbers.	A-190
PICMIN	Determines the minimum value of an array of up to twenty numbers.	A-191
PLANCK	PLANCK Black body function.	A-219
PLOT1	Generates a plot of radiant intensity vs. wavelength for both the non attenuated and the atmospheric attenuated radiation data.	A-206

TABLE 1 (Cont)

<u>ROUTINE NAME</u>	<u>BASIC FUNCTION</u>	<u>PAGE</u>
PRNDT1	Calculate the Prandtl number as a function of temperature for routine CONFLM.	A-147
PRNDTL	Calculates the Prandtl number as a function of temperature for routines TURBLT and RIMAIN.	A-129
PSOLN	Generates surface cooling flow supply and discharge characteristics and solves these simultaneously for calculation of the available surface cooling mass flow rate and pressure.	A-120
QUAD	Determines the roots of a second order equation.	A-177
REDI	Computes the spectral radiant intensity (watts/Steradian) for each engine off-axis angle.	A-220
REDII	Computes and prints geometric view factors for a detector to the configurations surface nodes as a function of engine off-axis angle.	A-210
REMAIN	Control routine for the fluid flow, heat transfer, surface cooling and surface force factor calculations. Prints the fluid flow information.	A-110
RING	Determines the intersection of a shadowing body with the "cone of vision" that a point on one node sees another node.	A-189
RITE	Used to print the heading information for routine REDII.	A-216
RITER1	Prints the surface radiation information.	A-224
SCRPTF	Computes internal radiation interchange factors for the thermal analyzer.	A-204
SETFLO	Determines the pressure balance for the surface cooling routines if a cooling mass flow rate is specified.	A-133, A-138
SHADOW	Describes the configuration surfaces used for shadowing in routine VIEW in a manner compatible for shadowing surface description of routine REDII.	A-209

TABLE 1 (Cont)

<u>ROUTINE NAME</u>	<u>BASIC FUNCTION</u>	<u>PAGE</u>
SIGNIR	The programs main routine. Controls the flow throughout the entire program.	A-32
STORE	Temporarily stores information necessary for average heat transfer coefficient calculations.	A-125
STORE1	Temporarily stores information necessary for force factor calculations.	A-124
STRATE	Computes solution utilizing linear interpolation routine used in describing the configuration surface data for boundary layer calculations.	A-121
SUMAT1	Summates and prints the radiant intensity for selected wavelength bands.	A-225
TABLEL	Computes solution utilizing second order interpolation of data and provides the first derivative of the interpolated function.	A-36
TAIL	Interface parameter generation and I/O program control routine.	A-205
TAIL1	Metal signature calculation control routing.	A-208
TAIL2	I/O and interface parameter calculation control routine.	A-218
TAS1R	Controls program flow and data involved in calculating the radiation interchange factor matrix, conduction matrix, performing the thermal balance and printing the wall temperature for each node.	A-193
TEST1	Tests the possibility of one node being shadowed by a second node which has the same axial location.	A-180
TEST2	Determines whether a point lies between two other points.	A-181
TESTN	Computes the last computed value of geometric view factor with the previously computed value to determine whether the view factor needs to be recalculated using finer divisions of the nodes. This routine also sets these divisions.	A-192

TABLE 1 (Cont)

<u>ROUTINE NAME</u>	<u>BASIC FUNCTION</u>	<u>PAGE</u>
TITLA	Controls output printing of the title page.	A-41
TRANCL	Calculates a pressure balance and wall temperatures for a transpiration cooled surface. Prints the coolant mass flow rate and pressure.	A-130
TURBLT	Calculates and prints the boundary layer and heat transfer information as a function of configuration axial distance.	A-154
VECANG	Calculates the angle of a node relative to the configuration center line.	A-217
VIEW	Calculates and prints for each configuration node, internal geometric view factors.	A-162
WRIT14	Transfers a two-dimensional array into a single dimensional array.	A-201

The equivalent Black Body Area and Temperature are extracted from the data generated by SIGNIR. The first step is to determine the equivalent Black Body Temperature. This is accomplished by searching the generated spectral data for the maximum intensity, figure 4, and applying the Wien Displacement Law:

$$T_{BB} = \frac{2897.9}{\lambda_{max}} \quad \text{K}$$

The equivalent Black Body Area is found by dividing the integrated signature obtained from SIGNIR by the Radiant Exitance over the band of interest.

$$A_{BB} = \int_{\lambda_1}^{\lambda_2} M_e(\text{SIGNIR}) / \int_{\lambda_1}^{\lambda_2} M_e(T_{BB})$$

Figure 5 shows a typical correlation between the predicted spectral signature and the spectral signature of the equivalent black body. These resultant temperatures and areas are the only parameters transferred back to ASDIR.

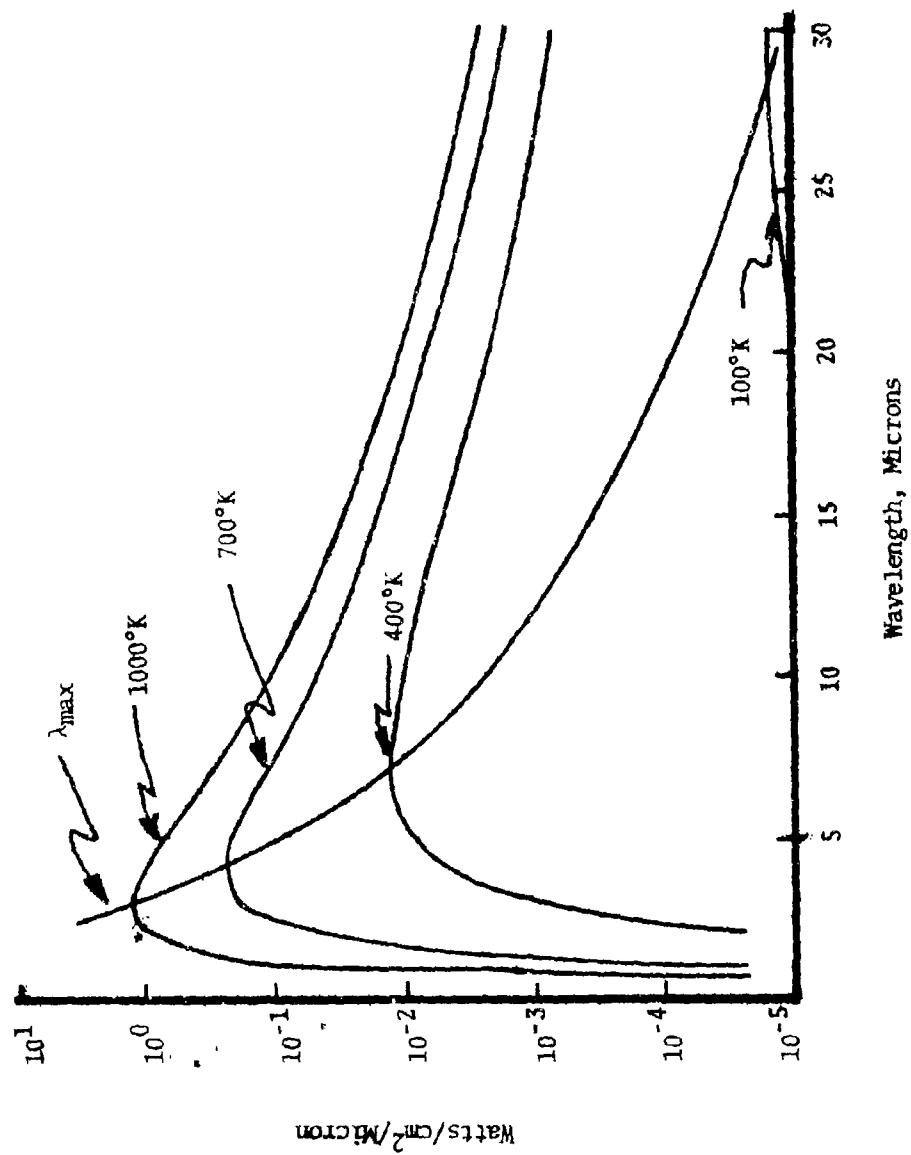


Figure 4. Black Body Curve

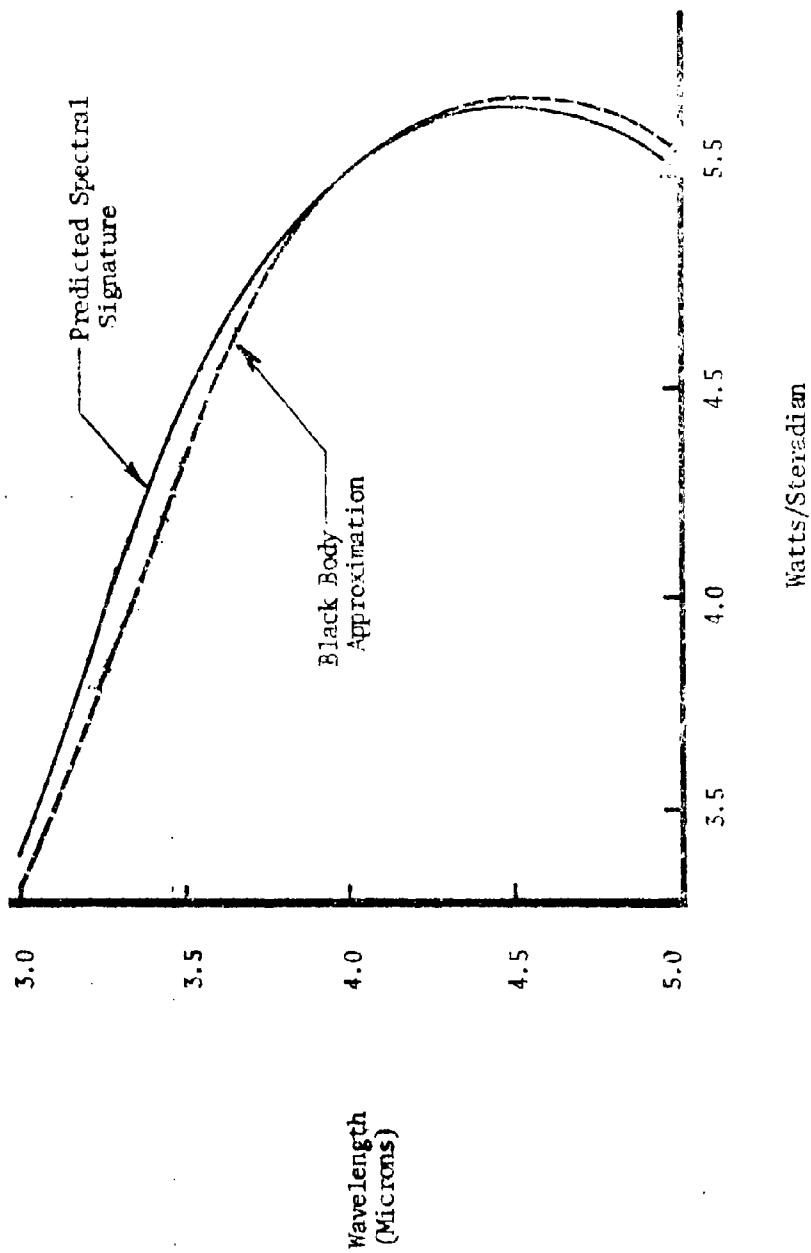


Figure 5. Black Body Correlation

PROGRAM: PLMDEF (Page A-81)

FUNCTION: Plume definition and gas data array development.

INPUT: Engine nozzle exit flow properties (velocity, pressure, temperature, and species [H2O, CO2] concentrations) as a function of radius.

OUTPUT: Plume gas data array. At this point, velocity (ft/sec) and pressure (atm x 10⁻³) are multiplexed into common registers.

SUBROUTINES: FLINP

DESCRIPTION: The gas dynamic calculations made for the plume in this program, figure 6, are applicable to axisymmetric turbojet and turbofan engine with mixed or separate co-annular co-planar exhaust jets. The finite difference calculations were developed to express the conservation (mass, momentum, energy, and species) laws for numerical integration by General Electric in their early SCORPIO work reported in reference [5]. Two effective kinematic viscosities were retained, one for physical mixing and the other for thermal mixing. The conservation laws were simplified for axisymmetric flow whereby all gradients in rotation about the centerline were not to zero, and all radial components of momentum were neglected as being small. Second axial derivatives and axial gradients divided by the radius were also neglected in momentum. Thermal radiative heat transfer and thermal generation were also neglected. In the derivation of the energy conservation and transfer functions the effects of the second viscosity, the square of axial gradients, dependence upon radial velocity, and gradients divided by the radius were minimized. The radial coordinate system was transformed into a stream function coordinate system after Von Mises. The transformation functions and the transformed conservation relations to which the finite difference procedure was applied are as follows:

Stream Function

$$\psi \frac{\partial \psi}{\partial r} = \rho u r \quad ; \quad \psi \frac{\partial \psi}{\partial x} = -\rho v r$$

$$\text{wherein: } \frac{\partial \psi}{\partial r} = -\frac{u}{r} \quad ; \quad \frac{\partial \psi}{\partial x} = \frac{v}{r}$$

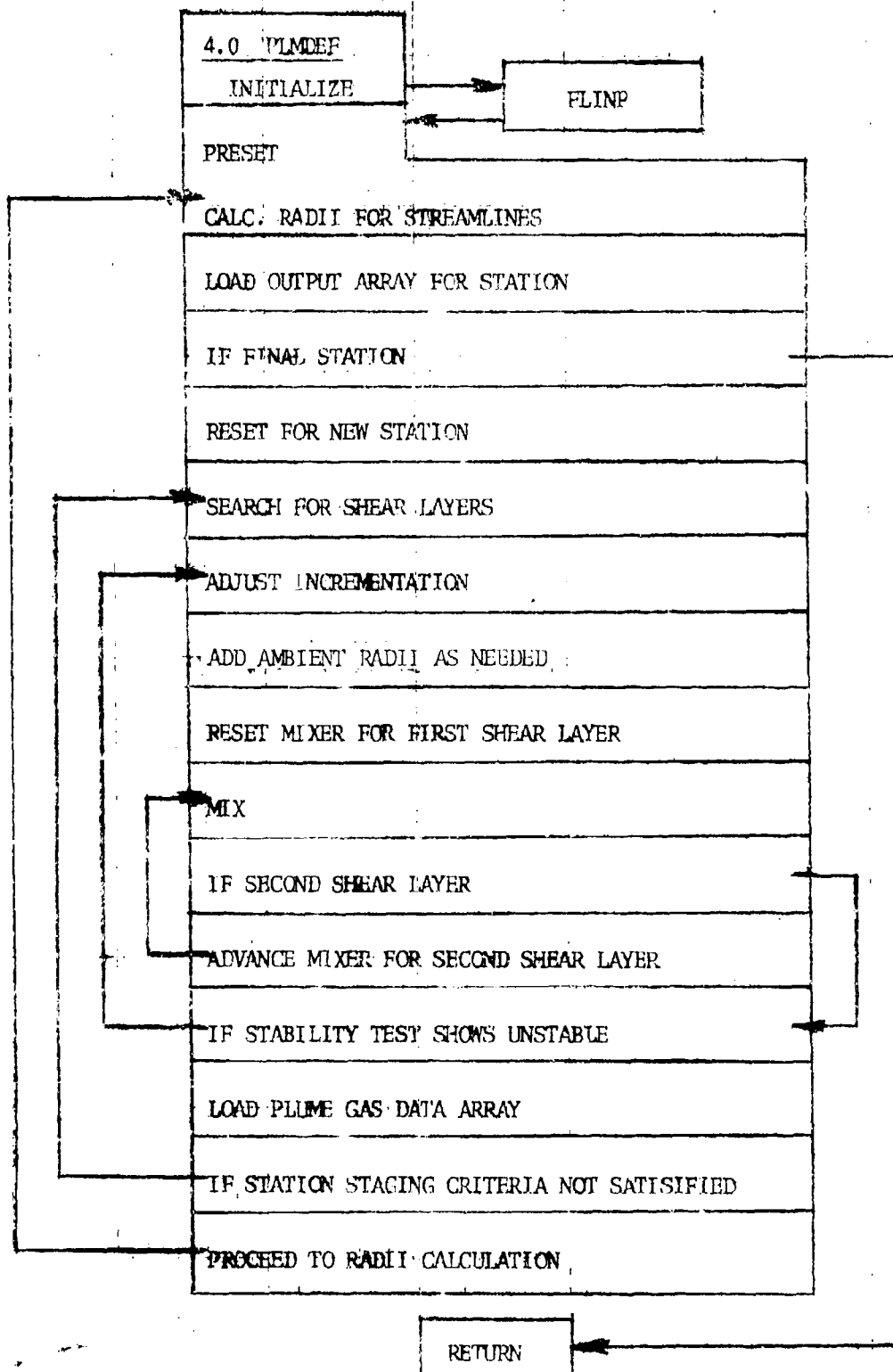


Figure 6. PLMDEF Flow Diagram

CONTINUITY:

for the stream function:

$$\Psi \frac{\partial^2 \Psi}{\partial x \partial r} + \frac{\partial \Psi}{\partial r} \frac{\partial \Psi}{\partial x} - \frac{\Psi \partial^2 \Psi}{\partial r \partial x} - \frac{\partial \Psi}{\partial x} \frac{\partial \Psi}{\partial r} = 0$$

and after the transformation:

$$-\frac{\partial}{\partial x} \left(\frac{\Psi}{\rho u r} \right) + \frac{\partial}{\partial \Psi} \left(\frac{\rho v r}{\rho u r} \right) = 0$$

MOMENTUM:

$$\frac{\partial u}{\partial x} = \frac{1}{\Psi} \frac{\partial}{\partial \Psi} \left(\frac{\rho^2 u r^2}{\Psi} \epsilon \frac{\partial u}{\partial \Psi} \right) - \frac{dp}{\rho u dx}$$

ENERGY:

$$\begin{aligned} \frac{\partial T}{\partial x} = & \left(\frac{\rho^2 u r^2}{\Psi} \epsilon_T \right) \left(\frac{1}{c_p \Psi} \right) \left(\frac{\partial u}{\partial \Psi} \right)^2 + \frac{\partial}{\partial \Psi} \left(\frac{\rho^2 u r^2}{\Psi} \epsilon_T \frac{\partial T}{\partial \Psi} \right) + \frac{dp}{\rho c_p dx} \\ & + \left(\frac{\rho^2 u r^2}{\Psi} \epsilon_T \right) \left(\frac{1}{c_p \Psi} \right) \frac{\partial T}{\partial \Psi} \left(c_{p1} \frac{\partial \alpha_1}{\partial \Psi} \right) \end{aligned}$$

DIFFUSION:

$$\frac{\partial \alpha_1}{\partial x} = \frac{\partial}{\partial \Psi} \left(\frac{\rho^2 u r^2}{\Psi} \epsilon \frac{\partial \alpha_1}{\partial \Psi} \right)$$

where:

T = gas static temperature or thermal subscript

u = gas axial velocity

v = gas radial velocity

Prandtl number = $c_p \rho \epsilon / k = 1$

Schmidt number = $\epsilon / D = 1$; in which D is the binary diffusion coefficient

ϵ = effective kinematic viscosity

α_1 = species concentration

$\frac{\partial c_p}{\partial r}$ is an assumed radial dependence for the gradient
of the specific heat of a mixture of gases = c_p/r .

Other quantities and terms are conventional.

The effective viscosity adopted for ASDIR includes the Donaldson and Gray treatment for the compressible free mixing of two dissimilar gases as reported in the AIAA journal, Vol 4, no. 11, in November 1966 and as applied by General Electric in SCORPIO-11 [5].

Overall, the plume model appears to reflect the essential features of measured plume data in those regions where the gas is hot. The regions where the model tends to lose accuracy are toward the outer edges where the gas shear appears to be too small thus allowing the plume to spread excessively. However, the plume temperatures and species concentration are essentially ambient in value so that the radiance and transmittance errors are small.

Viscosity Model

The choice of the turbulent viscosity, ϵ , is critical to the plume flow field. Past models, available in the literature (Schlichting, Abramovich, Warren and Applied Science Laboratories), show the turbulent viscosity as a function of axial distance and velocities in the mixing region. Preliminary results for the flow field showed that the analysis using these models did not agree with jet engine test data. A modified temperature dependent model for viscosity was formulated to include the temperature effects of hot flow.

The model being used in this analysis is:

$$\epsilon = x \cdot \{U_1 - U_2\} / [\text{CNST} \cdot (T_1/T_2)^2] \cdot \gamma$$

where

$$\gamma = 1 ; M_c < 0.6$$

$$\gamma = 1.6 / (1 + M_c) ; M_c > 0.6$$

The value for γ is from a paper by Donaldson and Gray. The value of CNST depends on the nozzle exit Mach number (M_c) and the centerline temperature. (See Page A-85).

Stability and Print Criteria

In order to insure stability, the axial step size, Δx , must be kept small. It was found that the system became unstable when the influence parameter

$$cz = \{\Delta x \cdot \epsilon \cdot u \cdot r^2 \cdot p^2\} / \{2 \cdot \psi^2 \cdot T^2 \cdot r^2\} \geq 0.20$$

To achieve a solution in a reasonable length of time, the step size Δx should be as large as possible. Accordingly, c_{zm} , the maximum value of c_z for each axial location is examined. If c_{zm} is too great, Δx is reduced for ensuing calculations. If c_{zm} is too small, Δx is increased for ensuing calculations.

Flow parameters are not entered into the data array at every value of Δx calculated. The calculation step sizes are too small. Tabulation occurs whenever the number of Δx increments from the previous calculation exceeds NBS or the sum of the Δx 's exceed Δx_p . Δx_p is incremented after each tabulation such that

$$\Delta x_{pN} = x_{p0} (0.5N)$$

Excessive static pressure at the nozzle exit plane is treated in a pseudo convergent-divergent nozzle manner which reduces the pressure to ambient value while accelerating and expanding the plume core to supersonic velocity over an axial distance of one nozzle diameter.

The program develops a plume gas data array containing the velocity, pressure, temperature, CO_2 concentration, H_2O concentration, and radius for up to 30 radii over an axial span of 49 stations. The velocity and pressure are multiplexed to share common registers. (See PLMDM for demultiplexing).

PROGRAM: FLINP (Page A-87)

FUNCTION: Provide a vehicle by which the required calculation parameters, nozzle exit flow quantities and data initialization can be read into ASDTR.

INPUT: All control and computational variables in the PLUMIN namelist.

OUTPUT: Computationally compatible engine nozzle exit plane flow quantity data. Nozzle and ambient data are printed.

SUBROUTINES: CHEM, THRUST

DESCRIPTION: The flow diagram of Program FLINP is shown in Figure 7. The function of this program is to initialize engine operational input and control quantities. The control function is derived from the input data. If the engine operational input quantities are not of the proper form, certain operations and additional reads are invoked to put the input into a form compatible with the PLMDEF program. Details can be found in ASDIR-II, Volume I, Users Manual.

In general, if PA is contained in namelist PLUMIN, the Mil Std 210 standard atmosphere in subroutine THRUST is bypassed. The inference is that an off-standard or test facility ambient condition is being simulated and the other ambient quantities are required in PLUMIN. Similarly, this program will bypass the default engine sample case if a nozzle exit velocity U8(1) is given greater than 1 ft per sec or if an ambient velocity UA is given greater than 11 ft per sec. Further, if U8(1) is greater than 1 the volume for T8T, P8, PQ, XCO2, XH2O will be accepted as given in PLUMIN. Again, if XCO2 has been omitted or given a small value (i.e. \leq XCO2A), the XCO2, XH2O, R, GAMMA, etc. will be calculated in CHEM for the fuel type (TANE) and stoichiometric equivalent ratio (EQR). Finally, if a gas quantity distribution for U8, T8T, XCO2, and XH2O is given in PLUMIN, they will be accepted unchanged since the load array key is taken from a test on U8(2).

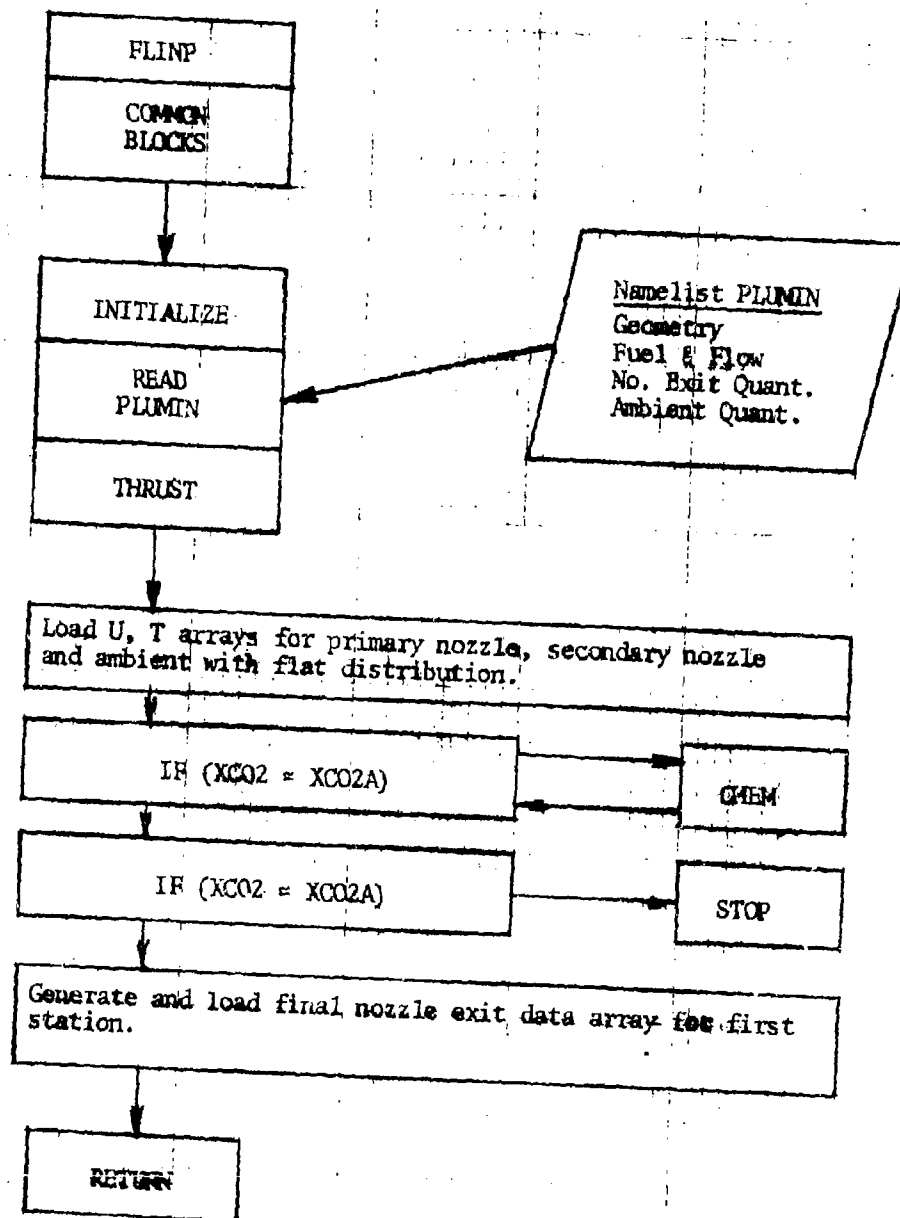


Figure 7. FLINP Flow Diagram

PROGRAM: CHEM (Page A-91)

FUNCTION: Generate the post combustion gas description (gas constant, specific heat and specific heat ratio, molecular weight, species conservation, etc) for a given fuel type, TANE, stoichiometric equivalence ratio, EQR.

INPUT: TANE, EQR

OUTPUT: Fuel to air ratio, gas constant, specific heat, gamma, CO₂ concentration, and H₂O concentration.

SUBROUTINES: None

DESCRIPTION: This program calculates the gas properties for the products of combustion with ideal combustion. Since combustion products properties vary only slightly with pressure and tend to chemically freeze near 2500°F in typical nozzle flow, the precision of this simple college chemistry approach is adequate and the fast calculation makes it a worthwhile approach.

PROGRAM: THRUST (Page A-93)

FUNCTION: Provide a vehicle by which the required calculation parameters and engine operating quantities can be read into ASDIR.

INPUT: All control and computational variables in the POWER namelist.

OUTPUT: Computationally compatible engine nozzle exit plane flow quantities not provided in FLINP input namelist PLUMIN. Flight condition data is printed.

SUBROUTINES: CHEM

DESCRIPTION: The flow diagram of subroutine THRUST is shown in figure 8. The function of this program is to read atmospheric, engine type, data type code, and engine specific performance data. The program control functions described for Program FLINP apply throughout this program.

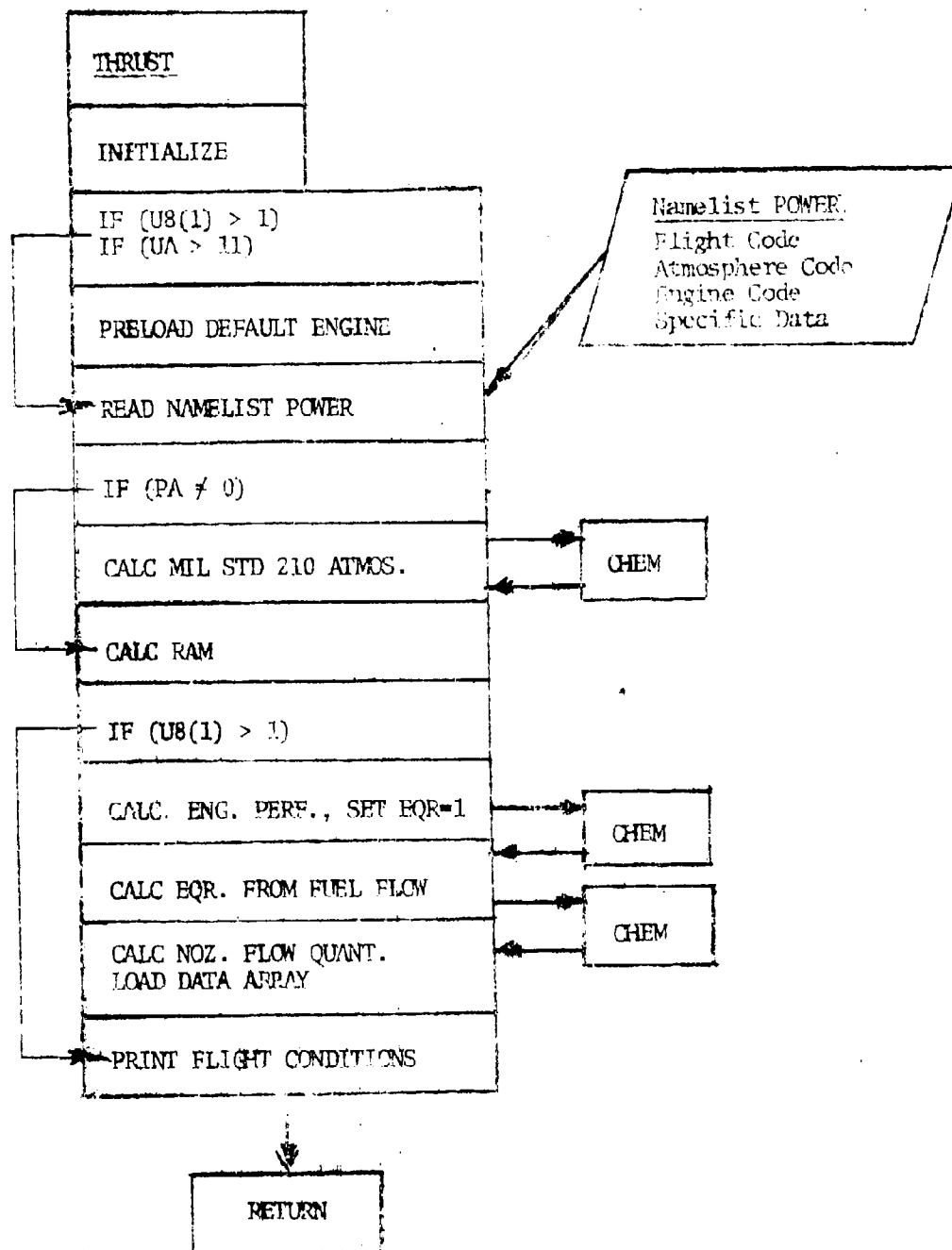


Figure 8. THRUST Flow Diagram

PROGRAM: PLMDM (Page A-98)

FUNCTION: To manage the plume gas data. An input control parameter, KDATA, controls the dispatch of the plume gas data.

INPUT: Plume gas data and the control code KDATA.

OUTPUT: Plume gas data output to cards, tape, printer, or printer plot in any combination.

SUBROUTINES: PLMPLT, PLMPRNT

DESCRIPTION: Each digit of the five digit integer KDATA controls an I/O function. KDATA is represented by the value:

KDATA = A B C D E

If A = 0, a new plume will be calculated. If A = 1*, an old plume previously filed will be brought in and plume calculations will be bypassed. If A > 1, plume gas data will be read from input cards.

If B = 1*, the plume gas data array is filed in the computer for later or repeated analysis. If B ≠ 1, the filing operation is bypassed.

If C = 1*, the plume gas data array is punched into output cards for later or repeated analysis. If C ≠ 1, the punch operation is bypassed.

If D = 1, the plume gas data array is printed in output by subroutine PLMPRNT. If D ≠ 1, the print operation is bypassed.

The subroutine PLMPLT is called with the final value E in the KDATA code. The E value has a different pattern than exhibited by A through D, see PLMPLT.

In addition to breaking down the code carried by KDATA, this program adds a layer of ambient data all around the plume data. The ambient data blanket is necessary to contain the interpolation exercises performed in the ray tracing calculations. The program then searches the plume gas data array to locate the tip of the core and

record such other parameters such as plume length AL, plume diameter REND, plume edge tangent TNB, etc. The minimum output RB, XC, REND, and AL is printed.

The PLMDM flow chart is shown in Figure 9.

*This code represents a machine dependent operation and may require further development for satisfactory operation.

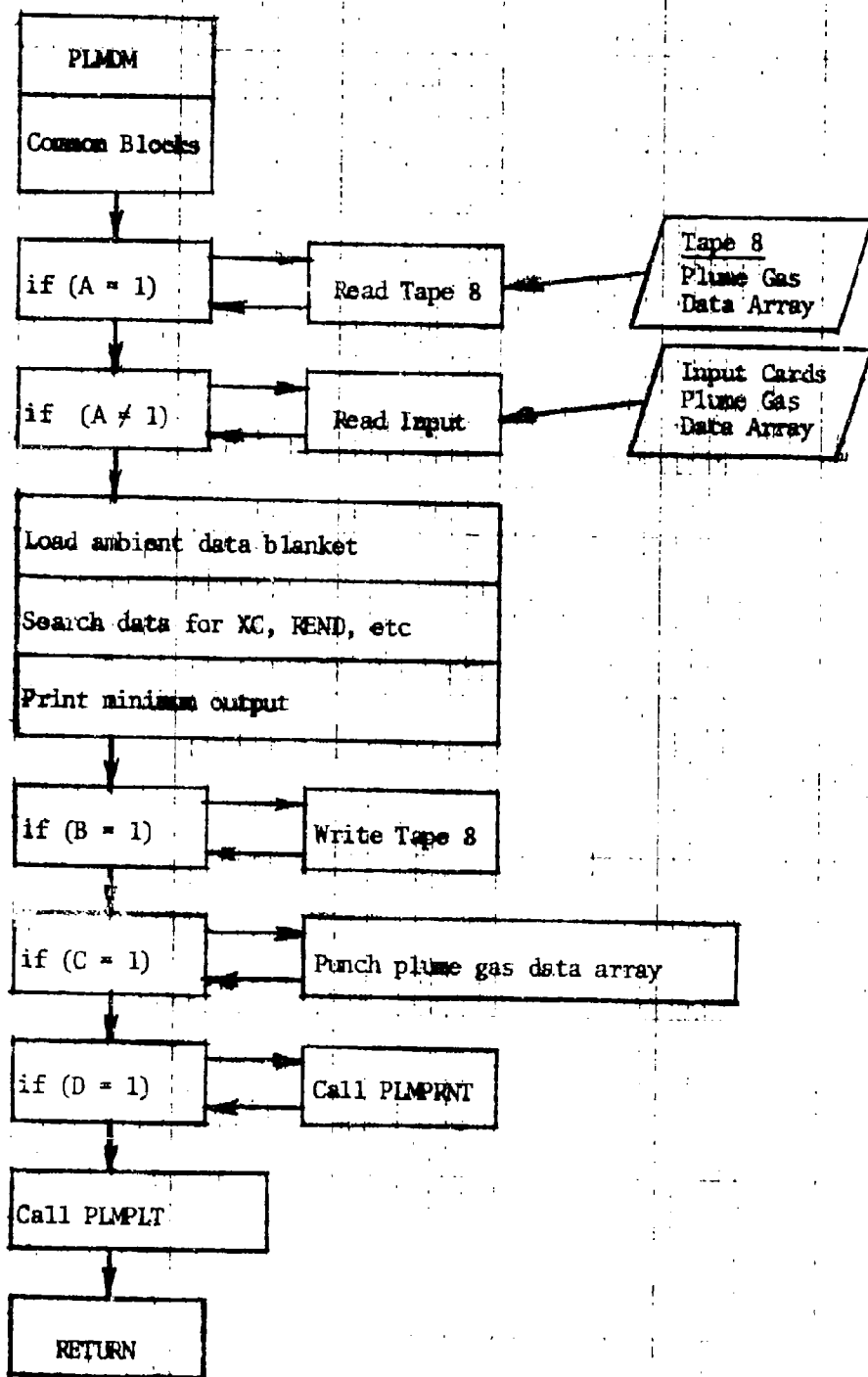


Figure 9. PLMDM Flow Diagram

PROGRAM: PLMPRNT (See Page A-100)

FUNCTION: Print the contents of the plume gas data array on the output printer.

INPUT: The plume gas data array

OUTPUT: The plume gas data

SUBROUTINE: None

DESCRIPTION: Print the plume gas data array. The plume gas data is printed in the following sequence:

- general caption
- plume station number and location
- centerline and edge Mach numbers
- radius, velocity, pressure, temperature, and CO2 and H2O concentration

Units are printed in the captions. The quantities printed are all self explanatory except the edge Mach number. The edge Mach number is that value at the outer edge of the innermost shear plane. This quantity will tend to oscillate due to the stepping and clipping process which occurs in the finite differencing procedure.

PROGRAM: PLMPLT (See Page A-101)

FUNCTION: Plot selected plume gas data quantities on the output printer.

INPUT: The plume gas data array and the final digit of the KDATA control code.

OUTPUT: Selected arguments of the plume gas data plotted on the output printer.

SUBROUTINES: None

DESCRIPTION: The output printer has 136 characters horizontally and more than 60 lines vertically. The grid represented by lines and characters are assigned one of the letters in the word plume (P L U M E) with the addition of # to permit the plotting of six ranges. A space is assigned the first character portion after a change in range. The nozzle exit plane value establishes the separator between # for values greater than the nozzle exit value and P for values between 80% and 100% of the nozzle exit value. Values in the 60% to 80% range are assigned L. Values between 40% and 60% are assigned U, etc. Each line represents a radius, and the interstation distance accumulates a number of characters. With two way interpolation a printer line is compiled and printed. After the data has been plotted, the axial scale is compiled and printed.

The code designating the plume gas data to be plotted is provided by the single digit value remaining in KDATA after having been stripped in program PLMDM. Up to four plots can be generated. In their plotting sequence, they are temperature, XO2 concentration, H2O concentration, and plume velocity. The appropriate captions are included. All four data arguments are plotted if the E value of KDATA is given as 0. If E = 1, no plots are printed. If E = 2, the last three are printed, if E = 3, the last two are printed, if E = 4, the last plot only is printed, and if E is greater than 4, the program will fail. For the general breakdown of KDATA, see program PLMDM.

The final activity accomplished in program PLMPLT is the de-multiplexing of the velocity and pressure. The pressure is brought up from the back of each velocity-pressure register and replaces the velocity. The velocity is no longer retained in the plume gas data array.

PROGRAM: ALPLUM (See Page A-47)

FUNCTION: Calculate total apparent spectral radiance of exhaust plume and hot engine parts as received by an observer with plume and atmospheric emissions and attenuation, including background contributions considered.

INPUT: Flight conditions, engine hot parts and plume parameters.

OUTPUT: Engine/Plume IR Signature

SUBROUTINES: RAYCAL, PLURAY, PLUSIG

DESCRIPTION: The flow diagram of program ALPLUM is shown in figure 10. The prime function of this routine is to be the controlling program to allow calculation of aircraft infrared signatures. Description of the working programs controlled by ALPLUM are contained under the individual program titles.

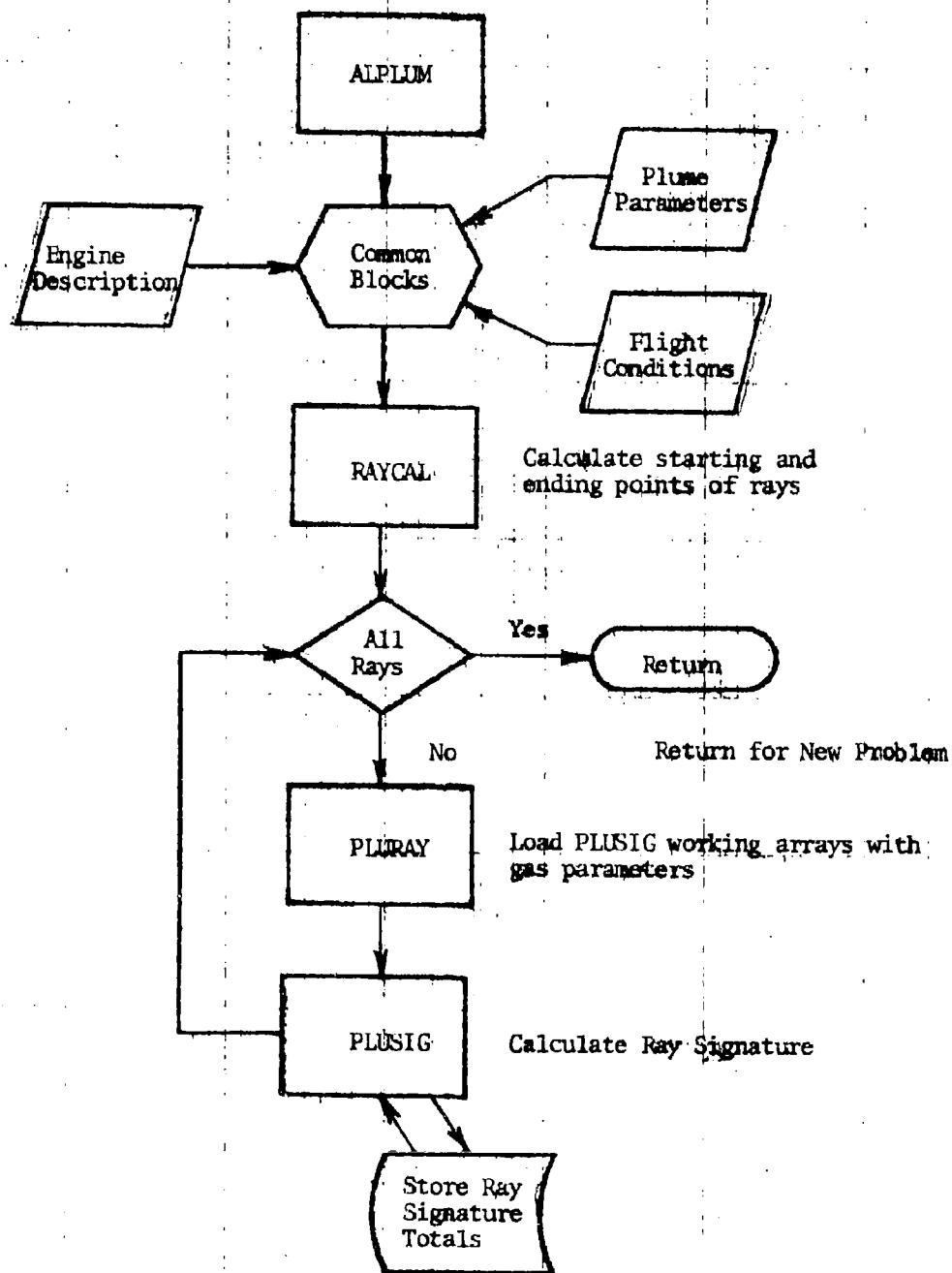


Figure 10. Total IR Signature Calculation.

PROGRAM: RAYCAL (Page A-50)

FUNCTION: To segment plume into discrete areas for signature analysis in other routines.

INPUT: Plume and engine geometry.

OUTPUT: Array of plume segment parameters.

SUBROUTINES: None

DESCRIPTION: RAYCAL, being basically geometric, is a relatively simple program. However, since signature prediction accuracy is dependent upon the geometric representation of the engine nozzle and the plume, graphical detail will be presented for this routine.

The engine nozzle and plume are characterized as a series of planar area segments each representing the termination of a ray or beam of radiated energy. Each segment represents either free (background) space or a black surface. The cross-sectional shape and area of each ray is defined by the segmentation scheme and is constant along the ray centerline. The segmentation scheme takes full advantage of symmetry as described with reference to the six accompanying figures.

Rectangular coordinates provide, figure 11, the framework for the ray definition. The X axis represents the engine nozzle centerline. The D axis, in the nozzle exit and perpendicular to the centerline X, is free to rotate about X so that the plane D-X will contain the centerline ray. The lateral axis, Z, is normal to both D and X. The angle of view, known as the aspect angle or ASPDEG, A8, is measured from the centerline X and lies in the D-X plane as shown in figure 12.

Dimensions on D represent the normal intercept of the ray centerline on plane D-Z from the Z axis.

Dimensions on Z represent the lateral intercept of the ray centerline on plane D-Z from the D axis.

Dimensions on X represent the axial intercept of the ray centerline on plane X-Z from the Z axis.

The simplified plume geometry adopted for use in this program is shown in figure 13. The plume is analyzed in three independent but adjoining regions:

(1) The plume core is segmented in the X-Z plane into a number of radial and angular segments shown in figure 14. Segmentation begins at the extremity of the nozzle exit projection on the X-Z plane and continues to the extremity of the core.

(2) The plume skirt is segmented in the X-Z plane into a number of radial and angular segments shown in figure 15. Segmentation begins at the extremity of the core and continues to the extremity of the plume.

(3) The engine nozzle is segmented in the D-Z plane into a number of radial and angular segments shown in figure 16.

Each planar segment so generated also defines a ray segment. The D-Z or D-X ray segment centerline intercept is centrally located, see asterisks, in each planar segment. Further, each segment is considered to be the ray segments own projection on the D-Z and D-X planes from which the ray segment cross section area, RAR, is calculated.

The ray segments are generated on the first call to RAYCAL. Successive calls simply transfer previously generated data.

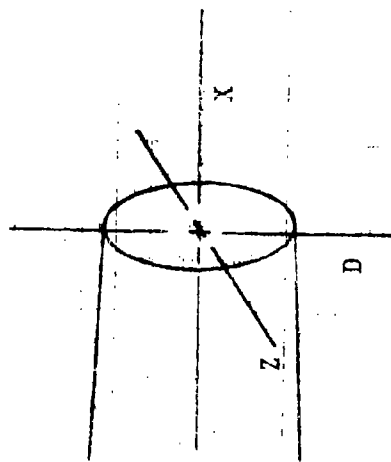


Figure 11. Ray Coordinate System

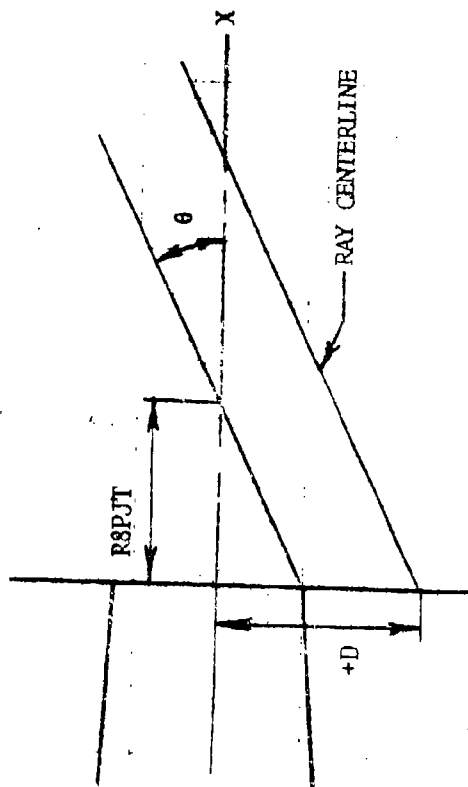


Figure 12. (D, X) Plane

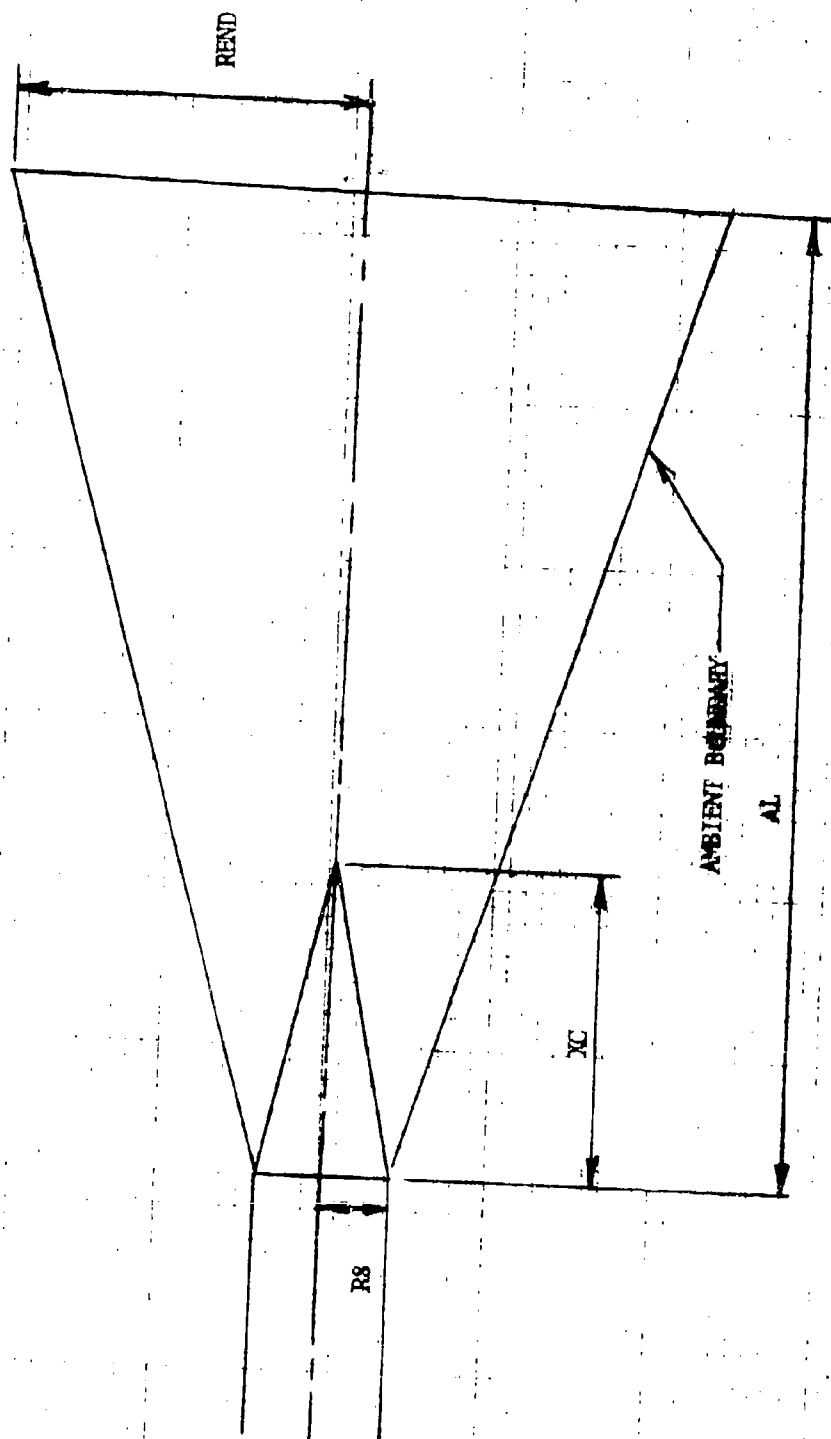


Figure 13. Plume Geometry

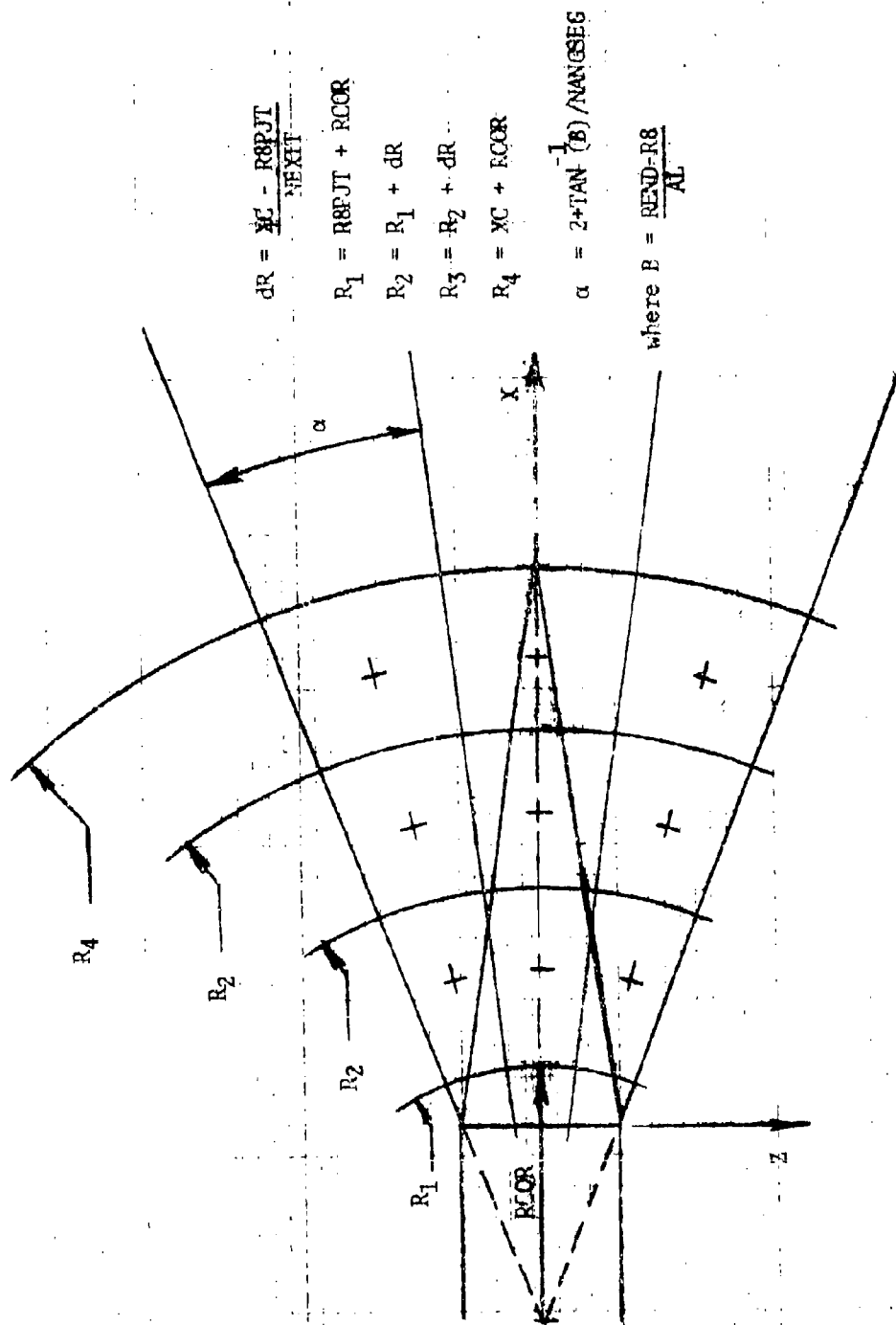
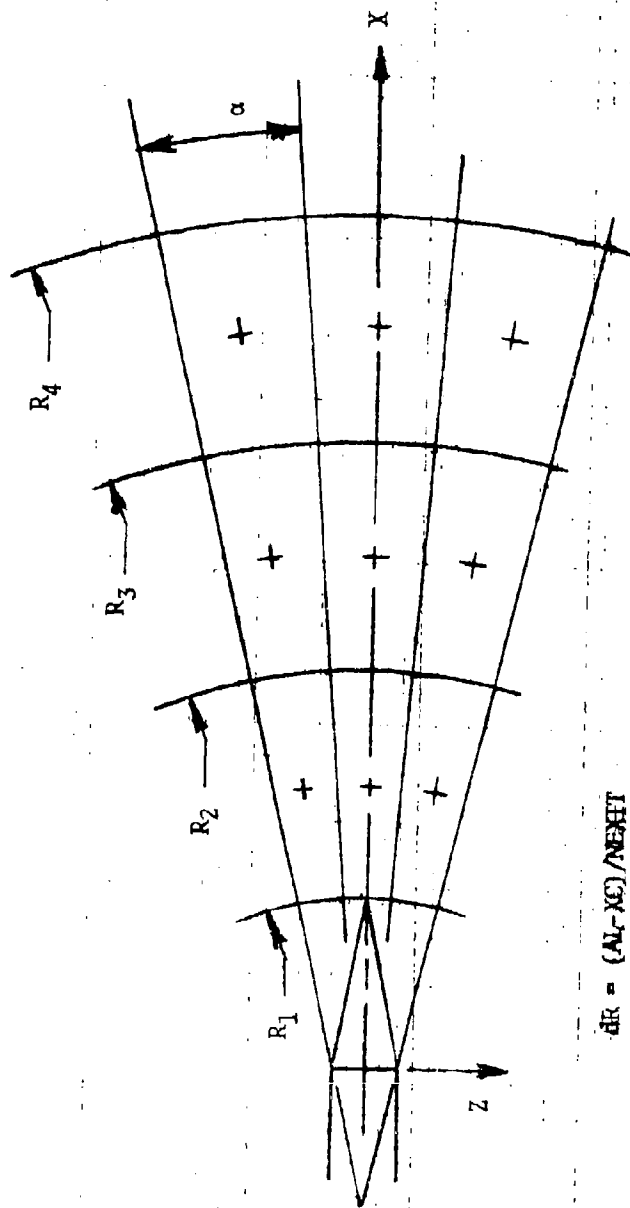


Figure 14. Segmentation of Core Region (X, Z) Plume



$$dR = (AL - XC) / NEHT$$

$$R_1 = XC + R_{COR}$$

$$R_2 = R_1 + dR$$

$$R_3 = R_2 + dR$$

$$R_4 = AL + R_{COR}$$

Figure 15. Segmentation of Non-Core Region (X, Z) Plume

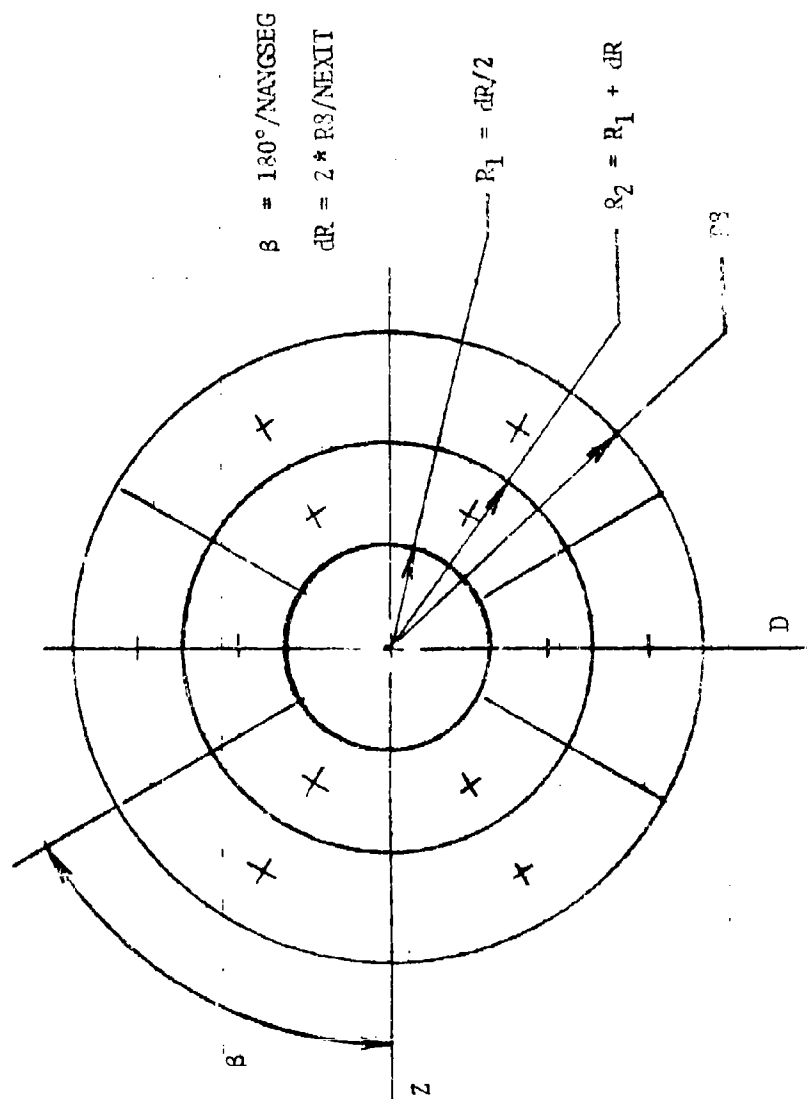


Figure 16. Nozzle Exit Segmentation

PROGRAM: PLURAY (Page A-54)

FUNCTION: Generate the parameters describing the ray which are required in the signature analysis routines.

INPUT: Ray starting geometry, plume gas parameters.

OUTPUT: Ray geometry, gas partial pressures and gas static temperature arrays.

SUBROUTINES: INTERP, START

DESCRIPTION: By referencing the plume gas data and the ray definition parameters, this routine fills the pressure, temperature, and length array with the proper data for ray signature analysis, see figure 17.

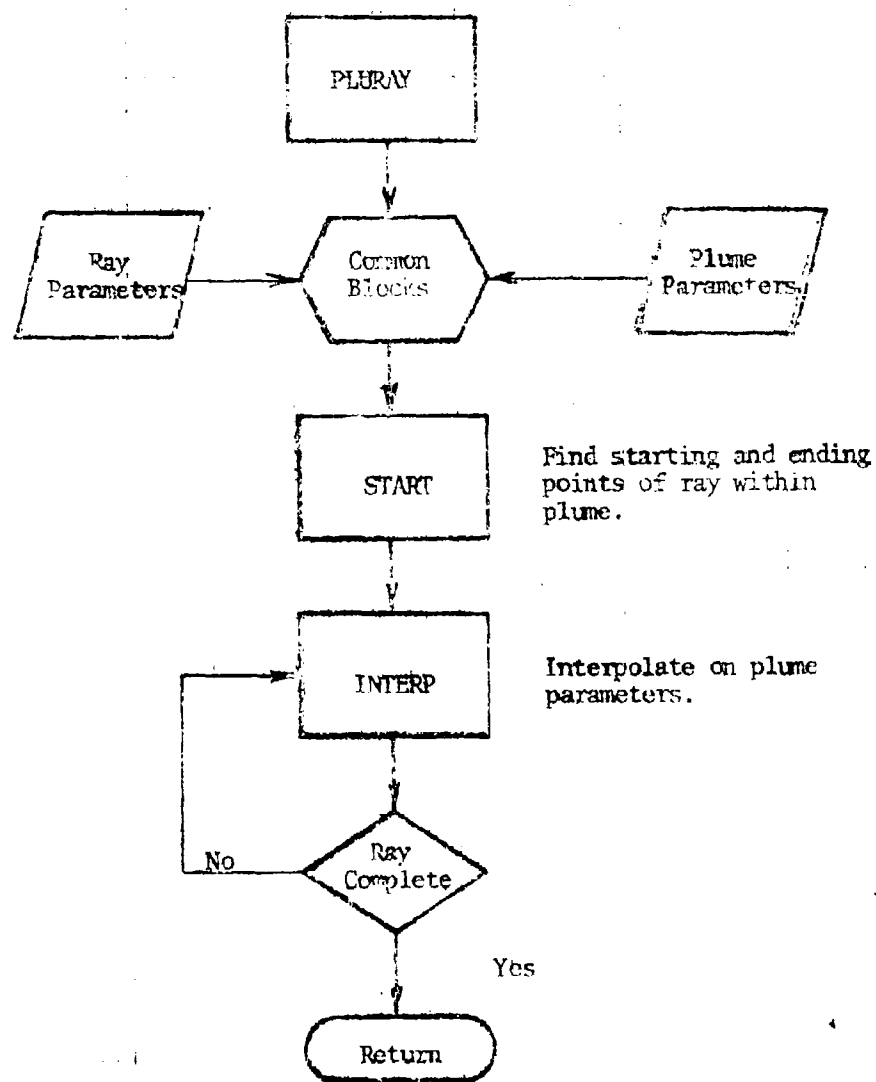


Figure 17. PLURAY Flow Diagram

PROGRAM: START (Page A-57)

FUNCTION: To calculate the starting and ending points of a ray through the plume.

INPUT: Plume geometry, ray intersections

OUTPUT: Starting and ending dimensions of ray

SUBROUTINES: None

DESCRIPTION: The starting and ending points are banded by engine geometry, engine plug geometry and flow field boundaries.

PROGRAM: INTERP (Page A-61)

FUNCTION: Interpolate on gas parameters to find values at a given point within the plume.

INPUT: Gas parameters and coordinates of point in plume.

OUTPUT: Concentration and temperature at input point.

SUBROUTINES: None

DESCRIPTION: This program interpolates between stations along the centerline of the plume and along the radial dimension of the plume to find the static temperature, mole concentrations of water vapor and carbon dioxide and gas pressure at the input coordinate.

PROGRAM: PLUSIG (Page A-63)

FUNCTION: Evaluate the spectral signature and transmittance of a nonuniform gaseous path of NT segments.

INPUT: Ray properties (temp, pressures and lengths), and frequency interval.

OUTPUT: Spectral signature of gaseous ray and spectral transmittance of ray.

SUBROUTINES: ATMOS, KBCAL, PLANCK, INTERPO, SETTAU, TAUCAL, TAUN20, ERF, DAH20, DCO2

DESCRIPTION: The flow diagram for PLUSIG is shown in figure 18. The prime function of this program is to calculate the spectral signatures of nonuniform gas paths with various end conditions. The gaseous ray is divided into NT nonuniform segments with each segment defined by the partial pressures of H_2O (PH_i), CO_2 (PC_i) and broadening gas (PN_i), length (D_i) and static temperature (T_i). A brief discussion of spectral radiators follows:

Continuum radiation is obtained from liquids and solids because the molecules of the substance are in direct contact and exert forces on each other causing all levels of molecular emissions to occur. However, in the case of gas molecules, the intermolecular spacing is large and the free molecular vibrations and rotations result in discrete spectral emissions.

The intensity of these discrete gaseous emissions obeys the PLANCK radiation law as modified by Kirchoff's law. However, the emissivity of the gas is spectrally dependent and radiation is emitted or absorbed only in narrow wavelength intervals called spectral lines. These spectral lines are clustered into tightly spaced sets called bands. The emissivity of the gas is zero outside these bands and dependent upon line spacing and intensity within the bands.

The inhomogeneous gas band-model expressions used in this program were developed at the University of Michigan and are based on the Curtis-Godson approximation. Rather than attempting to fully explain the excellent work performed at the University of Michigan Infrared and Optics Laboratory (now ERIM) in the areas of gaseous emission and absorptions, see references [5, 6, 7, 8, 9, 10].

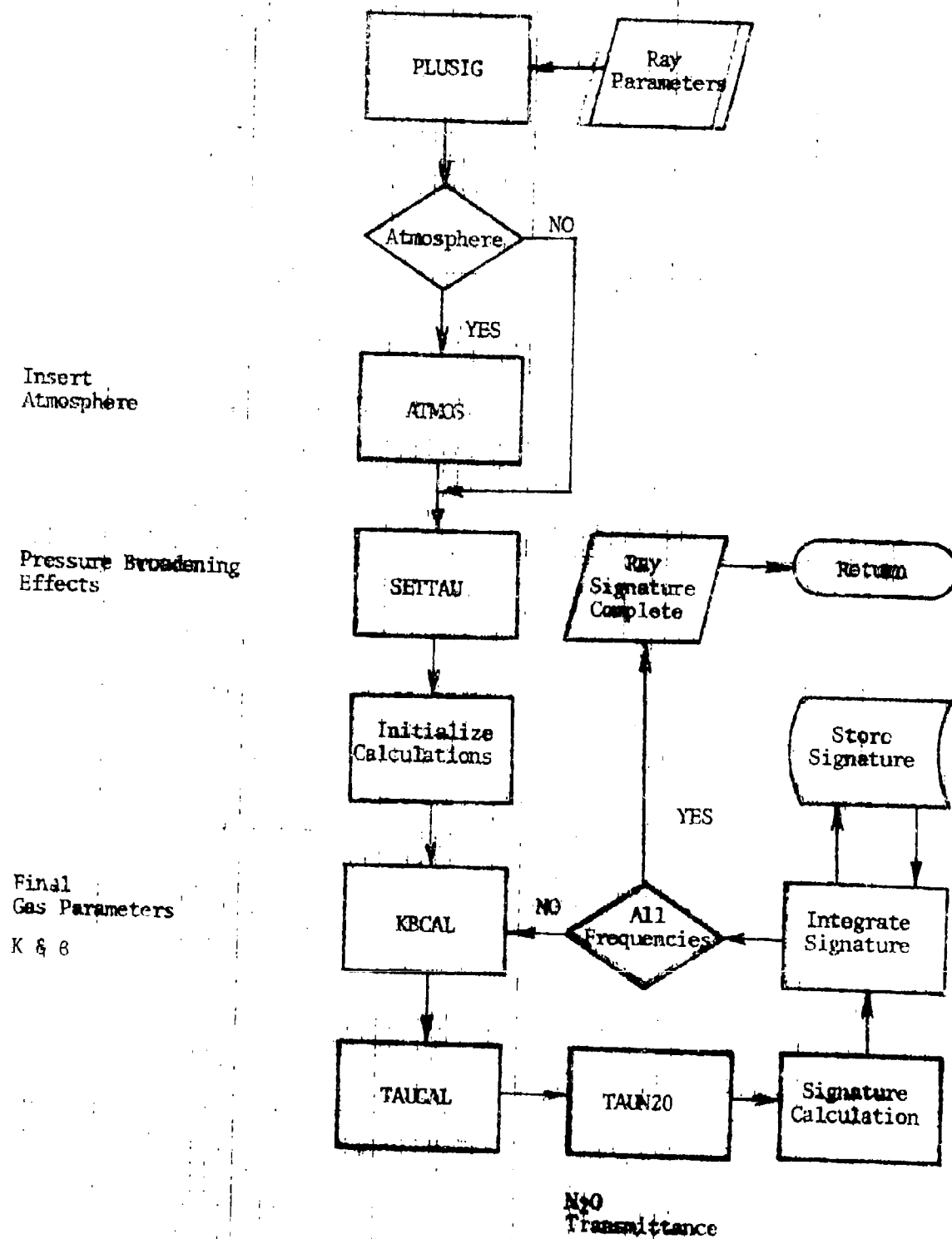


Figure 18. PLUSIG Flow Diagram

A simplified discussion of the function of the program PLUSIG follows: A ray of NT segments, NA of which are atmospheric, of cross sectional area A is entered into the program, figure 19. Each of the NT-NA segments, representing the exhaust plume gas, are described by the gaseous partial pressures, temperatures, and lengths. The atmospheric segments are front loaded in the ray array through the use of the subroutine ATMOS and the range between, and altitudes of the observer and vehicle. The transmissions of each ray segment are calculated in PLUSIG using subroutines KBCAL, INTERPO, SETTAU, TAUCAL, TAUN20, ERF and data contained in Data Blocks DAH20 and DC02.

Figure 19 depicts the information available for a given frequency interval after the exercise of the transmittance calculation subroutines. The signature of the ray is found from

$$L_{ev_ray} = \sum_{i=1}^{NT} L_{ev}(T_i) \cdot \alpha_{vi}$$

where L_{ev} is the PLANCK function and α_{vi} is the absorptance when

$$\alpha_{vi} = (1 - \tau_{vi}) \cdot \prod_{j=1}^i \tau_{vj}$$

The total transmittance, τ , for the gaseous path containing NT elements is extractable,

$$\tau_{v_ray} = \prod_{i=1}^{NT} \tau_{vi}$$

Thus the spectral transmittance can be used to determine the plume and atmospheric attenuation of a black surface at the terminus of the ray, figure 20.

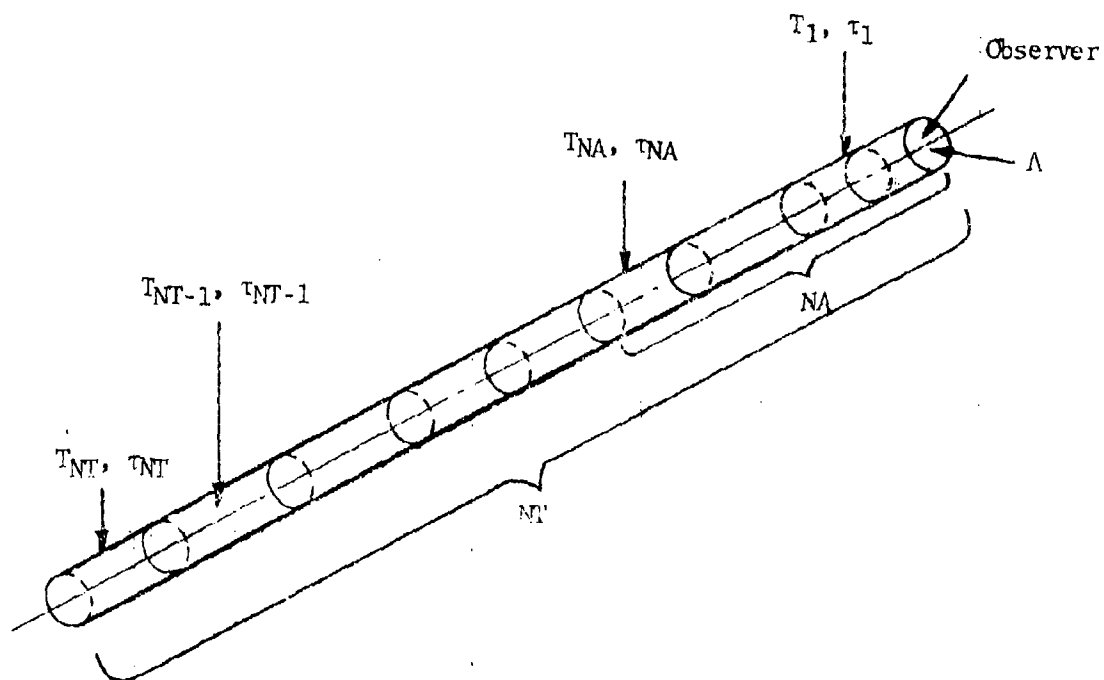


Figure 19. Ray Geometry

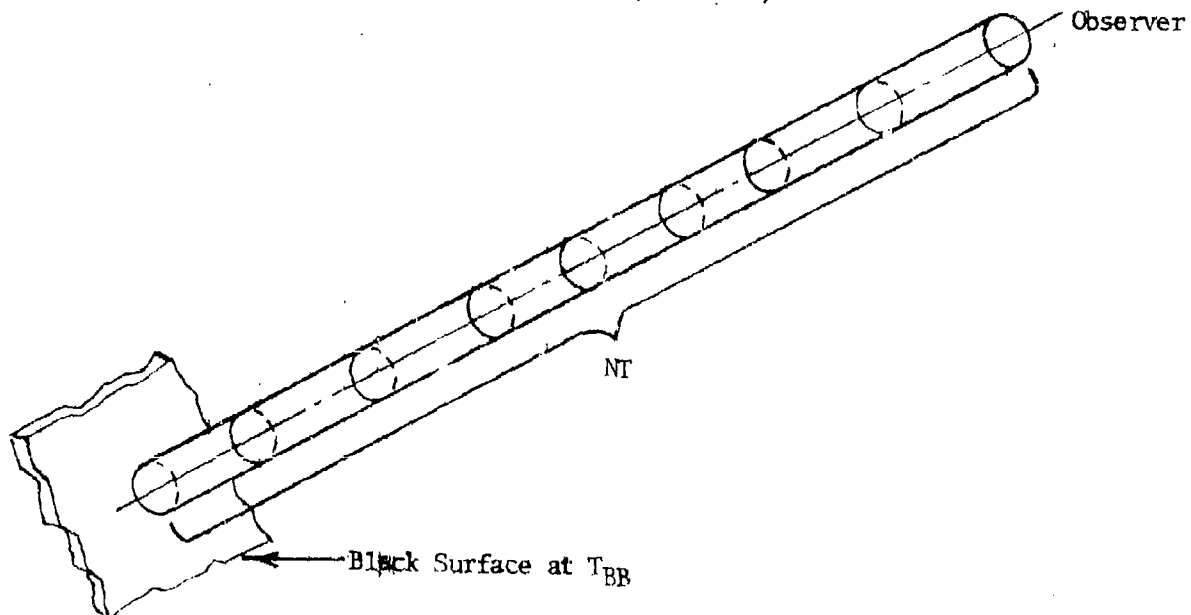


Figure 20. Ray Geometry with Terminating Black Surface

PROGRAM: ATMOS (Page A-69)

FUNCTION: Generate temperatures and partial pressures along an atmospheric path of NA elements and front load the ray pressure and temperature array with the atmospheric data.

INPUT: Range, altitude of plume and observer, number of atmospheric segments

OUTPUT: H₂O, CO₂ and N₂ Pressures

SUBROUTINES: None

DESCRIPTION: Given the geometry of figure 21, the altitude at point r is generated and the temperature and pressures are found from the empirical curve fits used in the computer code. References [8, 11, 12, 13].

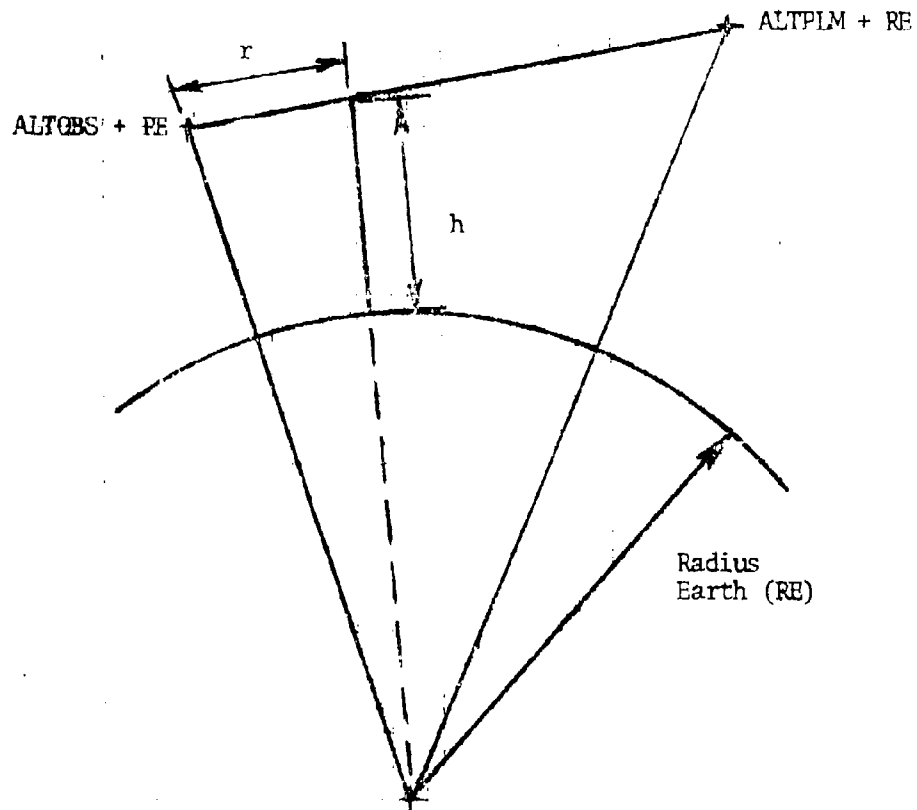


Figure 21. Geometry used in Atmospheric Model

PROGRAM: SETTAU (Page A-70)

FUNCTION: Insert pressure broadening effect of broadening gas by modifying effective gas pressures.

INPUT: H₂O or CO₂ and N₂ gas pressures

OUTPUT: Modified gas pressures (H₂O-N₂ and CO₂-N₂ mixtures)

SUBROUTINE: None

DESCRIPTION: References [6, 7, 8, 9, 10]

PROGRAM: TAUCAL (Page A-71)

FUNCTION: Calculate the gaseous transmittance in a given frequency interval.

INPUT: Pressures, temperatures, gas parameters (X & β)

OUTPUT: Gaseous Transmittances, $\tau(\nu)$

SUBROUTINES: INTERPO

DESCRIPTION: Calculate transmittance of gaseous substance over a given frequency interval using overlapping line approximations.

$$\tau(\nu) = \exp[-\beta_e \cdot f]$$

Where β_e is the effective value of β and f is the Ladenburg-Reiche function. References [6, 10].

PROGRAM: KBCAL (Page A-73)

FUNCTION: To look-up and interpolate on the band model parameters for a given frequency.

INPUT: Frequency, gas type

OUTPUT: K, β , temp and number of temperatures

SUBROUTINES: None

DESCRIPTION: The average line width to spacing ratio multiplied by $1/2 \pi$ called β , and the average line strength to spacing ratio called K are generated in this subroutine. These parameters are found at a given input frequency for H₂O and CO₂ over the temperature range from 300°K to 3000°K.

PROGRAM: Function PLANCK (Page A-75)

FUNCTION: Calculate PLANCK's blackbody function

INPUT: Frequency (cm^{-1}), temperature ($^{\circ}\text{K}$).

OUTPUT: Watts/Steradian/ cm^3

SUBROUTINES: None

DESCRIPTION: From the classical expression for the radiant emittance into a Lambertian hemisphere

$$M_{\text{ev}} = \frac{2\pi(\kappa T)^4}{c^2 h^3} \left(\frac{x^3}{\exp(x) - 1} \right)$$

where

$$x = h\nu/\kappa T$$

the spectral radiant sterance for a given frequency and temperature can be found

$$L_{\text{ev}} = 2hc^2\nu^3/(\exp(x) - 1)$$

See Reference [14].

PROGRAM: Function INTERPO (Page A-76)

FUNCTION: Interpolate over the N dimensional set (X, Y) to find the value at a given point (ARG).

INPUT: X, Y, N, ARG

OUTPUT: INTERPO

SUBROUTINES: None

DESCRIPTION: See Page A-76.

PROGRAM: TAUN20 (Page A-77)

FUNCTION: Calculate transmittance of N_2O in the atmosphere
over selected frequency intervals.

INPUT: Frequency, atmospheric N_2O .

OUTPUT: Transmittance of N_2O in atmosphere.

SUBROUTINES: ERF, INTERFO

DESCRIPTION: See Page A-77.

PROGRAM: Function ERF (Page A-78)

FUNCTION: To evaluate the error function, erf(x).

INPUT: X

OUTPUT: ERF (x)

SUBROUTINES: None

DESCRIPTION: Evaluates the error function.

$$\text{erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x \exp(-t^2) dt$$

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APPENDIX

ASDIR-II

PROGRAM LISTING

APPENDIX

This appendix contains a listing of the Aeronautical Systems Division's Infrared Signature Predicting Model (ASDIR). The computer code was developed in the structural form shown in figure 22. The overlays are organized in three major functional groupings with a fourth overlay dedicated to data initialization. The prime functions of each overlay are:

Overlay

(0,0)	Program Control
(1,0)	Data Input & Initialization
(2,0)	Plume Signature Calculations
(3,0)	Data Initialization
(4,0)	Plume Gas Dynamics
(5,0)	Plume Data I/O
(6,0)	Spectral Filter Data Initialization
(7,0)	Spatial Output
(11,0)	Hot Parts Temperature Calculation
(12,0)	View Factor Calculations
(13,0)	Hot Part Radiation Calculations
(14,0)	Hot Part Data Control

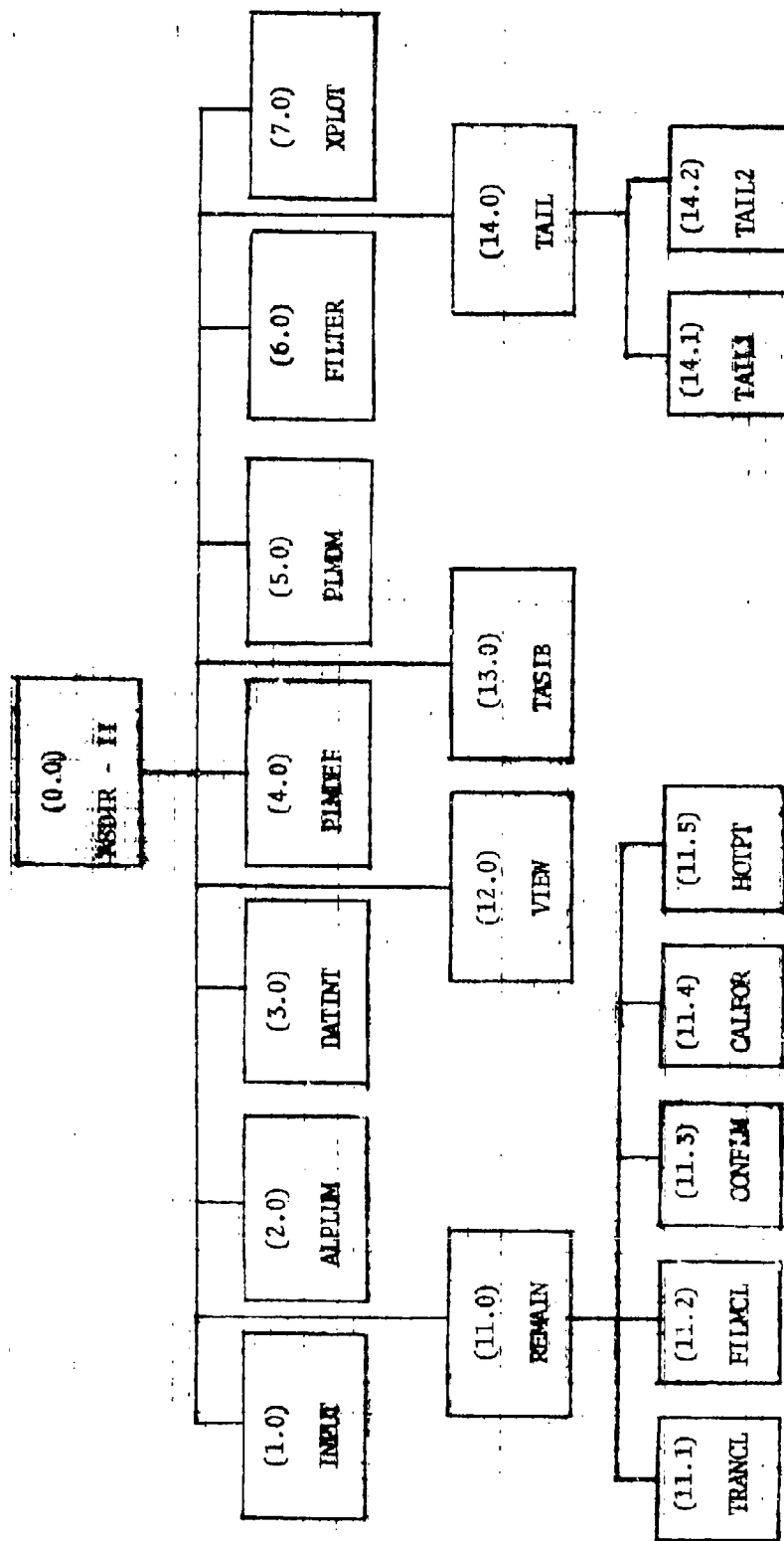


Figure 22. ASDIR-II Overlay Structure

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DECK/TYPE,0,0
COMMON/ASD1R23/INPUT,OUTPUT,PUNCH,TAPE2,TAPE3,
1 TAPE6=TAPE4,TAPE5=INPUT,TAPE6=OUTPUT
2 ASD1R23
3 PLUME COMPUTATION
4 CO=0.0,LINK2/ALINK2,102
5 COMMON/LINK3/ALINK2,102,IMS
6 ASD1R23
7
8
9
10 COMMON/GEN/
11 AL, BA, DQS, MEN, MP,
12 RO, RO2, REM100, RE, RO,
13 RO2, RP2, SC, SS, TANAL,
14 TANP, XC, XEN100, NF, XO,
15 X2, RENO
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60	C	CALL ALPLUMS GO TO 270	ASDIR28 59
	271	CONTINUE	ASDIR28 60
		IF(MCFLOW,EO,1) GO TO 188	ASDIR28 61
		IF(FILTER,ME,0) CALL OVERLAY(MXHP,6,8)	ASDIR28 62
	C	IF(FILTER,ME,0) CALL FILTER	ASDIR28 63
			ASDIR28 64
65	C		ASDIR28 65
			ASDIR28 66
	C	FLOW FIELD IN MAIN REGION	ASDIR28 67
	C		ASDIR28 68
			ASDIR28 69
70		IREAD=DATA/1000000000	ASDIR28 70
		IF(IREAD,EO,400) WRITE(6,400)	ASDIR28 71
		IF(IREAD,EO,400) WRITE(6,400)	ASDIR28 72
		IF(IREAD,EO,400) WRITE(6,400)	ASDIR28 73
		6300 FORMAT(//33M** PLUME DATA IS CALCULATED, **)	ASDIR28 74
75		4431 FORMAT(//33M** PLUME DATA READ FROM INPUT, **)	ASDIR28 75
		4432 FORMAT(//33M** PLUME DATA READ FROM INPUT, **)	ASDIR28 76
		IF(IREAD,ME,400) GO TO 15	ASDIR28 77
		CALL OVERLAY(MXHP,4,0)	ASDIR28 78
	C	CALL PLMDEF8	ASDIR28 79
		IF(IREAD,EO,400) GO TO 15	ASDIR28 80
80		READ(1)	ASDIR28 81
		WRITE(8)	ASDIR28 82
	15	CONTINUE	ASDIR28 83
		CALL OVERLAY(MXHP,5,0)	ASDIR28 84
	C	CALL PLMDEF8	ASDIR28 85
85		OPDX=(PA-P8)/12.08)	ASDIR28 86
		RENINEN+1=REN(10)	ASDIR28 87
		XENINEN+1=0.9	ASDIR28 88
		ZIST=REN0	ASDIR28 89
90	C	INITIALIZE CALCULATION PARAMETERS	ASDIR28 90
	C		ASDIR28 91
		AL=AMT(2)	ASDIR28 92
		IF(AL,CT,XY(49)) AL=XY(49)	ASDIR28 93
		REN0=IN8*AL*P8	ASDIR28 94
95		IF(A5,EO,100.1) DTST =ZTST	ASDIR28 95
		BOS=BOS	ASDIR28 96
		ZM=N02-1	ASDIR28 97
		N0FLON=1	ASDIR28 98
	100	CONTINUE	ASDIR28 99
		A=A5*.0174532926	ASDIR28 101
100	1000	SC=COS(A)	ASDIR28 101
		SS=SIN(A)	ASDIR28 102
		IF(A3,EO,99.08,A8,EO,0.1,60 TO 200	ASDIR28 103
		TANA=SS/SC	ASDIR28 104
105		DTST=AL*TANA	ASDIR28 105
		D=XY(49)/SC	ASDIR28 106
		IF(D,LT,DTST) DTST=D	ASDIR28 107
	200	CONTINUE	ASDIR28 108
		N0Z=36/74	ASDIR28 109
110		IF(N0Z,EO,0.1) GO TO 1000	ASDIR28 110
		N0=N0Z/2	ASDIR28 111
		ADS=105	ASDIR28 112
	C	CALL OVERLAY(MXHP,2,0)	ASDIR28 113
		CALL ALPLUMS	ASDIR28 114
			ASDIR28 115

115

IF ISPA, L, 81 GO TO 270
CALL OVERLAY (AHR-P, 7, 01
C CALL NPLGT
1804 GO TO 270
END

ASDIR23 116

ASDIR24 117

ASDIR25 118

ASDIR26 119

ASDIR27 120

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[illegible]

[illegible]

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364	5621E+01	6284E+01	6975E+01	7786E+01	8493E+01	DC02	364
365	9204E+02	1016E+02	1890E+02	1185E+02	1276E+02	DC02	365
366	1315E+02	1439E+02	1921E+02	1505E+02	1640E+02	DC02	366
367	1697E+02	1734E+02	1769E+02	1793E+02	1817E+02	DC02	367
368	1746E+02	1809E+02	1869E+02	1889E+02	1817E+02	DC02	368
369	DATA (K0215,J)=61,1281					DC02	369
370	1775E+02	1765E+02	1745E+02	1785E+02	1654E+02	DC02	370
371	1680E+02	1706E+02	1556E+02	1444E+02	1223E+02	DC02	371
372	176E+02	692E+01	6427E+01	3314E+01	2496E+01	DC02	372
373	0	0	0	0	0	DC02	373
374	0	0	0	0	0	DC02	374
375	0	0	0	0	0	DC02	375
376	0	0	0	0	0	DC02	376
377	0	0	0	0	0	DC02	377
378	1269E+00	1727E+00	2284E+00	2985E+00	3803E+00	DC02	378
379	5130E+00	6483E+00	8320E+00	1059E+01	1331E+01	DC02	379
380	1663E+01	2558E+01	2539E+01	3083E+01	3717E+01	DC02	380
381	4521E+01	6499E+01	5726E+01	6169E+01	6722E+01	DC02	381
382	6652E+01	7133E+01	7724E+01	8313E+01	8829E+01	DC02	382
383	9144E+01	9470E+01	1045E+02	1090E+02	1140E+02	DC02	383
384	1208E+02	1261E+02	1258E+02	1336E+02	1366E+02	DC02	384
385	1395E+02	1479E+02	1525E+02	1525E+02	1489E+02	DC02	385
386	1483E+02	1477E+02	1422E+02	1447E+02	1310E+02	DC02	386
387	1574E+02	1434E+02	1474E+02	1594E+02	1364E+02	DC02	387
388	DATA (K0216,J)=61,1281					DC02	388
389	1128E+02	1271E+02	1202E+02	1308E+02	1039E+02	DC02	389
390	1113E+02	1177E+02	9080E+01	8851E+01	6587E+01	DC02	390
391	6275E+01	2566E+01	3568E+01	1505E+01	1502E+01	DC02	391
392	0	0	0	0	0	DC02	392
393	0	0	0	0	0	DC02	393
394	1131E+01	3399E+02	6798E+02	8290E+02	9782E+02	DC02	394
395	2458E+01	1324E+01	1565E+01	1806E+01	2132E+01	DC02	395
396	6569E+01	2755E+01	3525E+01	3505E+01	3586E+01	DC02	396
397	7927E+01	5179E+01	5726E+01	6296E+01	7520E+01	DC02	397
398	1334E+01	6882E+01	940F+01	1071E+00	1179E+00	DC02	398
399	1451E+00	1225E+00	1495E+00	1785E+00	1763E+00	DC02	399
400	1451E+00	2463E+00	2116E+00	2256E+00	2471E+00	DC02	400

DATA	CEP2/	DATA	CEP3/	DATA	CEP4/
1.1050E-2	2.160E-0	1.450E+1	2.748E+1	3.190E+1	3.070E+1
1.350E-3	1.40E-0	1.100E+1	2.200E+1	3.300E+1	2.800E+1
1.260E-3	8.20E-1	9.100E-9	5.040E+1	2.700E+1	2.090E+1
1.430E-4	4.450E-1	5.900E-0	4.740E+1	2.400E+1	2.750E+1
1.507E-4	2.49E-1	4.270E-0	1.450E+1	2.200E+1	1.260E+1
1.510E-5	1.270E-1	2.940E-0	1.100E+1	1.900E+1	2.410E+1
1.173E-5	6.30E-2	2.000E-0	9.500E-1	1.690E+1	2.210E+1
1.5710E-5	3.01E-2	1.340E-0	7.40E-0	1.600E+1	1.2290E+1
1.1950E-6	1.40E-2	9.720E-1	1.930E+0	1.200E+1	1.700E+1
1.600E-7	6.20E-3	5.900E-1	4.430E-0	1.030E+1	1.360E+1
1.670E-7	2.750E-3	3.1500E-1	3.300E-0	8.450E-1	1.350E+1
1.113E-6	5.00E-3	2.690E-1	1.1740E-0	5.600E-1	1.000E+1
1.137E-6	2.70E-3	1.2450E-1	1.230E-0	4.500E-1	8.550E-1
1.720E-6	1.030E-3	2.140E-1	1.100E-0	3.500E-1	7.160E-1
1.500E-6	4.60E-3	1.690E-1	1.000E-1	2.700E-1	5.950E-1
1.950E-6	2.930E-3	1.1750E-1	1.730E-1	2.390E-1	4.920E-1
1.100E-5	1.100E-3	5.166E-1	1.6650E-1	2.110E-1	4.050E-1
1.750E-5	1.350E-3	1.650E-1	6.00E-1	1.590E-1	3.520E-1
DATA CEP3/					
1.473E-5	9.570E-5	1.1670E-1	1.6200E-1	1.990E-1	3.120E-1
1.110E-5	2.430E-4	1.1750E-1	1.6300E-1	1.540E-1	2.080E-1
1.100E-5	5.700E-4	1.1000E-1	1.6750E-1	1.1900E-1	1.7810E-1
1.2350E-5	1.50E-3	1.2000E-1	1.750E-1	2.600E-1	2.630E-1
1.400E-4	3.00E-3	2.330E-1	1.650E-1	2.210E-1	3.140E-1
1.600E-4	9.50E-3	3.260E-1	1.8220E-1	2.600E-1	3.600E-1
1.120E-3	2.450E-2	3.430E-1	1.1760E-1	3.200E-1	4.631E-1
1.100E-3	4.20E-2	3.630E-1	1.2510E-1	4.100E-1	5.110E-1
1.3650E-3	1.463E-1	1.1070E-1	1.3900E-1	4.590E-1	5.5420E-1
1.630E-3	3.70E-1	1.1660E-1	1.4050E-1	4.800E-1	5.7140E-1
1.130E-2	6.94E-1	1.2440E-1	1.6590E-1	5.300E-1	5.5770E-1
1.250E-2	1.230E-1	3.410E-1	1.6770E-1	5.020E-1	5.620E-1
1.500E-2	2.120E-1	4.470E-1	1.5470E-1	5.160E-1	5.760E-1
1.100E-1	2.850E-1	1.4830E-1	1.5920E-1	4.970E-1	4.860E-1
1.1219E-1	3.20E-1	1.4910E-1	1.5580E-1	4.670E-1	4.440E-1
1.1350E-1	3.40E-1	5.050E-1	1.6210E-1	4.770E-1	4.540E-1
1.1140E-1	3.610E-1	5.360E-1	1.630E-1	5.030E-1	5.020E-1
1.2490E-1	4.600E-1	6.210E-1	1.6240E-1	5.380E-1	5.140E-1
1.3971E-1	5.80E-1	7.490E-1	1.760E-1	5.010E-1	5.650E-1
DATA CEP4/					
1.1150E-1	1.5270E-2	1.9240E-0	8.490E-1	1.640E-1	1.5440E-1
1.1463E-1	1.250E-1	1.1130E+1	9.400E-1	8.070E-1	6.630E-1
1.1650E-1	1.1550E+1	1.0110E+1	1.6760E-1	5.600E-1	4.630E-1
1.142E-1	6.750E-0	5.570E-0	3.490E-0	2.700E-0	2.630E-0
1.1510E-1	2.030E-1	1.130E-1	1.190E-1	1.300E-1	1.560E-1
1.6030E-1	5.80E-1	1.6630E-1	1.1120E-1	1.200E-1	1.25

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230	1.2100E-4..6680E-4..270E-3..1520E-2..5730E-2..1488E-1..1470E-1..	DAH20	239
	1.2150E-4..6710E-4..280E-3..1540E-2..5790E-2..1498E-1..1470E-1..	DAH20	239
	1.2170E-4..6950E-4..2850E-3..1610E-2..6770E-2..1738E-1..14230E-1..	DAH20	232
	1.2190E-4..7200E-4..2970E-3..1690E-2..7830E-2..1978E-1..1460E-1..	DAH20	233
	1.2200E-4..7710E-4..3430E-3..2360E-2..9250E-2..2268E-1..14700E-1..	DAH20	234
	1.2260E-4..8150E-4..3870E-3..2860E-2..1060E-1..14250E-1..14300E-1..	DAH20	235
	1.2300E-4..8450E-4..4200E-3..3570E-2..1240E-1..1470E-1..1380E-1..	DAH20	236
	1.2310E-4..1920E-3..4700E-3..4670E-2..1680E-1..13130E-1..13900E-1..	DAH20	237
	1.4350E-4..260E-3..1050E-2..5660E-2..1850E-1..13410E-1..13700E-1..	DAH20	238
	DATA CORF11/	DAH20	239
231	1.5220E-4..1230E-3..1200E-2..7360E-2..2290E-1..3780E-1..4220E-1..	DAH20	241
	1.6710E-4..305E-3..1830E-2..9320E-2..2590E-1..4040E-1..4400E-1..	DAH20	241
	1.8850E-4..3950E-3..2450E-2..1280E-1..3020E-1..4300E-1..4560E-1..	DAH20	242
	1.1130E-3..6190E-3..3460E-2..1610E-1..3580E-1..44590E-1..4650E-1..	DAH20	243
	1.1740E-3..8250E-3..440E-2..2000E-1..4170E-1..4930E-1..4730E-1..	DAH20	244
	1.2650E-3..1630E-2..7770E-2..2450E-1..4310E-1..5070E-1..4780E-1..	DAH20	245
	1.3550E-3..2000E-2..9780E-2..3170E-1..4920E-1..5270E-1..4780E-1..	DAH20	246
	1.5110E-3..2710E-2..1670E-1..4010E-1..5030E-1..5230E-1..4730E-1..	DAH20	247
	1.6510E-3..3010E-2..2640E-1..6670E-1..5200E-1..5260E-1..4600E-1..	DAH20	248
	1.9070E-3..5100E-2..3210E-1..6990E-1..5230E-1..5100E-1..4470E-1..	DAH20	249
250	1.1350E-2..550E-2..3090E-1..5280E-1..5130E-1..4920E-1..4300E-1..	DAH20	250
	1.2260E-2..1300E-1..470E-1..5590E-1..5000E-1..4690E-1..4450E-1..	DAH20	251
	1.4110E-2..1980E-1..5280E-1..5570E-1..4830E-1..4520E-1..4000E-1..	DAH20	252
	1.6200E-2..2820E-1..840E-1..4950E-1..4510E-1..4300E-1..3900E-1..	DAH20	253
	1.9000E-2..3900E-1..470E-1..4490E-1..4300E-1..4230E-1..3850E-1..	DAH20	254
	1.1300E-1..4620E-1..1420E-1..3910E-1..4030E-1..44150E-1..3930E-1..	DAH20	255
	1.3400E-1..7100E-1..4020E-1..3600E-1..3840E-1..4410E-1..4050E-1..	DAH20	256
	1.7480E-1..5900E-1..3990E-1..3600E-1..3760E-1..4200E-1..4180E-1..	DAH20	257
	1.1110E-0..3680E-1..3400E-1..3690E-1..4090E-1..4540E-1..4340E-1..	DAH20	258
	DATA CORF12/	DAH20	259
260	1.3590E-1..2850E-1..3690E-1..6230E-1..610E-1..4820E-1..4500E-1..	DAH20	260
	1.2010E-1..2780E-1..4320E-1..5290E-1..5290E-1..5110E-1..4620E-1..	DAH20	261
	1.1810E-1..4220E-1..520E-1..5980E-1..5720E-1..5440E-1..4700E-1..	DAH20	262
	1.1390E-1..1050E-0..840E-1..6870E-1..5930E-1..5600E-1..4800E-1..	DAH20	263
	1.7740E-1..7100E-1..6830E-1..6180E-1..5560E-1..5340E-1..4780E-1..	DAH20	264
	1.7580E-1..4430E-1..5790E-1..5470E-1..5030E-1..4950E-1..4600E-1..	DAH20	265
	1.9850E-1..570E-1..5890E-1..5100E-1..4510E-1..4490E-1..4250E-1..	DAH20	266
	1.930E-1..6320E-1..5390E-1..6890E-1..4540E-1..4460E-1..4000E-1..	DAH20	267
	1.6800E-1..6800E-1..5430E-1..4950E-1..4600E-1..4580E-1..4050E-1..	DAH20	268
	1.3250E-1..5230E-1..5150E-1..430E-1..4490E-1..4540E-1..4180E-1..	DAH20	269
270	1.1500E-1..3500E-1..4510E-1..4640E-1..4520E-1..4490E-1..4380E-1..	DAH20	270
	1.5200E-2..2380E-1..3690E-1..4680E-1..4140E-1..4170E-1..4200E-1..	DAH20	271
	1.2700E-2..1500E-1..2820E-1..3390E-1..3660E-1..3840E-1..4080E-1..	DAH20	272
	1.1130E-2..1810E-1..2030E-1..2630E-1..3830E-1..3380E-1..3600E-1..	DAH20	273
	1.890E-3..5900E-2..1400E-1..2060E-1..2470E-1..2950E-1..3200E-1..	DAH20	274
	1.3650E-3..3100E-2..3690E-2..1540E-1..2030E-1..2580E-1..2800E-1..	DAH20	275
	1.2480E-3..1300E-2..5800E-2..1120E-1..1160E-1..12280E-1..2500E-1..	DAH20	276
	1.1280E-3..1400E-3..4170E-2..8500E-2..1340E-1..1908E-1..2200E-1..	DAH20	277
	1.1330E-3..2620E-3..2080E-2..5940E-2..1090E-1..1620E-1..1900E-1..	DAH20	278
	DATA CORF13/	DAH20	279
280	1.7110E-4..1810E-3..1420E-2..4550E-2..9070E-2..1410E-1..1700E-1..	DAH20	280
	1.6550E-4..1150E-3..8100E-3..316E-2..6980E-2..1210E-1..1500E-1..	DAH20	281
	1.4990E-4..1110E-3..6240E-3..2300E-2..5510E-2..1820E-1..1300E-1..	DAH20	282
	1.3590E-4..6770E-4..4250E-3..1240E-2..3850E-2..1100E-2..1200E-1..	DAH20	283
	1.2310E-4..5630E-4..2780E-3..9860E-3..2900E-2..6720E-2..1850E-1..	DAH20	284
	1.1550E-4..4810E-4..2470E-3..9440E-3..2530E-2..6120E-2..9490E-2..	DAH20	285
	1.1260E-4..4130E-4..2410E-3..8860E-3..2200E-2..5820E-2..9400E-2..	DAH20	286

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345	1.1175E-1..3690E-1..3850E-1..2490E-1..2120E-1..2080E-1..2000E-1..	DAM20	344
	1.1400E-1..3700E-1..4190E-1..2720E-1..2280E-1..2130E-1..2240E-1..	DAM20	345
	1.1250E-1..4130E-1..4680E-1..2400E-1..2400E-1..2290E-1..2430E-1..	DAM20	346
	1.1600E-1..4600E-1..4270E-1..2500E-1..2630E-1..2380E-1..2600E-1..	DAM20	347
	1.1305E-1..3450E-1..3740E-1..2590E-1..2350E-1..2400E-1..2600E-1..	DAM20	348
	1.1820E-1..1730E-1..2020E-1..2310E-1..2140E-1..2140E-1..2430E-1..	DAM20	349
	1.1700E-1..6100E-2..1910E-1..1750E-1..1810E-1..1340E-1..2100E-1..	DAM20	350
	1.1413E-1..3700E-2..1054E-1..1270E-1..1520E-1..1370E-1..1800E-1..	DAM20	351
	1.1451E-1..1700E-2..5540E-2..8550E-2..1130E-1..1310E-1..1500E-1..	DAM20	352
	1.1751E-2..1450E-2..3850E-2..5550E-2..6030E-2..9450E-2..1200E-1..	DAM20	353
350	1.1722E-3..7540E-3..3840E-2..5750E-2..5370E-2..5940E-2..8000E-2..	DAM20	354
	1.1431E-3..6030E-3..3810E-2..4530E-2..3400E-2..4140E-2..6200E-2..	DAM20	355
	1.1275E-3..4100E-3..1930E-2..3600E-2..3190E-2..3320E-2..5000E-2..	DAM20	356
	1.1451E-3..2000E-3..1310E-2..2320E-2..2470E-2..2560E-2..4200E-2..	DAM20	357
	1.1310E-3..1600E-3..9150E-3..1500E-2..1860E-2..1970E-2..3700E-2..	DAM20	358
	DATA COEF17		359
	1.6311E-4..1105E-3..5650E-3..1140E-2..2050E-2..1920E-2..3400E-2..	DAM20	360
	1.4743E-4..7571E-4..1181E-2..1240E-2..1750E-2..1870E-2..3200E-2..	DAM20	361
	1.1353E-4..5950E-4..5280E-3..1140E-2..1600E-2..1850E-2..3000E-2..	DAM20	362
	1.2403E-4..4930E-4..2530E-3..8420E-3..1410E-2..1840E-2..2900E-2..	DAM20	363
365	1.1703E-4..3630E-4..1230E-3..4350E-3..1240E-2..1620E-2..2920E-2..	DAM20	364
	1.1201E-4..2490E-4..1210E-3..4350E-3..1180E-2..1670E-2..2910E-2..	DAM20	365
	1.1810E-5..1700E-4..1030E-3..4390E-3..1260E-2..1920E-2..2950E-2..	DAM20	366
	1.1557E-5..1200E-4..660E-4..3670E-3..1195E-2..1930E-2..3000E-2..	DAM20	367
	1.1391E-5..9030E-5..7160E-4..3510E-3..1160E-2..1940E-2..3030E-2..	DAM20	368
	1.2951E-5..8300E-5..3730E-4..2540E-3..1140E-2..1960E-2..3100E-2..	DAM20	369
	1.1230E-5..5030E-5..4450E-4..2500E-3..1170E-2..2010E-2..3200E-2..	DAM20	370
	1.1251E-5..4200E-5..3670E-4..2520E-3..1160E-2..2150E-2..3300E-2..	DAM20	371
	1.1223E-5..6430E-5..3710E-4..2680E-3..11270E-2..2110E-2..3400E-2..	DAM20	372
	1.1223E-5..9200E-5..3960E-4..2730E-3..1280E-2..2160E-2..3550E-2..	DAM20	373
370	1.2351E-5..1030E-4..4150E-4..2630E-3..1210E-2..2210E-2..3650E-2..	DAM20	374
	1.2801E-5..1250E-4..6330E-4..3630E-3..1360E-2..2310E-2..3800E-2..	DAM20	375
	1.1310E-5..1500E-4..9790E-4..4620E-3..1580E-2..2410E-2..4000E-2..	DAM20	376
	1.1370E-5..1800E-4..1200E-3..5400E-3..1670E-2..2510E-2..4100E-2..	DAM20	377
	1.1420E-5..2000E-4..9870E-4..5890E-3..1710E-2..2570E-2..4200E-2..	DAM20	378
	DATA COEF18		379
	1.5181E-5..2600E-4..1340E-3..5470E-3..1730E-2..2670E-2..4400E-2..	DAM20	380
	1.6401E-5..2700E-4..1210E-3..5340E-3..1720E-2..2740E-2..4570E-2..	DAM20	381
	1.1720E-5..3000E-4..2040E-3..6840E-3..1840E-2..2850E-2..4680E-2..	DAM20	382
	1.1920E-5..3300E-4..2780E-3..8190E-3..1990E-2..2970E-2..4790E-2..	DAM20	383
385	1.1403E-4..3030E-4..3170E-3..8590E-3..2140E-2..3080E-2..4350E-2..	DAM20	384
	1.1253E-4..4200E-4..2400E-3..8180E-3..2200E-2..3170E-2..4300E-2..	DAM20	385
	1.1457E-4..5050E-4..4520E-3..1090E-2..2300E-2..2930E-2..4990E-2..	DAM20	386
	1.1751E-4..5600E-4..3010E-3..940E-2..2430E-2..3420E-2..5000E-2..	DAM20	387
	1.1981E-4..6300E-4..2800E-3..1070E-2..2600E-2..3530E-2..5300E-2..	DAM20	388
	1.2301E-4..7100E-4..2760E-3..1090E-2..2720E-2..3650E-2..5020E-2..	DAM20	389
	1.2601E-4..8100E-4..3690E-3..1270E-2..2950E-2..3770E-2..5100E-2..	DAM20	390
	1.3301E-4..8900E-4..4300E-3..1390E-2..3160E-2..3850E-2..5200E-2..	DAM20	391
	1.3601E-4..9500E-4..4710E-3..1350E-2..3080E-2..3840E-2..4990E-2..	DAM20	392
	1.3901E-4..9800E-4..4340E-3..1470E-2..3160E-2..3850E-2..4950E-2..	DAM20	393
395	1.4201E-4..9900E-4..3970E-3..1430E-2..3180E-2..3840E-2..4900E-2..	DAM20	394
	1.4301E-4..9800E-4..3640E-3..1410E-2..3170E-2..3810E-2..4800E-2..	DAM20	395
	1.3900E-4..9400E-4..3903E-3..1420E-2..3140E-2..3760E-2..4750E-2..	DAM20	396
	1.3801E-4..9000E-4..3100E-3..1450E-2..3180E-2..3750E-2..4630E-2..	DAM20	397
	1.3301E-4..7500E-4..3580E-3..1360E-2..3100E-2..3720E-2..4550E-2..	DAM20	398
	DATA COEF19		399
	1.3301E-4..6930E-4..1430E-3..1360E-2..3090E-2..3690E-2..4430E-2..	DAM20	400

[illegible]

[illegible]

685	*.1F 21E+1..419E+0..1439E+1..5949E+1..2580E+2..6158E+2..1169E+3..	DAH20	686
	*.1822E+1..3738E+0..1281E+1..5159E+1..2310E+2..5474E+2..1060E+3..	DAH20	687
	*.1613E+1..3311E+0..1138E+1..4475E+1..2086E+2..4858E+2..9625E+2..	DAH20	688
	*.1594E+1..2954E+0..1005E+1..3866E+1..1841E+2..4311E+2..8739E+2..	DAH20	689
	*.1565E+1..2623E+0..889E+0..3365E+1..1647E+2..3827E+2..7979E+2..	DAH20	690
690	*.1525E+1..2128E+0..787E+0..2925E+1..1472E+2..3392E+2..7219E+2..	DAH20	691
	*.1482E+1..2036E+0..6973E+0..2538E+1..1319E+2..3011E+2..6586E+2..	DAH20	692
	*.1433E+1..1835E+0..6175E+0..2203E+1..1178E+2..2674E+2..5953E+2..	DAH20	693
	*.1371E+1..1619E+0..5472E+0..1913E+1..1049E+2..2370E+2..5404E+2..	DAH20	694
	*.1309E+1..1465E+0..4843E+0..1640E+1..933E+1..2102E+2..4939E+2..	DAH20	695
695	*.1245E+1..1230E+0..4285E+0..1371E+1..8384E+1..1667E+2..4475E+2..	DAH20	696
	*.1177E+1..1156E+0..3802E+0..1254E+1..7735E+1..1527E+2..3492E+2..	DAH20	697
	*.1105E+1..1032E+0..3361E+0..1079E+1..6694E+1..1471E+2..3711E+2..	DAH20	698
	*.1022E+1..9147E+0..2983E+0..9379E+0..5980E+1..1305E+2..3373E+2..	DAH20	699
	*.9753E+0..2816E+0..4495E+0..9156E+0..2591E+1..1075E+2..3449E+2..	DAH20	700
700	*.9123E+0..2557E+0..4153E+0..9007E+0..2990E+1..1007E+2..3677E+2..	DAH20	701
	DATA CCEP37	DAH20	702
	*.8509E+0..4000E+0..1041E+0..8858E+0..2386E+1..8933E+1..1434E+2..	DAH20	703
	*.7925E+0..2869E+0..4159E+0..6748E+0..2728E+1..9873E+1..4222E+2..	DAH20	704
	*.7381E+0..2475E+0..3689E+0..8710E+0..2709E+1..9433E+1..3774E+2..	DAH20	705
705	*.6871E+0..2197E+0..3539E+0..6561E+0..2351E+1..8504E+1..3251E+2..	DAH20	706
	*.6401E+0..2428E+0..3658E+0..8466E+0..2163E+1..7478E+1..2930E+2..	DAH20	707
	*.5973E+0..1577E+0..3204E+0..8337E+0..2310E+1..8113E+1..2651E+2..	DAH20	708
	*.5279E+0..1242E+0..2710E+0..1263E+0..2415E+1..1826E+1..2328E+2..	DAH20	709
710	*.5221E+0..1030E+0..2415E+0..8188E+0..2779E+1..9140E+1..2517E+2..	DAH20	710
	*.4615E+0..7574E+0..12121E+0..7891E+0..2720E+1..8139E+1..2140E+2..	DAH20	711
	*.4365E+0..1139E+0..2710E+0..9188E+0..2697E+1..8260E+1..2204E+2..	DAH20	712
	*.4168E+0..9852E+0..2394E+0..7593E+0..2597E+1..7927E+1..2107E+2..	DAH20	713
	*.3953E+0..1289E+0..2741E+0..7748E+0..2527E+1..7758E+1..2140E+2..	DAH20	714
715	*.3788E+0..1602E+0..3172E+0..8710E+0..2650E+1..8456E+1..2515E+2..	DAH20	715
	*.3651E+0..2295E+0..4012E+0..1005E+1..2726E+1..8522E+1..2516E+2..	DAH20	716
	*.3531E+0..2361E+0..4190E+0..1159E+1..2685E+1..9140E+1..2706E+2..	DAH20	717
	*.3499E+0..1205E+0..2731E+0..9454E+0..2720E+1..9286E+1..2596E+2..	DAH20	718
	*.3385E+0..5188E+0..1701E+0..8040E+0..2814E+1..8945E+1..2254E+2..	DAH20	719
720	*.3339E+0..5508E+0..1676E+0..7445E+0..2474E+1..6843E+1..1921E+2..	DAH20	720
	DATA CCEP37	DAH20	721
	*.3319E+0..4590E+0..1449E+0..6752E+0..2245E+1..6598E+1..1786E+2..	DAH20	722
	*.3314E+0..7148E+0..1785E+0..6796E+0..2140E+1..7136E+1..2242E+2..	DAH20	723
	*.3309E+0..7918E+0..1932E+0..7109E+0..2310E+1..7478E+1..2461E+2..	DAH20	724
725	*.3379E+0..1228E+0..2531E+0..8263E+0..2761E+1..9629E+1..3998E+2..	DAH20	725
	*.3343E+0..5590E+0..5350E+0..1124E+1..3916E+1..1214E+2..3523E+3..	DAH20	726
	*.3532E+0..1103E+1..7372E+0..1340E+1..5165E+1..5376E+2..1406E+4..	DAH20	727
	*.3624E+0..5623E+0..4883E+0..1102E+1..4731E+1..4340E+2..1022E+4..	DAH20	728
	*.3776E+0..9705E+0..5976E+0..9520E+0..3043E+1..9824E+1..3069E+3..	DAH20	729
730	*.3934E+0..2609E+0..1634E+0..8185E+0..2392E+1..6305E+1..4559E+2..	DAH20	730
	*.4128E+0..2197E+0..3287E+0..8114E+0..2468E+1..6549E+1..3685E+2..	DAH20	731
	*.4344E+0..1526E+0..2686E+0..8114E+0..2345E+1..6452E+1..2191E+2..	DAH20	732
	*.4585E+0..1785E+0..3258E+0..9082E+0..2638E+1..7575E+1..2575E+2..	DAH20	733
	*.4679E+0..1579E+0..3571E+0..1087E+1..3096E+1..8211E+1..1955E+2..	DAH20	734
735	*.5194E+0..1220E+0..3476E+0..1295E+1..4145E+1..1202E+2..2579E+2..	DAH20	735
	*.5544E+0..1120E+0..3508E+0..1422E+1..5752E+1..1540E+2..4032E+2..	DAH20	736
	*.5949E+0..9902E+0..3198E+0..1458E+1..6566E+1..2353E+2..5446E+2..	DAH20	737
	*.6367E+0..1059E+0..3623E+0..1608E+1..7739E+1..2624E+2..46670E+2..	DAH20	738
	*.6835E+0..1135E+0..3958E+0..1787E+1..9088E+1..2854E+2..6190E+2..	DAH20	739
740	*.7339E+0..1216E+0..4337E+0..1985E+1..1067E+2..3168E+2..1005E+3..	DAH20	740
	DATA CCEP37	DAH20	741
		DAH20	742

800	DATA COEF=0	0.3453E+00, 0.229E-10, 1.781E+00, 9.821E+00, 4.374E+01, 1.579E+20, 4.686E+20, 3.550E+00, 3.410E-10, 1.505E+00, 9.454E+00, 4.896E+01, 1.862E+20, 5.910E+20	DAM20	809
801			DAM20	801
802			DAM20	802
803			DAM20	803
804			DAM20	804
805			DAM20	805
806			DAM20	806
807			DAM20	807
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810			DAM20	810
811			DAM20	811
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813			DAM20	813
814			DAM20	814
815			DAM20	815
816			DAM20	816
817			DAM20	817
818			DAM20	818
819			DAM20	819
820			DAM20	820
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852			DAM20	852
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854			DAM20	854
855			DAM20	855
856			DAM20	856

857	5899E+00	6103E+00	1629E+01	7072E+01	3862E+01	6344E+01	8096E+01	DAH20	857
858	4791E+01	5718E+01	9688E+01	1967E+01	3638E+01	9963E+01	8656E+01	DAH20	858
859	4519E+00	5410E+00	9119E+00	1887E+00	3428E+00	5828E+01	7978E+01	DAH20	859
860	4209E+00	5123E+00	8634E+00	1739E+00	3243E+00	5328E+01	7553E+01	DAH20	860
861	4073E+00	4972E+00	8510E+00	1658E+00	3088E+00	5064E+01	7101E+01	DAH20	861
862	DATA CODES/							DAH20	862
863	3089E+00	4656E+00	7546E+00	1590E+00	2946E+00	4841E+01	6064E+01	DAH20	863
864	3737E+00	4470E+00	7535E+00	1481E+00	2828E+00	4649E+01	5900E+01	DAH20	864
865	3604E+00	4314E+00	7277E+00	1466E+00	2733E+00	4490E+01	5766E+01	DAH20	865
866	3503E+00	4193E+00	7069E+00	1424E+00	2654E+00	4361E+01	5640E+01	DAH20	866
867	3422E+00	4090E+00	6907E+00	1351E+00	2593E+00	4261E+01	5541E+01	DAH20	867
868	3367E+00	4029E+00	6891E+00	1335E+00	2590E+00	4189E+01	5490E+01	DAH20	868
869	3331E+00	3935E+00	6712E+00	1335E+00	2628E+00	4145E+01	5477E+01	DAH20	869
870	3314E+00	3899E+00	6692E+00	1347E+00	2518E+00	4127E+01	5451E+01	DAH20	870
871	3324E+00	3977E+00	6704E+00	1370E+00	2510E+00	4136E+01	5464E+01	DAH20	871
872	3324E+00	4014E+00	6761E+00	1362E+00	2530E+00	4172E+01	5515E+01	DAH20	872
873	3324E+00	4072E+00	6851E+00	1382E+00	2577E+00	4234E+01	5603E+01	DAH20	873
874	3374E+00	4159E+00	7019E+00	1432E+00	2635E+00	4325E+01	56510E+01	DAH20	874
875	3369E+00	4274E+00	7202E+00	1491E+00	2705E+00	4444E+01	5829E+01	DAH20	875
876	3382E+00	4415E+00	7444E+00	1499E+00	2795E+00	4593E+01	6010E+01	DAH20	876
877	3384E+00	4530E+00	7737E+00	1599E+00	2905E+00	4773E+01	6767E+01	DAH20	877
878	4065E+00	4795E+00	8063E+00	1628E+00	3035E+00	4985E+01	7071E+01	DAH20	878
879	4207E+00	5034E+00	8467E+00	1710E+00	3186E+00	5235E+01	7422E+01	DAH20	879
880	4436E+00	5317E+00	8951E+00	1807E+00	3361E+00	5523E+01	7827E+01	DAH20	880
881	4693E+00	5623E+00	9478E+00	1938E+00	3599E+00	5846E+01	8231E+01	DAH20	881
882	DATA CODES/							DAH20	882
883	4992E+00	5977E+00	1007E+01	2009E+01	3736E+01	6217E+01	8011E+01	DAH20	883
884	5326E+00	6372E+00	1074E+01	2163E+01	4033E+01	6528E+01	8393E+01	DAH20	884
885	5684E+00	6810E+00	1143E+01	2312E+01	4310E+01	7082E+01	1004E+02	DAH20	885
886	5939E+00	7293E+00	1230E+01	2477E+01	4616E+01	7806E+01	1078E+02	DAH20	886
887	6535E+00	7825E+00	1330E+01	2667E+01	4952E+01	8138E+01	1153E+02	DAH20	887
888	7041E+00	8400E+00	1416E+01	2835E+01	5316E+01	8734E+01	1234E+02	DAH20	888
889	7517E+00	9023E+00	1521E+01	3063E+01	5936E+01	9336E+01	1333E+02	DAH20	889
890	8093E+00	9688E+00	1631E+01	3290E+01	6133E+01	1007E+02	1428E+02	DAH20	890
891	8686E+00	10403E+00	1752E+01	3524E+01	6578E+01	1081E+02	1532E+02	DAH20	891
892	9300E+00	1114E+01	1874E+01	3732E+01	7047E+01	1158E+02	1642E+02	DAH20	892
893	9351E+00	1191E+01	2009E+01	4046E+01	7540E+01	1239E+02	1751E+02	DAH20	893
894	1022E+01	1271E+01	2141E+01	4315E+01	8044E+01	1328E+02	1874E+02	DAH20	894
895	1129E+01	1352E+01	2279E+01	4589E+01	8554E+01	1406E+02	1993E+02	DAH20	895
896	1197E+01	1433E+01	2414E+01	4864E+01	9068E+01	1490E+02	2112E+02	DAH20	896
897	1261E+01	1512E+01	2549E+01	5135E+01	9574E+01	1573E+02	2229E+02	DAH20	897
898	1324E+01	1590E+01	2679E+01	5399E+01	1008E+02	1653E+02	2343E+02	DAH20	898
899	1389E+01	1662E+01	2803E+01	5646E+01	1056E+02	1729E+02	2452E+02	DAH20	899
900	1466E+01	1731E+01	2916E+01	5875E+01	1095E+02	1800E+02	2551E+02	DAH20	900
901	1496E+01	1798E+01	3018E+01	6080E+01	1133E+02	1862E+02	2640E+02	DAH20	901
902	DATA CODES/							DAH20	902
903	1541E+01	1863E+01	3106E+01	6257E+01	1166E+02	1916E+02	2717E+02	DAH20	903
904	1579E+01	1905E+01	3177E+01	6400E+01	1193E+02	1968E+02	2779E+02	DAH20	904
905	1631E+01	1916E+01	3229E+01	6505E+01	1212E+02	1993E+02	2825E+02	DAH20	905
906	1617E+01	1936E+01	3265E+01	6572E+01	1225E+02	2013E+02	2853E+02	DAH20	906
907	1623E+01	1943E+01	3275E+01	6595E+01	1229E+02	2020E+02	2864E+02	DAH20	907
908	1613E+01	1938E+01	3265E+01	6578E+01	1226E+02	2015E+02	2856E+02	DAH20	908
909	1604E+01	1920E+01	3236E+01	6516E+01	1215E+02	1996E+02	2830E+02	DAH20	909
910	1579E+01	1930E+01	3185E+01	6477E+01	1196E+02	1965E+02	2786E+02	DAH20	910
911	1545E+01	1949E+01	3117E+01	6280E+01	1171E+02	1923E+02	2727E+02	DAH20	911
912	1503E+01	1798E+01	3032E+01	6139E+01	1139E+02	1870E+02	2652E+02	DAH20	912
913	1451E+01	1733E+01	2932E+01	5927E+01	1101E+02	1809E+02	2505E+02	DAH20	913

915	914	913	912	911	910	909	908	907	906	905	904	903	902	901	900	899	898	897	896	895	894	893	892	891	890	889	888	887	886	885	884	883	882	881	880	879	878	877	876	875	874	873	872	871	870	869	868	867	866	865	864	863	862	861	860	859	858	857	856	855	854	853	852	851	850	849	848	847	846	845	844	843	842	841	840	839	838	837	836	835	834	833	832	831	830	829	828	827	826	825	824	823	822	821	820	819	818	817	816	815	814	813	812	811	810	809	808	807	806	805	804	803	802	801	800	799	798	797	796	795	794	793	792	791	790	789	788	787	786	785	784	783	782	781	780	779	778	777	776	775	774	773	772	771	770	769	768	767	766	765	764	763	762	761	760	759	758	757	756	755	754	753	752	751	750	749	748	747	746	745	744	743	742	741	740	739	738	737	736	735	734	733	732	731	730	729	728	727	726	725	724	723	722	721	720	719	718	717	716	715	714	713	712	711	710	709	708	707	706	705	704	703	702	701	700	699	698	697	696	695	694	693	692	691	690	689	688	687	686	685	684	683	682	681	680	679	678	677	676	675	674	673	672	671	670	669	668	667	666	665	664	663	662	661	660	659	658	657	656	655	654	653	652	651	650	649	648	647	646	645	644	643	642	641	640	639	638	637	636	635	634	633	632	631	630	629	628	627	626	625	624	623	622	621	620	619	618	617	616	615	614	613	612	611	610	609	608	607	606	605	604	603	602	601	600	599	598	597	596	595	594	593	592	591	590	589	588	587	586	585	584	583	582	581	580	579	578	577	576	575	574	573	572	571	570	569	568	567	566	565	564	563	562	561	560	559	558	557	556	555	554	553	552	551	550	549	548	547	546	545	544	543	542	541	540	539	538	537	536	535	534	533	532	531	530	529	528	527	526	525	524	523	522	521	520	519	518	517	516	515	514	513	512	511	510	509	508	507	506	505	504	503	502	501	500	499	498	497	496	495	494	493	492	491	490	489	488	487	486	485	484	483	482	481	480	479	478	477	476	475	474	473	472	471	470	469	468	467	466	465	464	463	462	461	460	459	458	457	456	455	454	453	452	451	450	449	448	447	446	445	444	443	442	441	440	439	438	437	436	435	434	433	432	431	430	429	428	427	426	425	424	423	422	421	420	419	418	417	416	415	414	413	412	411	410	409	408	407	406	405	404	403	402	401	400	399	398	397	396	395	394	393	392	391	390	389	388	387	386	385	384	383	382	381	380	379	378	377	376	375	374	373	372	371	370	369	368	367	366	365	364	363	362	361	360	359	358	357	356	355	354	353	352	351	350	349	348	347	346	345	344	343	342	341	340	339	338	337	336	335	334	333	332	331	330	329	328	327	326	325	324	323	322	321	320	319	318	317	316	315	314	313	312	311	310	309	308	307	306	305	304	303	302	301	300	299	298	297	296	295	294	293	292	291	290	289	288	287	286	285	284	283	282	281	280	279	278	277	276	275	274	273	272	271	270	269	268	267	266	265	264	263	262	261	260	259	258	257	256	255	254	253	252	251	250	249	248	247	246	245	244	243	242	241	240	239	238	237	236	235	234	233	232	231	230	229	228	227	226	225	224	223	222	221	220	219	218	217	216	215	214	213	212	211	210	209	208	207	206	205	204	203	202	201	200	199	198	197	196	195	194	193	192	191	190	189	188	187	186	185	184	183	182	181	180	179	178	177	176	175	174	173	172	171	170	169	168	167	166	165	164	163	162	161	160	159	158	157	156	155	154	153	152	151	150	149	148	147	146	145	144	143	142	141	140	139	138	137	136	135	134	133	132	131	130	129	128	127	126	125	124	123	122	121	120	119	118	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
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55	DO 110 I=2,NO	SIGNIR
56	IFIX10(I).GT.X10(INO) INO=I	SIGNIR
57	110 CONTINUE	SIGNIR
58	IMIN=1	SIGNIR
59	DO 120 I=2,N	SIGNIR
60	IFIX2(I).LT.Y2(IMIN) IMIN=I	SIGNIR
61	120 CONTINUE	SIGNIR
62	JJ=0	SIGNIR
63	DO 130 I=1,N	SIGNIR
64	IFIXSURF(I).ME.ISURF(IMIN) GO TO 138	SIGNIR
65	JJ=JJ+1	SIGNIR
66	130 CONTINUE	SIGNIR
67	KUR(JJ)=Y2(I)	SIGNIR
68	Y2(I)=V2(I)	SIGNIR
69	130 CONTINUE	SIGNIR
70	CALL ORDEP (KUR,YU2,JJ)	SIGNIR
71	IFIXYU2(JJ).LE.X10(INO) GO TO 150	SIGNIR
72	XP=YU2(JJ)-X10(INO)	SIGNIR
73	AN=X10(INO)	SIGNIR
74	CALL TABLE(XU2,YU2,X10(INO),RP,OXOY,JJ)	SIGNIR
75	DO 101 I=1,NO	SIGNIR
76	TEMPO(I)=TEMPO(I)-480.0	SIGNIR
77	101 CONTINUE	SIGNIR
78	NTOT1=N*NO	SIGNIR
79	READ(5,1) KXI,KXI	SIGNIR
80	CALL YTPA (YTPLE,KXI)	SIGNIR
81	IFIXK .EQ. 0 GO TO 4	SIGNIR
82	READ(5,1) NMAI	SIGNIR
83	NTOT2=NTOT1+NMAI	SIGNIR
84	IFIXJUCT .NE. 0 NTOT2=NTOT2+1	SIGNIR
85	READ(5,1043) (TM(I),I=1,NTOT2)	SIGNIR
86	FORMAT(6F10.5)	SIGNIR
87	1003	SIGNIR
88	5	SIGNIR
89	FORMAT(1H1,2X,"SYSTEM MODE TEMPERATURES",//)	SIGNIR
90	1013	SIGNIR
91	FORMAT(135X,"MODE NO. ",I2,"/26X,"TEMPERATURE=",F7.2," DEG. R",//)	SIGNIR
92	1014	SIGNIR
93	IFIXPRINT .EQ. 0 GO TO 6	SIGNIR
94	WRITE(6,1013)	SIGNIR
95	1004	SIGNIR
96	DO 211 I=1,NTOT2	SIGNIR
97	IFIXLINECT .LE. 56 GO TO 203	SIGNIR
98	WRITE(6,1013)	SIGNIR
99	1005	SIGNIR
100	203	SIGNIR
101	WRITE(6,1014) I,TM(I)	SIGNIR
102	1006	SIGNIR
103	201	SIGNIR
104	CONTINUE	SIGNIR
105	IFIXKXI.LE.0 GO TO 9	SIGNIR
106	IFIXPRINT6 .EQ. 0 GO TO 60	SIGNIR
107	WRITE(6,1010)	SIGNIR
108	1010	SIGNIR
109	FORMAT(1H1,26X,20HSYSTEM INTERNAL VIEW FACTORS,//)	SIGNIR
110	1007	SIGNIR
111	60	SIGNIR
112	IFIXJUCT .NE. 0 NTOT1=NTOT1+1	SIGNIR
113	DO 733 I=1,NTOT1	SIGNIR
114	READ(5,5) (FI(I),J=I,NTOT1)	SIGNIR
115	733	SIGNIR
116	READ(5,5) AREA(I)	SIGNIR
117	DO 57 I=1,NTOT1	SIGNIR
118	IFIXPRINT6 .EQ. 0 GO TO 53	SIGNIR
119	DO 53 J=I,NTOT1	SIGNIR
120	IFIXLINEV .LT. 56 GO TO 55	SIGNIR
121	WRITE(6,1010)	SIGNIR

115	LINEV=6		SIGNR	116
55	WRITE(6,1011) I,J,F(I,J)		SIGNR	117
1011	FORMAT(3X,'F',I2,'-',J2,'-',F7.9)		SIGNR	118
58	LINEV=LINEV+1		SIGNR	119
59	CONTINUE		SIGNR	120
120	IFERRITE.EQ.0) GO TO 53		SIGNR	121
1012	WRITE(6,1012) I,AREALL		SIGNR	122
	FORMAT(2X,'AREALL',I2,'-',F7.2,' 50. IN.',//)		SIGNR	123
57	LINEV=LINEV+2		SIGNR	124
57	IFERRI.EQ.0) GO TO 57		SIGNR	125
	AREALL=AREALL/144.0		SIGNR	126
57	CONTINUE		SIGNR	127
9	IFERRI.EQ.0) GO TO 10		SIGNR	128
	DO 6 I=1,N		SIGNR	129
	READ(5,2) Y(I)		SIGNR	130
6	READ(5,1) (SURF(I),I=1,I2)		SIGNR	131
	GO TO 11		SIGNR	132
10	CALL OVERLAY(HERF,9,0)		SIGNR	133
C10	CALL REMIN3		SIGNR	134
	NOTE=NOTE+NMAT		SIGNR	135
35	DO 36 I=1,40		SIGNR	136
36	TIMEI=0.0		SIGNR	137
	DO 37 I=1,NMAT		SIGNR	138
	IJ=MOD(I,1)		SIGNR	139
37	TIMEI=TIMEI+I		SIGNR	140
	DO 38 I=1,N		SIGNR	141
	IJ=MOD(I,1)		SIGNR	142
39	TIMEI=TIMEI+I		SIGNR	143
	IF(XC(I)-E0,0) GO TO 11		SIGNR	144
	DO 39 I=1,N		SIGNR	145
	IJ=MOD(I,1)		SIGNR	146
39	TIMEI=TIMEI+I		SIGNR	147
	DO 40 I=1,N		SIGNR	148
	CALL AFRYIX(I,Y1,X2,Y2,XF,M,I,SURF,SURF,XU1,YU1,XU2,YU2,KK,		SIGNR	149
	IKK,1)		SIGNR	150
150			SIGNR	151
	ISUR=JSURF(I,J)		SIGNR	152
	NPISUR=KK		SIGNR	153
	DO 46 J=1,KK		SIGNR	154
46	VF(I,SUR,J)=XU(I,J)		SIGNR	155
	RF(I,SUR,J)=YU(I,J)*0.015		SIGNR	156
47			SIGNR	157
	ISUR=JSURF(I,J)		SIGNR	158
	NPISUR=KK		SIGNR	159
	DO 47 J=1,KK		SIGNR	160
47	VF(I,SUR,J)=XU2(J,J)		SIGNR	161
	RF(I,SUR,J)=YU2(J,J)*0.015		SIGNR	162
	IF(I,PFISUR,KK)=0.0		SIGNR	163
	RF(I,SUR,KK)=0.0		SIGNR	164
	VF(I,SUR,KK)=VF(I,SUR,KK)-0.015		SIGNR	165
165	CONTINUE		SIGNR	166
	NOBS=N+1		SIGNR	167
	ITU=0		SIGNR	168
	DO 42 I=1,NOBS,NTOT1		SIGNR	169
	ITU=ITU+1		SIGNR	170
170	X(I)=X(I+ITU)		SIGNR	171
	Y(I)=Y(I+ITU)		SIGNR	172

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173	X2(I)=X20(I,I)	SIGNIR	173
	V2(I)=V20(I,I)	SIGNIR	174
	VECT(I)=VECT0(I,I)	SIGNIR	175
175	NOJE(I)=NODE0(I,I)	SIGNIR	176
176	IF(KKI.LY.1) GO TO 59	SIGNIR	177
	CALL OVERLAY(SHXRHP,18,0)	SIGNIR	178
	CALL VIEWS	SIGNIR	179
180	IF(IGUCT.NE.0) NTOT2=NTOT2+1	SIGNIR	180
	IF(KKI.NE.0) GO TO 56	SIGNIR	181
	READ(5,1) MCK	SIGNIR	182
	IF(MCK.EQ.0) GO TO 600	SIGNIR	183
	CALL CONDINCK(KKI)	SIGNIR	184
185	600 NTOT3=NTOT1+1	SIGNIR	185
	00 72 I=NTOT3,NTOT2	SIGNIR	186
	AREA(I)=0	SIGNIR	187
	72 EMT(I)=0.0	SIGNIR	188
190	56 READ(5,5)(EMT(I),I=1,NTOT1)	SIGNIR	189
	IF(KKI.EQ.0) GO TO 70	SIGNIR	190
	CALL OVERLAY(SHXRHP,11,0)	SIGNIR	191
	CALL TASI8	SIGNIR	192
	6 70 CALL OVERLAY(SHXRHP,12,0)	SIGNIR	193
	072 CALL TAIL8	SIGNIR	194
	RETURN	SIGNIR	195
195	END	SIGNIR	196

		SUBROUTINE TABLE(X1,X2,X3,DVDT,MT)	
		DIMENSION MT(1), VT(1)	TABLER 2
		IF(MT-2) 300,200,100	TABLER 3
5	100	IF(MT,GT,3) GO TO 150	TABLER 4
		DELSIGN(0,001,MT(1)-X1(1))	TABLER 5
		MT(1)=VT(1)+DEL	TABLER 6
		VT(1)=(VT(1)-VT(2))*VT(1)/(VT(1)-VT(2))+VT(2)	TABLER 7
		I=3	TABLER 8
10	150	IF(DEL,4,300,13)	TABLER 9
		MT=MT-1	TABLER 10
		IF(VT(1),1,MT(1)) GO TO 6	TABLER 11
		DO 12 1,3,MT	TABLER 12
		IF(VT(1)) 12,13,13	TABLER 13
15	12	CONTINUE	TABLER 14
		I=MT	TABLER 15
		I=I-1	TABLER 16
20	13	X0=VT(1+2)	TABLER 17
		Y0=VT(1+7)	TABLER 18
		X1=VT(1+1)	TABLER 19
		Y1=VT(1+6)	TABLER 20
		X2=VT(1)	TABLER 21
		Y2=VT(1)	TABLER 22
		X3=VT(1-1)	TABLER 23
		Y3=VT(1-1)	TABLER 24
25		GO TO 15	TABLER 25
		DO 1 1,3,MT	TABLER 26
		IF(VT(1)) 6,6,1	TABLER 27
		CONTINUE	TABLER 28
		I=MT	TABLER 29
		I=I-1	TABLER 30
		X0=VT(1-1)	TABLER 31
		Y0=VT(1-1)	TABLER 32
		X1=VT(1-1)	TABLER 33
		Y1=VT(1-1)	TABLER 34
		X2=VT(1)	TABLER 35
35		Y2=VT(1)	TABLER 36
		X3=VT(1+1)	TABLER 37
		Y3=VT(1+1)	TABLER 38
		X0=VT(1+2)	TABLER 39
		Y0=VT(1+7)	TABLER 40
40		X1=VT(1+1)	TABLER 41
		Y1=VT(1+6)	TABLER 42
		X2=VT(1)	TABLER 43
		Y2=VT(1)	TABLER 44
		X3=VT(1-1)	TABLER 45
		Y3=VT(1-1)	TABLER 46
		X0=VT(1-1)	TABLER 47
		Y0=VT(1-1)	TABLER 48
		X1=VT(1-1)	TABLER 49
		Y1=VT(1-1)	TABLER 50
		X2=VT(1)	TABLER 51
		Y2=VT(1)	TABLER 52
		X3=VT(1+1)	TABLER 53
		Y3=VT(1+1)	TABLER 54
45		X0=VT(1+2)	TABLER 55
		Y0=VT(1+7)	TABLER 56
		X1=VT(1+1)	TABLER 57
		Y1=VT(1+6)	TABLER 58
		X2=VT(1)	TABLER 59
		Y2=VT(1)	TABLER 60
		X3=VT(1-1)	TABLER 61
		Y3=VT(1-1)	TABLER 62
		X0=VT(1-1)	TABLER 63
		Y0=VT(1-1)	TABLER 64
		X1=VT(1-1)	TABLER 65
		Y1=VT(1-1)	TABLER 66
		X2=VT(1)	TABLER 67
		Y2=VT(1)	TABLER 68
		X3=VT(1+1)	TABLER 69
		Y3=VT(1+1)	TABLER 70
		X0=VT(1+2)	TABLER 71
		Y0=VT(1+7)	TABLER 72
		X1=VT(1+1)	TABLER 73
		Y1=VT(1+6)	TABLER 74
		X2=VT(1)	TABLER 75
		Y2=VT(1)	TABLER 76
		X3=VT(1-1)	TABLER 77
		Y3=VT(1-1)	TABLER 78
		X0=VT(1-1)	TABLER 79
		Y0=VT(1-1)	TABLER 80
		X1=VT(1-1)	TABLER 81
		Y1=VT(1-1)	TABLER 82
		X2=VT(1)	TABLER 83
		Y2=VT(1)	TABLER 84
		X3=VT(1+1)	TABLER 85
		Y3=VT(1+1)	TABLER 86
		X0=VT(1+2)	TABLER 87
		Y0=VT(1+7)	TABLER 88
		X1=VT(1+1)	TABLER 89
		Y1=VT(1+6)	TABLER 90
		X2=VT(1)	TABLER 91
		Y2=VT(1)	TABLER 92
		X3=VT(1-1)	TABLER 93
		Y3=VT(1-1)	TABLER 94
		X0=VT(1-1)	TABLER 95
		Y0=VT(1-1)	TABLER 96
		X1=VT(1-1)	TABLER 97
		Y1=VT(1-1)	TABLER 98
		X2=VT(1)	TABLER 99
		Y2=VT(1)	TABLER 100
		X3=VT(1+1)	TABLER 101
		Y3=VT(1+1)	TABLER 102
		X0=VT(1+2)	TABLER 103
		Y0=VT(1+7)	TABLER 104
		X1=VT(1+1)	TABLER 105
		Y1=VT(1+6)	TABLER 106
		X2=VT(1)	TABLER 107
		Y2=VT(1)	TABLER 108
		X3=VT(1-1)	TABLER 109
		Y3=VT(1-1)	TABLER 110
		X0=VT(1-1)	TABLER 111
		Y0=VT(1-1)	TABLER 112
		X1=VT(1-1)	TABLER 113
		Y1=VT(1-1)	TABLER 114
		X2=VT(1)	TABLER 115
		Y2=VT(1)	TABLER 116
		X3=VT(1+1)	TABLER 117
		Y3=VT(1+1)	TABLER 118
		X0=VT(1+2)	TABLER 119
		Y0=VT(1+7)	TABLER 120
		X1=VT(1+1)	TABLER 121
		Y1=VT(1+6)	TABLER 122
		X2=VT(1)	TABLER 123
		Y2=VT(1)	TABLER 124
		X3=VT(1-1)	TABLER 125
		Y3=VT(1-1)	TABLER 126
		X0=VT(1-1)	TABLER 127
		Y0=VT(1-1)	TABLER 128
		X1=VT(1-1)	TABLER 129
		Y1=VT(1-1)	TABLER 130
		X2=VT(1)	TABLER 131
		Y2=VT(1)	TABLER 132
		X3=VT(1+1)	TABLER 133
		Y3=VT(1+1)	TABLER 134
		X0=VT(1+2)	TABLER 135
		Y0=VT(1+7)	TABLER 136
		X1=VT(1+1)	TABLER 137
		Y1=VT(1+6)	TABLER 138
		X2=VT(1)	TABLER 139
		Y2=VT(1)	TABLER 140
		X3=VT(1-1)	TABLER 141
		Y3=VT(1-1)	TABLER 142
		X0=VT(1-1)	TABLER 143
		Y0=VT(1-1)	TABLER 144
		X1=VT(1-1)	TABLER 145
		Y1=VT(1-1)	TABLER 146
		X2=VT(1)	TABLER 147
		Y2=VT(1)	TABLER 148
		X3=VT(1+1)	TABLER 149
		Y3=VT(1+1)	TABLER 150
		X0=VT(1+2)	TABLER 151
		Y0=VT(1+7)	TABLER 152
		X1=VT(1+1)	TABLER 153
		Y1=VT(1+6)	TABLER 154
		X2=VT(1)	TABLER 155
		Y2=VT(1)	TABLER 156
		X3=VT(1-1)	TABLER 157
		Y3=VT(1-1)	TABLER 158
		X0=VT(1-1)	TABLER 159
		Y0=VT(1-1)	TABLER 160
		X1=VT(1-1)	TABLER 161
		Y1=VT(1-1)	TABLER 162
		X2=VT(1)	TABLER 163
		Y2=VT(1)	TABLER 164
		X3=VT(1+1)	TABLER 165
		Y3=VT(1+1)	TABLER 166
		X0=VT(1+2)	TABLER 167
		Y0=VT(1+7)	TABLER 168
		X1=VT(1+1)	TABLER 169
		Y1=VT(1+6)	TABLER 170
		X2=VT(1)	TABLER 171
		Y2=VT(1)	TABLER 172
		X3=VT(1-1)	TABLER 173
		Y3=VT(1-1)	TABLER 174
		X0=VT(1-1)	TABLER 175
		Y0=VT(1-1)	TABLER 176
		X1=VT(1-1)	TABLER 177
		Y1=VT(1-1)	TABLER 178
		X2=VT(1)	TABLER 179
		Y2=VT(1)	TABLER 180
		X3=VT(1+1)	TABLER 181
		Y3=VT(1+1)	TABLER 182
		X0=VT(1+2)	TABLER 183
		Y0=VT(1+7)	TABLER 184
		X1=VT(1+1)	TABLER 185
		Y1=VT(1+6)	TABLER 186
		X2=VT(1)	TABLER 187
		Y2=VT(1)	TABLER 188
		X3=VT(1-1)	TABLER 189
		Y3=VT(1-1)	TABLER 190
		X0=VT(1-1)	TABLER 191
		Y0=VT(1-1)	TABLER 192
		X1=VT(1-1)	TABLER 193
		Y1=VT(1-1)	TABLER 194
		X2=VT(1)	TABLER 195
		Y2=VT(1)	TABLER 196
		X3=VT(1+1)	TABLER 197
		Y3=VT(1+1)	TABLER 198
		X0=VT(1+2)	TABLER 199
		Y0=VT(1+7)	TABLER 200
		X1=VT(1+1)	TABLER 201
		Y1=VT(1+6)	TABLER 202
		X2=VT(1)	TABLER 203
		Y2=VT(1)	TABLER 204
		X3=VT(1-1)	TABLER 205
		Y3=VT(1-1)	TABLER 206
		X0=VT(1-1)	TABLER 207
		Y0=VT(1-1)	TABLER 208
		X1=VT(1-1)	TABLER 209
		Y1=VT(1-1)	TABLER 210
		X2=VT(1)	TABLER 211
		Y2=VT(1)	TABLER 212
		X3=VT(1+1)	TABLER 213
		Y3=VT(1+1)	TABLER 214
		X0=VT(1+2)	TABLER 215
		Y0=VT(1+7)	TABLER 216
		X1=VT(1+1)	TABLER 217
		Y1=VT(1+6)	TABLER 218
		X2=VT(1)	TABLER 219
		Y2=VT(1)	TABLER 220
		X3=VT(1-1)	TABLER 221
		Y3=VT(1-1)	TABLER 222
		X0=VT(1-1)	TABLER 223
		Y0=VT(1-1)	TABLER 224
		X1=VT(1-1)	TABLER 225
		Y1=VT(1-1)	TABLER 226
		X2=VT(1)	TABLER 227
		Y2=VT(1)	TABLER 228
		X3=VT(1+1)	TABLER 229
		Y3=VT(1+1)	TABLER 230
		X0=VT(1+2)	TABLER 231
		Y0=VT(1+7)	TABLER 232
		X1=VT(1+1)	TABLER 233
		Y1=VT(1+6)	TABLER 234
		X2=VT(1)	TABLER 235
		Y2=VT(1)	TABLER 236
		X3=VT(1-1)	TABLER 237
		Y3=VT(1-1)	TABLER 238
		X0=VT(1-1)	TABLER 239
		Y0=VT(1-1)	TABLER 240
		X1=VT(1-1)	TABLER 241
		Y1=VT(1-1)	TABLER 242
		X2=VT(1)	TABLER 243
		Y2=VT(1)	TABLER 244
		X3=VT(1+1)	TABLER 245
		Y3=VT(1+1)	TABLER 246
		X0=VT(1+2)	TABLER 247
		Y0=VT(1+7)	TABLER 248
		X1=VT(1+1)	TABLER 249
		Y1=VT(1+6)	TABLER 250
		X2=VT(1)	TABLER 251
		Y2=VT(1)	TABLER 252
		X3=VT(1-1)	TABLER 253
		Y3=VT(1-1)	TABLER 254
		X0=VT(1-1)	TABLER 255
		Y0=VT(1-1)	TABLER 256
		X1=VT(1-1)	TABLER 257
		Y1=VT(1-1)	TABLER 258
		X2=VT(1)	TABLER 259
		Y2=VT(1)	TABLER 260
		X3=VT(1+1)	TABLER 261
		Y3=VT(1+1)	TABLER 262
		X0=VT(1+2)	TABLER 263
		Y0=VT(1+7)	TABLER 264
		X1=VT(1+1)	TABLER 265
		Y1=VT(1+6)	TABLER 266
		X2=VT(1)	TABLER 267
		Y2=VT(1)	TABLER 268
		X3=VT(1-1)	TABLER 269
		Y3=VT(1-1)	TABLER 270
		X0=VT(1-1)	TABLER 271
		Y0=VT(1-1)	TABLER 272
		X1=VT(1-1)	TABLER 273
		Y1=VT(1-1)	TABLER 274
		X2=VT(1)	TABLER 275
		Y2=VT(1)	TABLER 276
		X3=VT(1+1)	TABLER 277
		Y3=VT(1+1)	TABLER 278
		X0=VT(1+2)	TABLER 279
		Y0=VT(1+7)	TABLER 280
		X1=VT(1+1)	TABLER 281
		Y1=VT(1+6)	TABLER 282
		X2=VT(1)	TABLER 283
		Y2=VT(1)	TABLER 284
		X3=VT(1-1)	TABLER 285
		Y3=VT(1-1)	TABLER 286
		X0=VT(1-1)	TABLER 287
		Y0=VT(1-1)	TABLER 288
		X1=VT(1-1)	TABLER 289
		Y1=VT(1-1)	TABLER 290
		X2=VT(1)	TABLER 291
		Y2=VT(1)	TABLER 292
		X3=VT(1+1)	TABLER 293
		Y3=VT(1+1)	TABLER 294
		X0=VT(1+2)	TABLER 295
		Y0=VT(1+7)	TABLER 296
		X1=VT(1+1)	TABLER 297
		Y1=VT(1+6)	TABLER 298
		X2=VT(1)	TABLER 299
		Y2=VT(1)	TABLER 300
		X3=VT(1-1)	TABLER 301
		Y3=VT(1-1)	TABLER 302
		X0=VT(1-1)	TABLER 303
		Y0=VT(1-1)	TABLER 304
		X1=VT(1-1)	TABLER 305
		Y1=VT(1-1)	TABLER 306
		X2=VT(1)	TABLER 307
		Y2=VT(1)	TABLER 308
		X3=VT(1+1)	TABLER 309
		Y3=VT(1+1)	TABLER 310
		X0=VT(1+2)	TABLER 311
		Y0=VT(1+7)	TABLER 312
		X1=VT(1+1)	TABLER 313
		Y1=VT(1+6)	TABLER 314
		X2=VT(1)	TABLER 315
		Y2=VT(1)	TABLER 316
		X3=VT(1-1)	TABLER 317
		Y3=VT(1-1)	TABLER 318
		X0=VT(1-1)	TABLER 319
		Y0=VT(1-1)	TABLER 320
		X1=VT(1-1)	TABLER 321
		Y1=VT(1-1)	TABLER 322
		X2=VT(1)	TABLER 323
		Y2=VT(1)	TABLER 324
		X3=VT(1+1)	TABLER 325
		Y3=VT(1+1)	TABLER 326
		X0=VT(1+2)	TABLER 327
		Y0=VT(1+7)	TABLER 328
		X1=VT(1+1)	TABLER 329
		Y1=VT(1+6)	TABLER 330
		X2=VT(1)	TABLER 331
		Y2=VT(1)	TABLER 332
		X3=VT(1-1)	TABLER 333
		Y3=VT(1-1)	TABLER 334
		X	

300 WRITE(6,310)
310 FORMAT(10INSUFFICIENT TABLE SIZE --- TABLE#)
STOP
END

TABLE 59
TABLE 60
TABLE 61
TABLE 62

		SUBROUTINE ARRAT(X1,Y1,Z1,X2,Y2,Z2,XF,N1,ISURF,JSURF,XU1,YU1,XU2,YU2, KK,KX,KJ)	ARRAT	2
		DIMENSION X1(1),X2(1),Y1(1),Y2(1),Z1(1),Z2(1),ISURF(1),JSURF(15,2),XF(1), OIMENSION KX(120),KX2(20),YU1(20),YU2(20),XU1(1),YU1(1),XU2(1), YU2(1)	ARRAT	4
5	1	DO 20 I=1,2	ARRAT	5
		KU1=1	ARRAT	6
		JJ=0	ARRAT	7
		DO 6 J=1,N	ARRAT	8
10	5	IF(JSURF(I,11)-ISURF(J)) 6,5,6	ARRAT	9
		JJ=JJ+1	ARRAT	10
		X1(JJ)=X1(J)	ARRAT	11
		X2(JJ)=X2(J)	ARRAT	12
		Y1(JJ)=Y1(J)	ARRAT	13
15	6	Y2(JJ)=Y2(J)	ARRAT	14
		CONTINUE	ARRAT	15
		IF(JJ,1,2) GO TO 3	ARRAT	16
		CALL ODERAT(X1,Y1,Z1)	ARRAT	17
		CALL ODERAT(X2,Y2,Z2)	ARRAT	18
20	3	IF(I=1,1) GO TO 10	ARRAT	19
		GO 2,3,1,1,1	ARRAT	20
		IF(X1,1,GT,XF) KU1=1	ARRAT	21
		XU1(J)=XU1(J)	ARRAT	22
25	2	IF(XU1,GT,0) GO TO 14	ARRAT	23
		CONTINUE	ARRAT	24
		KX=J+1	ARRAT	25
		KU1(KX)=XU2(JJ)	ARRAT	26
		YU1(KX)=YU2(JJ)	ARRAT	27
		GO TO 20	ARRAT	28
30	13	DO 13 J=1,25	ARRAT	29
		IF(X1,NE,0) GO TO 25	ARRAT	30
		IF(X1,1,GT,XF) KU1=1	ARRAT	31
35	25	XU2(J)=XU1(J)	ARRAT	32
		YU2(J)=YU1(J)	ARRAT	33
		IF(KU1,GT,0) GO TO 15	ARRAT	34
		CONTINUE	ARRAT	35
		KX=J+1	ARRAT	36
40	13	KU2(KX)=XU2(JJ)	ARRAT	37
		YU2(KX)=YU2(JJ)	ARRAT	38
		GO TO 20	ARRAT	39
		KX=J	ARRAT	40
		GO TO 23	ARRAT	41
45	15	KK=J	ARRAT	42
		CONTINUE	ARRAT	43
		RETURN	ARRAT	44
		END	ARRAT	45

A-38

	SUBROUTINE ORDER(X,Y,NUM)				2
	DIMENSION X(1),Y(1)				3
	K=NUM-1				4
	DO 10 I=1,K				5
5	M=NUM-I				6
	DO 10 J=1,M				7
	IF(X(J)-X(J+1)) 10,10,5				8
	TEMP=X(J)				9
	TEMPY=Y(J)				10
10	X(J)=X(J+1)				11
	Y(J)=Y(J+1)				12
	X(J+1)=TEMP				13
	Y(J+1)=TEMPY				14
	CONTINUE				15
15	RETURN				16
	END				17

```

SUBROUTINE COMDEN,KCTB
COMMON /ITPACK/ INT(63),INTARY(40),INTS
COMMON /TMY/CT(60),NTOT2
DO 11 I=1,N
  INTS=INTS+1
  READ(5,2) N,DEANODE2,MYARY(INTS)
  INIT(1:NTOT2)=MODEL+100*NODE2
  FORMAT(2X,2I2,4X,F10.5)
  IF(IK1.GT.8) GO TO 20
  READ(5,2) MY
  IF(MY.EQ.0) GO TO 20
  NTOT2=NTOT2+1
  DO 15 I=1,N
    READ(5,4) MODEL,I
    CT(NODE1)=I*ED.
    FORMAT(2X,12,5),F10.5)
    RETURN
  END

```

```

COND 2
COND 3
COND 4
COND 5
COND 6
COND 7
COND 8
COND 9
COND 10
COND 11
COND 12
COND 13
COND 14
COND 15
COND 16
COND 17
COND 18
COND 19

```

```

SUBROUTINE TITLA (TITL,KKI)
COMMON /PRINT/ PRINT1, PRINT2, PRINT3, PRINT4, PRINT5,
PRINT6, PRINT7, PRINT8, PRINT9, PRINT0
DIMENSION TITL(5,6)
INTEGER PRINT1,PRINT2,PRINT3,PRINT4,PRINT5,PRINT6,PRINT7,PRINT8,
PRINT9
WRITE(6,1)
FORMAT(1M5,//////,8X,63(JH*),/8X,1M*,61X,1M*,/8X,1M*,13X,"A I
R C R A F Y S I G N A T U R E",13X,1M*,/8X,1M*,61X,
21M*,/8X,1M*,13X,"P K F I C T I O N P R O C R A M",13X,1M*,/8X,
14M*,61X,1M*,/8X,63(JH*),//////,31X,"TITLE INFORMATION",/)
DO 2 J=1,5
2 WRITE(6,3) (TITL(J,J),J=1,6)
3 FORMAT(1CX,6A1)
WRITE(6,4)
4 FORMAT(//////,16X,"THESE RESULTS CONTAIN THE FOLLOWING INFORMATION",/)
11ON,"")
NC=0
IF(KKI.EQ.1) GO TO 14
IF(PRINT1.EQ.0) GO TO 10
NO=NO+1
WRITE(6,30) NO
30 FORMAT(17X,12,"", COMPOUND COMPRESSIBLE FLOW INFORMATION,"")
18 IF(PRINT2.EQ.0) GO TO 11
NO=NO+1
WRITE(6,31) NO
31 FORMAT(17X,12,"", SURFACE HEAT TRANSFER INFORMATION,"")
11 IF(PRINT3.EQ.0) GO TO 12
NO=NO+1
WRITE(6,32) NO
32 FORMAT(17X,12,"", AVERAGE SURFACE HEAT TRANSFER COEFFICIENTS,"")
12 IF(PRINT4.EQ.0) GO TO 13
NO=NO+1
WRITE(6,33) NO
33 FORMAT(17X,12,"", AVERAGE SYSTEM GAS TEMPERATURES,"")
13 IF(PRINT5.EQ.0) GO TO 14
NO=NO+1
WRITE(6,34) NO
34 FORMAT(17X,12,"", SURFACE COOLING INFORMATION,"")
41 IF(PRINT6.EQ.0) GO TO 14
NO=NO+1
WRITE(6,40) NO
40 FORMAT(17X,12,"", SYSTEM SURFACE FORCE FACTOR CALCULATIONS,"")
14 IF(PRINT6.EQ.0) GO TO 15
NO=NO+1
WRITE(6,35) NO
35 FORMAT(17X,12,"", SYSTEM INTERNAL VIEW FACTORS,"")
15 IF(PRINT7.EQ.0) GO TO 16
NO=NO+1
WRITE(6,36) NO
36 FORMAT(17X,12,"", SYSTEM WALL TEMPERATURES,"")
16 IF(PRINT8.EQ.0) GO TO 17
NO=NO+1
WRITE(6,37) NO
37 FORMAT(17X,12,"", SYSTEM EXTERNAL VIEW FACTORS,"")
17 NO=NO+1
WRITE(6,38) NO

```

38	FORMAT(17X,12,". SYSTEM RADIATION PATTERNS.")	TITLE	59
	NO-NO+1	TITLE	60
68	WRITE(6,39) NO	TITLE	61
	FORMAT(17X,12,". SYSTEM RADIATION LEVEL BANDWIDTHS.")	TITLE	62
39	RETURN	TITLE	63
	END	TITLE	64

LINE	CODE	DATA	INPUTS
2		OVERLAY/IMP,1,81	INPUTS
3		PROGRAM INPUT	INPUTS
4			INPUTS
5			INPUTS
6	C	IMP	INPUTS
7		COMMON/IMP/ D,00Z,0X,0TST,0Z,MANGSEG,MEXIT, RAYPNT, ZTST	INPUTS
8			INPUTS
9		COMMON /GE0/	INPUTS
10		1 A, B8, DDS, MEN, MP,	INPUTS
11		2 R, R80, REM(10), RF, RO, YANA,	INPUTS
12		3 RZ, RP, SC, SS, KO,	INPUTS
13		4 TMB, XC, REM(10), RF, KO,	INPUTS
14		5 X2, REND	INPUTS
15		COMMON/PLM/PLMGO(13),RCH,ST(50),NR0(50),PLMIS,20,50,NFLM,PA,PA,	INPUTS
16		1 D0Y,KDATA,ISHK,JSNK,TANE,EQR	INPUTS
17		DIMENSION YV(10)	INPUTS
18		EQUIVALENCE (NOFLON,NFLW), (XY(1),ST(1))	INPUTS
19			INPUTS
20		COMMON /0BST/ HL(10), HU(10),	INPUTS
21		1 NR5,EXTN(15),AMS(5),AME(5)	INPUTS
22		2, NO, KO	INPUTS
23		1 XI(5),KE(5),DI(5),DE(5),VI(5),WE(5)	INPUTS
24		DIMENSION XENKEN(4),XPR(4)	INPUTS
25		DIMENSION NU(30),JMU(30)	INPUTS
26		REAL NUINC	INPUTS
27		COMMON/CHUCK/NT,NA,MREQ,NU,MJFRST,MUINC,DMU	INPUTS
28		COMMON/STAN/ALTJBS(5),ALTPCN,RANGE(5),IATMO,TBB,CSOI(4),TBACK	INPUTS
29		COMMON/ATMC/NATMG,NRANG,ASDEG	INPUTS
30		COMMON/HALT/ITYPE,ITAU,IL,DZZ,A88,CSS(4)	INPUTS
31		COMMON/SPATIAL/ISPAI	INPUTS
32		COMMON/EXTMS/ZEANE(20),ETEMP(20),NEXT,XCC,SEXT(5,1)	INPUTS
33		COMMON/FILT/IFILTER,BFILTR(30)	INPUTS
34		COMMON /CUT/ ATX(20), AAR(20), MANG, INOT	INPUTS
35		COMMON /EXIT/ EXIT(5)	INPUTS
36		COMMON /ICHEX/ ICHECK	INPUTS
37		COMMON/GAS/IRACK	INPUTS
38		DIMENSION AB(5),AC(5)	INPUTS
39		LOGICAL TERN	INPUTS
40		DATA AB/1,9,3,75,3,6,2,6,2,5/	INPUTS
41		DATA AC/4,1,4,85,5,6,4,8,4,7/	INPUTS
42		NAMELIST/CASE/	INPUTS
43		1 ABB, AL, ALT09S, ALTPLM, AMF, ANI,	INPUTS
44		2 ASPDEG, DDS, EAREA, ETEMP, IFILTER, IL,	INPUTS
45		3 IRACK, ISPAT, ITAU, KDATA, MA,	INPUTS
46		4 MANGSEG, NATMO, MEXIT, MPLM, MP,	INPUTS
47		5 NRANG, NUINC, RANGE, RAYPNT, TBACK, TBB,	INPUTS
48		6 TERM, MJFRST, RPN, RTE, ANL, RSM, XP, RP	INPUTS
49			INPUTS
50		C ASPDEG ASPECT ANGLE IN DEGREES	INPUTS
51		C AL AXIAL CALCULATION LIMIT FT	INPUTS
52		C AMF BAND FINISH MICRONS	INPUTS
53		C ANI BAND INCEPTION MICRONS	INPUTS
54		C DDS NUMBER OF RAY SEGMENTS	INPUTS
55		C RPN RADIUS OF THE PRIMARY NOZZLE,	INPUTS
56		C RTE RADIUS AT THE TURBINE EXIT,	INPUTS
57		C ANL AXIAL NOZZLE LENGTH,	INPUTS
58		C RSM RADIUS OF THE SECONDARY NOZZLE,	INPUTS
59		C XP EXTENSION LENGTH OF THE NOZZLE PLUG BEYOND THE NOZZLE PLANE.	INPUTS

Line	Code	Description	Input	Output
68	C	RP PLUME PRINT OPTION	INPUT 59	
	C	RAYPRT PRINT GAS PARAMETERS ALONG RAY	INPUT 60	
	C	MA NUMBER OF ATMOSPHERIC SEGMENTS IN RAY	INPUT 61	
	C	NUING STEP SIZE OF RADIATION CALCULATIONS, CM-1	INPUT 62	
	C	ALLOSIAL ALTITUDE OF SENSOR FT	INPUT 63	
65	C	ALTPLM ALTITUDE OF VEHICLE FT	INPUT 64	
	C	RANGCIN RANGE FOR EACH SENSOR ALTITUDE FT	INPUT 65	
	C	TSRGN BLACK BODY TEMP DEG K	INPUT 66	
	C	TBACK BACKGROUND TEMP DEG K	INPUT 67	
	C	MAIHO ATMOSPHERIC TYPE	INPUT 68	
	C	NRANG NUMBER OF RANGES	INPUT 69	
70	C	IL SPECIAL PRINT OPTION FOR EACH RAY	INPUT 70	
	C	AC3(R) SPECIAL PRINT OPTION FOR EACH RAY	INPUT 71	
	C	TYPE AGEN OF BLACK BODY RADIATOR SQ CM	INPUT 72	
	C	ITAU SPECTRAL PRINT OF TOTAL PLUME	INPUT 73	
	C		INPUT 74	
	C		INPUT 75	
	C		INPUT 76	
75		IF(ISO)01,EO,01,ICHECKED	INPUT 77	
		IF(ISO)01,EO,01,ANL=RSN=J.	INPUT 78	
		XENREN(1)=XEN(1)	INPUT 79	
		XENREN(2)=XEN(2)	INPUT 80	
		XENREN(3)=XEN(3)	INPUT 81	
		XENREN(4)=XEN(4)	INPUT 82	
		XENREN(5)=XEN(5)	INPUT 83	
		XENREN(6)=XEN(6)	INPUT 84	
		ANL=ANSL(1)	INPUT 85	
		ANL=ANSL(2)	INPUT 86	
		TERE=FA*SE	INPUT 87	
		AL=1300.	INPUT 88	
		IF(ISO)01,EO,01,GO TO 278	INPUT 89	
		RSN=EXIT(1)	INPUT 90	
		RPN=EXIT(2)	INPUT 91	
		R=EXIT(3)	INPUT 92	
		XP=EXIT(4)	INPUT 93	
		ANL=EXIT(5)	INPUT 94	
		RPN=EXIT(6)	INPUT 95	
		READIS,CASE)	INPUT 96	
95		IF(ISO)01,EO,01,WRITE(6,CASE)	INPUT 97	
		IF(ISO)01,EO,01,GO TO 691	INPUT 98	
		ICHECK=ICHECK+1	INPUT 99	
		IF(ISO)01,EO,01,GO TO 3788	INPUT 100	
		ASB=AY(1)ICHECK	INPUT 101	
		TBS=ATX(1)ICHECK	INPUT 102	
		ASPDIC=ASB(1)ICHECK	INPUT 103	
		691 CONTINUE	INPUT 104	
		IF(ITER) GO TO 3788	INPUT 105	
		AMSL(2)=AL	INPUT 106	
		IF(ISO)01,EO,01,GO TO 801	INPUT 107	
		IF(ISO)01,EO,01,GO TO 691	INPUT 108	
		XENREN(1)=ANL/12.0	INPUT 109	
		XENREN(2)=RTE/12.0	INPUT 110	
		XENREN(3)=C.	INPUT 111	
		XENREN(4)=SPN/12.0	INPUT 112	
		XENREN(5)=C.	INPUT 113	
		IF(ISO)01,EO,01,RSN=RPN	INPUT 114	
		XENREN(6)=PSN/12.0	INPUT 115	
		XP=XP/12.0	INPUT 116	

115	RP=RP/12.0	INPUTS	116
	690 CONTINUE	INPUTS	117
	IF(FILTER.LE.0) GO TO 808	INPUTS	118
	AMF=AB(FILTER)	INPUTS	119
	AMF=AC(FILTER)	INPUTS	120
	CONTINUE	INPUTS	121
122	IF(1SPAT.GT.0) WRITE (8) NRANG	INPUTS	122
	IF(1SPAT.GT.0) WRITE (8) (NRANGE(I),I=1,NRANGE)	INPUTS	123
	DO 131 I=1,NRANG	INPUTS	124
	ALTOSS(I)=ALTOSS(I)*30.48	INPUTS	125
125	RANGE(I)=RANGE(I)*30.48	INPUTS	126
	PLMG(I)=ALIELM	INPUTS	127
	ALPLM=ALPLM+30.48	INPUTS	128
	IF(1PAQCK.GT.0) GO TO 802	INPUTS	129
	CONTINUE	INPUTS	130
130	WRITE (6,5000)	INPUTS	131
	A9=ASPOEG	INPUTS	132
	IF(8CFLOW.EQ.1) GO TO 802	INPUTS	133
	C	INPUTS	134
	C	INPUTS	135
135	NEN=2	INPUTS	136
	M=2*NEN+2	INPUTS	137
	DO 210 I=1,M+2	INPUTS	138
	J = (I+1) / 2	INPUTS	139
	XEN(J) = XENREN(I)	INPUTS	140
140	200 REN(I) = XENREN(I+1)	INPUTS	141
	210 CONTINUE	INPUTS	142
	595 WRITE (6, 2002) (XEN(I), REN(I), I=1,NEN)	INPUTS	143
	IF(1P.LE.0.1) GO TO 195	INPUTS	144
	XF=XP	INPUTS	145
145	RF=RP	INPUTS	146
	TANP=RF/XF	INPUTS	147
	WRITE (6,2001) XP,RP	INPUTS	148
149	CONTINUE	INPUTS	149
	88=REN(NEN)	INPUTS	150
150	88=2.*R8	INPUTS	151
	CONTINUE	INPUTS	152
152	WRITE (6,2600)	INPUTS	153
	IF(8FLOW.EQ.1) GO TO 808	INPUTS	154
	AMS(1)=AMI	INPUTS	155
155	AME(1)=AMF	INPUTS	156
	WRITE (6,2800) AMS(1),AME(1),ASPOES	INPUTS	157
	C	INPUTS	158
	C	INPUTS	159
	GO TO 3800	INPUTS	160
160	3788 STOP	INPUTS	161
	C	INPUTS	162
	C	INPUTS	163
	2881 FORMAT(1X,18H** PLUG DEFINITION//	INPUTS	164
	12X,30HAXIAL	INPUTS	165
165	25(5X,2F20.4//)	INPUTS	166
	2882 FORMAT(1X, 20H** ENGINE DEFINITION//	INPUTS	167
	120X,16HAXIAL	INPUTS	168
	210(51,2F20.4//)	INPUTS	169
	2888 FORMAT(2X,18H** CASE DEFINITION//	INPUTS	170
170	1)	INPUTS	171
	2889 FORMAT(2X,10HNAVELENGTH,2F15.4,8H MICRONS/	INPUTS	172

22X, 10KASP ANGLE °15.4, 2X, 7H0EGREES)
 5800 FORMAT (M1, 25X, 21N° ° ° ° ° A S D I R ° ° ° //
 129X, 14H, PLUME ANALYSIS//
 3800 CONTINUE
 NJ

INPUTS 173
 INPUT 1 174
 INPUTS 175
 INPUT 1 176
 INPUTS 177

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OVERLAY (XHP,2,81)
PROGRAM ALPLUM
COMMON/LINK2/ AL,MO,NO2

5 * GEO
COMMON /GEO/
1 AL,
2 RA,
3 ROZ,
4 TMB,
5 XP,
6 TAB

ALPLUM$ 2
ALPLUM$ 3
ALPLUM$ 4
ALPLUM$ 5
ALPLUM$ 6
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ALPLUM$ 57
ALPLUM$ 58

10 * TAB
REIL NU
DIMENSION NUT(300),OHU(300)
DIRECTION NEA(3)
COMMON/CHUCK/NE,NA,NFREQ,NU,NUFREQ,NUINC,OMU
COMMON/LOS/DY(50),XY(50),PI(50),P2(50),PJ(50)
COMMON/OBST/XTRA(20),MRC,XTRA(15),AMI(5),AME(5),YTRA(2)
COMMON/MALY/ITYPE,ITAU,IL,DA,ABUS)
COMMON/STAN/ALTOBS(5),ALTPM,XRANGE(5),TATMO,TBB(5),TBACK
COMMON/ATMG/ATMG,NRANG,ASPOEG
COMMON/BETAK1/COEF(7,070)
COMMON/BETAK/ARK(2030)
COMMON/SSIG/SPSIG(1,5,300)
COMMON/SPATIAL/ISPAI
COMMON/SIG/SGAS(5,1),SMTL(5,1),SBER(5,1)
COMMON/EXTENS/EXTEN(20),ETEMP(20),NEXT,VCC,SEXT(5,1)
COMMON/FILSIG/FHP(5),FAMP(5),FGAS(5),FBG(5),FEXT(5)
COMMON/FILTR/IFILTER,8FILTR(300)
COMMON/GAS/IRADCK

30 * RAY
COMMON/RAY/
1 AOS, ATST, AQA, DO, OS, LI
* IMP
COMMON /IMP/
1 D, OZ, OX, OTST, OZ, NOZ, MOP, MPRINT, ZTST
DATA MEA/3HORY,HNOR,3HWEI/
MNO=0
ASPOFG=AB
DO 51 I=1,5
DO 51 J=1,300
SPSIG(I,I,J)=0.
SGAS(I,I)=0.
SMTL(I,I)=0.
FHP(I)=0.
FAMP(I)=0.
FGAS(I)=0.
FBG(I)=0.
FEXT(I)=0.
SEXT(I,I)=0.
SMTL(I,I)=0.
FHP(I,I)=0.
IF(IRADCK,LE,0) GO TO 451
CALL FLUEAY
IF(IRADCK,EQ,2) XCC=1
CALL PLUSIG
GO TO 150
151 CONTINUE

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	C	TEND=	ALPLUMS	59
68	C	RETURN FOR NEW DZ PLANE	ALPLUMS	60
	C	INITIALIZE FOR COMPONENT CALCULATIONS	ALPLUMS	61
268	C	CALL RAYCAL(IEND)	ALPLUMS	62
		IF(IEND.EQ.1000) GO TO 638	ALPLUMS	63
		DOS=ADS	ALPLUMS	64
65		RPZ=RE**2-.07**2	ALPLUMS	65
		IF(RPZ.LT.0.) RPZ=0.	ALPLUMS	66
		RPZ=SQRT(RPZ)	ALPLUMS	67
298		87=83**2-12**2	ALPLUMS	68
		Y(187,17,0.) 87*0.	ALPLUMS	69
70		Y(187,17,0.) 87*0.	ALPLUMS	70
265		82=57*1321	ALPLUMS	71
		82=32/2.	ALPLUMS	72
	C	ESTABLISH STARTING VALUES	ALPLUMS	73
75	C	Y(1A,50,0.) 08.A0.E0.100.1 GO TO 360	ALPLUMS	74
		Y(1A,50,0.) 08.1 GO TO 361	ALPLUMS	75
		Y(1A,50,0.) 08.1 GO TO 361	ALPLUMS	76
		Y(1C,17,X) GO TO 365	ALPLUMS	77
		Y(1A,50,0.) ADS=ADS/2.	ALPLUMS	78
		GO TO 360	ALPLUMS	79
80	361	DOCK=ARSLXC *TANA)	ALPLUMS	80
		Y(0,17,0CM) GO TO 360	ALPLUMS	81
		Y(1A,50,0.) ADS=ADS/2.	ALPLUMS	82
	C	DOS=ADS	ALPLUMS	83
85		CALL PLURAY	ALPLUMS	84
		AD=1.	ALPLUMS	85
		NEEDS	ALPLUMS	86
		IF(11.EQ.0) AG=0.	ALPLUMS	87
98		DA=40A*AG	ALPLUMS	88
		Y(1C,17,X) GO TO 612	ALPLUMS	89
		XCC=0.	ALPLUMS	90
		IATMO=0	ALPLUMS	91
		Y(1DZ,EO,0.) AND,0.E0.0.1 IATMO=1	ALPLUMS	92
		WIND=NTMO*1	ALPLUMS	93
95		IF(NTMO.E0.1) XCC=1.	ALPLUMS	94
		IF(NEXT.E0.0) XCC=3.	ALPLUMS	95
		CALL PLUSIG	ALPLUMS	96
		AD=1	ALPLUMS	97
612		GO TO 263	ALPLUMS	98
100	638	CONTINUE	ALPLUMS	99
		DO 102 J=1,NRG	ALPLUMS	100
		DO 102 I=1,NRANG	ALPLUMS	101
		RANGE=XRANGE(I)/1.0E+5	ALPLUMS	102
		ALT=ALTRM/1.0E+5	ALPLUMS	103
105		ALCAL103=1/1.2E+5	ALPLUMS	104
		WRITE(6,101) A(I,J),AME(J),RANGE,ASPROG,NEATMO	ALPLUMS	105
		WRITE(6,107) ALT,ALO	ALPLUMS	106
		IF(1A0,LT.0) GO TO 100	ALPLUMS	107
		WRITE(6,103)	ALPLUMS	108
110		DO 104 I=1,NFREQ	ALPLUMS	109
		K=REFR01-1	ALPLUMS	110
		SNJ=NRJ	ALPLUMS	111
		DSIJ=DI1KX	ALPLUMS	112
		Y(1,1,0) 17*0	ALPLUMS	113
		ALPLUMS	ALPLUMS	114
		ALPLUMS	ALPLUMS	115

115	KW=1.E4/(SNU*1)	ALPLUMS	116
	KW=(XNL-XNM)*DSNU	ALPLUMS	117
104	RML=SPSIG(I,I,K)*SNU*SNU*1.E-4/DMU(K)	ALPLUMS	118
101	WRITE(6,105) XNL,XNM,SPSIG(I,I,K),SNU,DSNU,RML	ALPLUMS	119
	SNU=SANTL(I,I)*SGAS(I,I)*SBOG(I,I)	ALPLUMS	120
120	SNU=SNU*SEVI(I,I)	ALPLUMS	121
	WRITE(6,106) AB(I,I),TBB(I,I),TBACK,SNU,SANTL(I,I),SNTL(I,I)	ALPLUMS	122
	1SGAS(I,I)*SGR(I,I)	ALPLUMS	123
	IF(NEXT.NE.0) WRITE(6,108) SENT(I,I)	ALPLUMS	124
125	IF(FILTER.EQ.0) GO TO 182	ALPLUMS	125
	WRITE(6,109) IFILTER	ALPLUMS	126
	IF(IIAU.II.0) GO TO 182	ALPLUMS	127
	WRITE(6,103)	ALPLUMS	128
	DO 401 II=1,NFREQ	ALPLUMS	129
	K=MPRF01-II	ALPLUMS	130
130	SNU=NU(K)	ALPLUMS	131
	OSAU=OSU(K)	ALPLUMS	132
	XNL=1.E+4/SNU	ALPLUMS	133
	SS=SPSIG(I,I,K)*TBFILTR(K)	ALPLUMS	134
135	XNM=1.E+4/(SNU*1)	ALPLUMS	135
	XNM=(XNL-XNM)*DSNU	ALPLUMS	136
401	RML=SPSIG(I,I,K)*SNU*SNU*1.E-4*BFILTR(K)/DMU(K)	ALPLUMS	137
402	WRITE(6,105) XNL,XNM,SS,SNU,DSNU,RML	ALPLUMS	138
	SNU=FAMP(II)*SGAS(II)*FEG(II)*FEXT(II)	ALPLUMS	139
140	WRITE(6,106) AB(I,I),TBB(I,I),TBACK,SNU,FAMP(II),FEG(II),FEXT(II)	ALPLUMS	140
	IF(NEXT.NE.0) WRITE(6,108) FEXT(II)	ALPLUMS	141
102	CONTINUE	ALPLUMS	142
101	FORMAT(1H0,1H//6X,3H***,1H TOTAL SIGNATURE OVER THE SPECTRAL BAND *	ALPLUMS	143
	*F6.2,1H TO *F6.2,1H MICRONS AT A RANGE OF *F10.3,1H KM/6X,1H FOR AN	ALPLUMS	144
145	*ASPECT ANGLE OF *F5.1,1H DEGREES IN A *F4,1H ATMOSPHERE *3H***1H0	ALPLUMS	145
	*)	ALPLUMS	146
103	FORMAT(1H0,9X,1H BAND CENTER BAND WIDTH APPARENT RADIANCE WAVEN	ALPLUMS	147
	UMBER INCREMENT SPECTRAL RADIANCE/12X,1H MICRONS MICRONS	ALPLUMS	148
105	* WATTS/STERADIAN (CENTER)CH-1 CH-1 WATTS/MICRON/SR*/1	ALPLUMS	149
106	FORMAT(12X,F6.4,7X,F6.4,7X,F12.4,5X,F10.2,5X,F5.1,5X,F12.4)	ALPLUMS	150
	CT20*EFFECTIVE BLACK BODY AREA - AB9 = *F10.4,1H CMSQ*/	ALPLUMS	151
	CT20*EFFECTIVE 38 TEMPERATURE - T89 = *F10.4,1H DEGR*/	ALPLUMS	152
	CT20*EFFECTIVE BACKGROUND TEMP.-T8CK = *F10.4,1H DEGR*/	ALPLUMS	153
155	CT20*APPARENT RADIANCE = *F10.4,1H WATTS/STERADIAN*/	ALPLUMS	154
	CT20*ATTENUATED METALS = *F10.4,1H WATTS/STERADIAN*/	ALPLUMS	155
	CT20*ETALS = *F10.4,1H WATTS/STERADIAN*/	ALPLUMS	156
	CT20*PLUME GAS SPECIES = *F10.4,1H WATTS/STERADIAN*/	ALPLUMS	157
	CT20*BACKGROUND = *F10.4,1H WATTS/STERADIAN*/	ALPLUMS	158
107	FORMAT(6X,1H,*VEHICLE ALTITUDE = *F6.2,1H KM AND OBSERVER ALTITUDE	ALPLUMS	159
	1E = *F6.2,1H KM*)	ALPLUMS	160
108	FORMAT(19X,*EXTERNAL EMISSIONS = *F10.4,1H	ALPLUMS	161
109	FORMAT(1H0,1H//6X,3H***,1H TOTAL FILTERED SIGNATURE FOR FILTER 0 *	ALPLUMS	162
150	CONTINUE	ALPLUMS	163
	END	ALPLUMS	164
		ALPLUMS	165

[illegible]

		GO TO 8	RAYCAL 59
	7	RDJ(KI)=RDD(KI)=8.	RAYCAL 60
	8	CONTINUE	RAYCAL 61
60		D=D+DEL	RAYCAL 62
		IF(A3S(DI).LT.1.E-10) D=8.0	RAYCAL 63
	1	CONTINUE	RAYCAL 64
		GO TO 15	RAYCAL 65
65	14	G=REPJT	RAYCAL 66
		DELR=0.	RAYCAL 67
		N9=0	RAYCAL 68
		GO TO 16	RAYCAL 69
70	15	N9=NEXIT	RAYCAL 70
	16	CONTINUE	RAYCAL 71
		IF(A3OFI.EQ.0) GO TO 3	RAYCAL 72
		D=D-(DELR-DR8)/2.	RAYCAL 73
		DO 2 I=1,NCOR	RAYCAL 74
		R8=GAMB*ORAD/80	RAYCAL 75
75		R1=D+DR8/2.+RCOR	RAYCAL 76
		R2=D-DR8/2.+RCOR	RAYCAL 77
		AREA=PIE*P9*RI**2-R2**2)/360.	RAYCAL 78
		DO 9 J=1,NESEG	RAYCAL 79
		K=X+1	RAYCAL 80
80		XY=2.	RAYCAL 81
		THETA=J	RAYCAL 82
		THETA=(THETA-1.1*PI)/ORAD	RAYCAL 83
		RDJ(KI)=(10*FCOR)*SIN(THETA)	RAYCAL 84
		RDJ(KI)=(10*RCOR)*COS(THETA)-(RCOR)*TAN8	RAYCAL 85
85	9	IF(IJ.EQ.1) XY=1.	RAYCAL 86
		RA(KI)=AREA*XY*TAN8+COST	RAYCAL 87
		D=D+DR8	RAYCAL 88
	2	CONTINUE	RAYCAL 89
		DY2=0.	RAYCAL 90
90		D=D-DR8/2.	RAYCAL 91
		GO TO 4	RAYCAL 92
	3	D=D-DELR/2.	RAYCAL 93
	4	NTMO=NEXIT	RAYCAL 94
		DIV=NTMO	RAYCAL 95
95		R8=GAMB*OFAD/80	RAYCAL 96
		DAL=DAL/2IV	RAYCAL 97
		DELR=RCOR+722	RAYCAL 98
		DELR=DELR	RAYCAL 99
		DYL=DAL	RAYCAL 100
100		DAL=J.	RAYCAL 101
		DO 111 I=1,NTMO	RAYCAL 102
		DAL=DAL+DYL	RAYCAL 103
		R1=DAL+DEL	RAYCAL 104
		R2=DELF	RAYCAL 105
105		DELTA=(R1-P2)/2.	RAYCAL 106
		AREA=PIE*(PI**2-R2**2)*R8/360.	RAYCAL 107
		DELR=P1	RAYCAL 108
		O=Q2+DELTA	RAYCAL 109
		DO 111 J=1,NESEG	RAYCAL 110
110		K=X+1	RAYCAL 111
		XY=2.	RAYCAL 112
		THETA=J	RAYCAL 113
		THETA=(THETA-1.1*PI)/ORAD	RAYCAL 114
		RDJ(KI)=0*SIN(THETA)	RAYCAL 115


```

00 72 J=1,MESEG
K=K+1
THETA=J
THETA=(THETA-1)*RB/DRAD
R02(K)=(D*RCOR)*SIN(THETA)
R03(K)=(D*RCOR)*COS(THETA)-RCOR
AREA=AREA
IF(I,EO,1,AND,J,EO,MESEG) AREA=AREA-DIVZ
XV=2.
IF(IJ,EO,1) XY=1.
72 RAR(K)=AREB*XY
DQ=XZ
71 DAL=AL-OR
MTWO=NEKIT
DIV=NTWO
DAL=DAL/DIV
DELR=XL*RCOR
DYL=DAL
DAL=0.
00 74 I=1,MTWO
DAL=DAL+DYL
R1=DAL*XL*RCOR
R2=DELR
DELTA=(R1-R2)/2.
AREA=PIE*RB*(R1+2-R2+21/360.
DELP=R1
D=R1-DELTA
00 74 J=1,MESEG
K=K+1
THETA=J
THETA=(THETA-1)*RB/DRAD
R02(K)=D*SIN(THETA)
R03(K)=D*COS(THETA)-RCOR
AREB=AREA
XV=2.
IF(IJ,EO,1) XY=1.
74 RAR(K)=AREB*XY
IEND=0
28 IF(TSPAT,LE,0) GO TO 12
WRITE (8) R8,REND,YC,AL,RCOR
WRITE (8) K
00 120 I=1,K
A=AR*(1-3C+46*33.48
B=K00(I)
C=ROZ(I)
188 WRITE (4) A,B,C
12 IEND=IEND+1
IF(IEND,GT,X) GO TO 25
002=RAR(IEND)*144.
D=ROZ(IEND)
DZ=ROZ(IEND)
RETURN
IEND=1000
25 RETURN
END
RAYCAL 173
RAYCAL 174
RAYCAL 175
RAYCAL 176
RAYCAL 177
RAYCAL 178
RAYCAL 179
RAYCAL 180
RAYCAL 181
RAYCAL 182
RAYCAL 183
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RAYCAL 224
RAYCAL 225
RAYCAL 226
RAYCAL 227

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```

IF(RAYPNT,NE,8.) WRITE(6,781) AQ,02,XO,R50
NTP=2
S=ACH-050/2.
60 C
C BEGIN S LOOP
C
754 X8=XO+SC*S
R=SQRT((200-SS)*S)
IF(X8,GE,C.1) S=
IF(R50,EQ,0.) GO TO 61
R=R+287/R50
GO TO 824
78 C
C
825 X8=X8
824 X8=X8
GO TO 800
820 CONTINUE
IF(R,GT,88) GO TO 800
75 C
C DETERMINE AVERAGE FLOW PROPERTIES
C
C GX=2*OS
S=S+2.*GX
LK=1
858 X8=XO+SC*S
IF(X8,LT,0.) GO TO 855
R=SQRT((250-SS)*S)+2*07**2)
CALL INTERP(X8,R,KN)
85 C
C
860 GG(LT=GG(LT)+Q(L)
LK=LK+1
S=S-GX
IF(LK,LE,5) GO TO 850
S=S+3.*GX
DO 870 L=1,4
Q(L)=GG(L)/5.
870 GG(L)=0.
GO TO 8301
880 CALL INTERP(X8,R,KN)
881 CONTINUE
Q(2)=Q(2)+Q(4)
Q(3)=Q(3)+Q(4)
IF(RAYPNT,EQ,0.) GO TO 830
WRITE(6,780) X8,R,050,Q(1),Q(2),Q(3),Q(4)
GO TO 830
158 IF(12ADCK,GT,1) GO TO 1000
READ(5,STONE)
AGA=100.
Q(4)=100.
WRITE(6,751) P(1),P(2),P(3),P(4),XT(1)
FORMAT(6X,'PH20 =',F6.4,' PC02 =',F6.4,' PGAS =',F6.4,' TEMP =',F7.2)
A,7,21
RETURN
110 C
C CONTINUE
838 NTP=NTP+1
876 NE=NTP
P(1,NE)=Q(2)
PLURAYS 59
PLURAYS 60
PLURAYS 61
PLURAYS 62
PLURAYS 63
PLURAYS 64
PLURAYS 65
PLURAYS 66
PLURAYS 67
PLURAYS 68
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PLURAYS 109
PLURAYS 110
PLURAYS 111
PLURAYS 112
PLURAYS 113
PLURAYS 114
PLURAYS 115

```


* SUBROUTINE START(XSTART, YSTART, DS)

* GEO COMMON /GEO/

1 AB, AL, BB, DOS, MEN, MP,
2 RA, RAO, RBZ, REN(10), RF, RO,
3 R0Z, RPZ, SC, SS, YANA,
4 TNG, TAMP, MCC, MEN(18), XF, XO,
5 XP, REND

* IMP COMMON /IMP/

1 D, DOZ, OY, DIST, OZ, NOZ, NOP, MPRINT, ZTST
EQUIVALENCE(RO, RO1, (RBZ, R0Z))
EQUIVALENCE(CA8, ALPHA)

15 C ROUTINE TO PRODUCE STARTING AND ENDING POINTS OF RAY THROUGH
C PLUME.
C

16 IX=YANA
TANA=ABS(TANA)
AL9=0.
OZ = ABS(OZ)

20 XSTART=O
OZSO = OZ * OZ
XZ = REND*2-OZSO

25 IF(XZ.LE.O.) XZ=0.
XZ=SQRT(XZ)
TNGP=(REND-RBZ)/AL

30 IF(IMP.EQ.1) GO TO 112H
TAP=RPZ/XF
XC=0.
112H XC=0.

35 IF(DOZ.GT.RB) XC=(DOZ-RB)/TNGP
TANB=(XZ-RBZ)/(AL-XC)
10 IF (ALPHA = 90.) 20, 609, 680

20 IF (ALPHA .GT. 90.) GO TO 268

30 ALPHA .EQ. 0.0
30 YSTART = D
YFINSH = D

40 XFINSH = AL
90 IF (DO .GE. RBZ) GO TO 115
IF(118.EQ.1.) GO TO 115

45 IF(RPZ.EQ.0.) GO TO 128
IF(13101.GE.RPZ) GO TO 120
XSTART=RPZ-ABS(O1)/TAP
GO TO 253

115 XSTART=(DO-RBZ)/TAN9+XC
GO TO 259

120 R1 = RBZ
100 DO 210 J=2, MEN

150 K = MEN - J + 1
R2 = REN(K) * REN(K) - OZSO
R2 = SIGN(SQRT(ABS(R2)), R2)

55 IF (R2 .LT. 0.0) GO TO 240
IF (DO .GE. R2) GO TO 240
R1 = R2

210 CONTINUE

	XSTART = XENI 1)	START	60
	GO TO 250	START	61
60	XSTART = (D0-R2) * (XENI K + 1) - XENI(K)) / (R1 - R2) +	START	62
	1 XENI(K)	START	63
250	IF XSTART-GE-ALP GO TO 345	START	64
	IF 1 XSTART-ALT, XENI(K)) XSTART = XENI(K)	START	65
65	IF 1 AND (EQ. 1.) GO TO 810	START	66
	GO TO 890	START	67
	0.0, LT, ALPHA, LT, 90.	START	68
	C	START	69
	C	START	70
	C	START	71
260	IF 1 R2, ALP, D.0) GO TO 340	START	72
	XK=0.	START	73
70	IF D, GE, R2) XK=D/TANA	START	74
	IF D, GE, YF) GO TO 1104	START	75
	IF 1-D, GE, R2) GO TO 1100	START	76
	XSTART=(D+R2)/(TANA*YAP)	START	77
75	GO TO 450	START	78
	XSTART=-R2	START	79
1100	XSTART=(D+R2)/TANA	START	80
	GO TO 1103	START	81
1104	IF D, GE, R2) GO TO 340	START	82
	XSTART=(D-R2)/(TANA*YAP)	START	83
	GO TO 490	START	84
	340 IF 1 D0, GE, R2) GO TO 500	START	85
	350 R1 = R2	START	86
	D0, 410 J = 2*JEN	START	87
85	K = JEN - J + 1	START	88
	R0 = D - TANA * XENI(K)	START	89
	R2 = XENI(K) * XENI(K) - D250	START	90
	R2 = SIGN(SORT(ABS(R2))) * R2)	START	91
90	IF (R2, LT, 0.0) GO TO 460	START	92
	IF (R0, GT, R2) GO TO 460	START	93
	R1 = R2	START	94
	410 CONTINUE	START	95
	XSTART = XENI(K)	START	96
55	GO TO 490	START	97
	TANE = (R2 - R1) / (XENI(K) - XENI(K + 1))	START	98
	XSTART = XENI(K) + (R0 - R2) / (TANE + TANA)	START	99
99	XSTART = D - XSTART * TANA	START	100
100	IF TANA, EQ, TAMB) GO TO 508	START	101
	XENISM=(D+R2)/(TANA-TAMB)	START	102
	IF XFINISH, LT, AL) GO TO 508	START	103
	GO TO 509	START	104
501	IF D0, GT, R8) GO TO 560	START	105
	XSTART=(D-R2)/(TANA-TAMB)	START	106
	XSTART=D-XSTART*TANA	START	107
105	IF TANA, EQ, TAMB) GO TO 509	START	108
	XENISM=(D+R2)/(TANA-TAMB)	START	109
	IF XFINISH, GT, AL) GO TO 569	START	110
	GO TO 509	START	111
110	XK=D/TANA	START	112
	IF D, LT, YC) GO TO 345	START	113
345	XSTART=(X0-TAMB+D)/(TANA-TAMB)	START	114
	XSTART=D-XSTART-TANA	START	115
	IF TANA, EQ, TAMB) GO TO 509	START	116

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115	XFIMSH=(D-XC*TANB)/(TANA-TANB)	START	117
517	IF(XFIMSH.LT.AL) GO TO 588	START	118
589	XFIMSH = AL	START	119
588	XFIMSH=D-XFIMSH*TANA	START	120
	GO TO 890	START	121
120	C	START	122
	ALPHA = 90.	START	123
	C	START	124
	C	START	125
608	IF(RPZ.LE.0.0) GO TO 658	START	126
	IF(D.GE.XF) GO TO 650	START	127
125	YSTART=R0Z*TANB*XSTART	START	128
	YFIMSH=RPZ-TAP*XSTART	START	129
	GO TO 660	START	130
658	YSTART=R0Z*TANB*(XSTART-XC)	START	131
	IF(YSTART.GT.0.) GO TO 651	START	132
130	345 DS=0.	START	133
	GO TO 500	START	134
651	YFIMSH = -YSTART	START	135
660	YFIMSH = XSTART	START	136
	GO TO 390	START	137
135	680 IF (ALPHA .GE. 180.) GO TO 828	START	138
	C	START	139
	C	START	140
	C	START	141
	90.0 .LT. ALPHA .LT. 180.0	START	142
148	IF(RPZ.EQ.0.) GO TO 681	START	143
	XK=D/TANA	START	144
	IF(XK.GE.XF) GO TO 681	START	145
	YSTART=(D-RPZ)/(TANA-TAP)	START	146
	GO TO 725	START	147
145	681 IF(191.EQ.0) GO TO 891	START	148
	IF(TANA.LE.TANB) GO TO 715	START	149
	YSTART=(D+RPZ)/(TANA-TANB)	START	150
	IF(XSTART.LE.AL) GO TO 725	START	151
	XSTART=AL	START	152
150	715 YSTART=D-XSTART*TANA	START	153
725	YFIMSH=(D-RPZ)/(TANA-TANB)	START	154
	IF(XFIMSH.GT.AL) GO TO 345	START	155
	YFIMSH=D-XFIMSH*TANA	START	156
	GO TO 890	START	157
155	891 XK=D/TANA	START	158
	IF(XK.LT.XC) GO TO 345	START	159
	IF(TANA.LE.TANB) GO TO 893	START	160
	XSTART=(D-XC*TANB)/(TANA-TANB)	START	161
	IF(XSTART.LT.AL) GO TO 892	START	162
160	892 XSTART=AL	START	163
	YSTART=D-XSTART*TANA	START	164
	YFIMSH=(D+XC*TANB)/(TANA-TANB)	START	165
	IF(XFIMSH.GT.AL) GO TO 345	START	166
	YFIMSH=D-TANA*XFIMSH	START	167
165	GO TO 890	START	168
	C	START	169
	C	START	170
	C	START	171
	ALPHA = 180.	START	172
170	828 A150 = 1.	START	173
	GO TO 30	START	
	830 A150 = XSTART	START	

	VSISTART = XFINSH	START	176
	XFINSH = A100	START	175
175	A100 = 8.	START	176
	CONTINUE	START	177
	TRANSFER	START	178
	803 DS = SCRT 1 1 XFINSH = VSISTART 1 002 1	START	179
	1 / 005	START	180
	VSISTART-A95(VSISTART)	START	181
180	900 RETURN	START	182
	END	START	183
	CINTERP	INTERP	2


```

      SUBROUTINE INTERP( O, X, R, KA )
      PLM
      COMMON/PLM/PLMG(J),RCM,ST(50),NRD(50),PLM(3,30,50),NFLM,PA,P8,
      1 DPOX,KDATA,ISHK,JSKH,TANE,EOB
      DIMENSION XY(50),NBX(50),XX(5,30,50)
      EQUIVALENCE (NBX(1),NRD(1)),(XX(1,1,1)),PLM(1,1,1)),(XY(1),ST(1))
      DIMENSION O(4)
      C
      C ROUTINE TO INTERPOLATE BETWEEN STATIONS ALONG CENTERLINE OF
      C PLUME AND ALONG RADIAL DIMENSION OF PLUME.
      C RETURNS THE FOLLOWING ARGUMENTS
      C O(1) STATIC TEMP IN DEGREE S
      C O(2) MOLE CONCENTRATION OF H2O
      C O(3) MOLE CONCENTRATION OF CO2
      C O(4) GAS PRESSURE ATMO
      C
      IF(X,LT,XY(49)) GO TO 20
      120 DO 125 I=2,5
      125 D(1)= XX(I,1,49)
      M=I-1
      RETURN
      20 INCR = 1
      N1= 1
      30 L = 2
      K1=N1+INCR
      IF ( X ,LT, XY( 1,1 ) ) GO TO 120
      IF ( X ,GE, XY( N1 ) ) GO TO 40
      K = N1
      K1 = N1
      GO TO 140
      40 DO 110 KK=L,49
      KML=K1-INCR
      IF(4-X*(K1))50,55,60
      50 IF ( X ,GE, XY( KML ) ) GO TO 70
      GO TO 100
      60 IF ( X ,LE, XY( KML ) ) GO TO 70
      100 K1=K1+INCR
      110 CONTINUE
      GO TO 120
      55 K=K1
      GO TO 140
      70 K=K1
      140 N = N3X( K1 )
      141 L = K
      DO 190 JJ=2,N
      IF(2-XY(1,JJ,K1))150,169,169
      150 IF(2-GE,XK(1,JJ-1,K1))GO TO 210
      GO TO 190
      160 IF(2-LE,XY(1,JJ-1,K1))GO TO 210
      190 CONTINUE
      GO TO 120
      169 JJ=JJ+1
      GO TO 220
      210 JJ=JJ+1
      220 N = NBX( K1 )
      DO 240 JJ=2,N
      IF(2-XY(1,JJ,K)) 230,249,240

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238	IF (R, GE, XX(I, J1 - L, K1))	GOTO 365	INTERP	60
	GO TO 260		INTERP	61
243	IF (R, LE, XX(I, J1 - L, K1))	GOTO 305	INTERP	62
280	CONTINUE		INTERP	63
	GO TO 120		INTERP	64
249	J=J1		INTERP	65
	GO TO 310		INTERP	66
65	385 J = J1 - 1		INTERP	67
	310 DO 330 N=1, 4		INTERP	68
	I = M + 1		INTERP	69
	IF (K, NE, K1)	GO TO 329	INTERP	70
	IF (J, NE, J1)	GO TO 327	INTERP	71
78	O(M) = XX(I, J, K)		INTERP	72
	GO TO 332		INTERP	73
	327 O(M) = XX(I, J, K) + (R - XX(I, J, K1)) / (XX(I, J1, K) - XX(I, J, K1))		INTERP	74
	I = XX(I, J, K1)		INTERP	75
	GO TO 332		INTERP	76
75	329 O(M) =	$XX(I, J, K1) + (XX(I, J1, K) - XX(I, J, K1)) / (XX(I, J1, K1) - XX(I, J, K1))$	INTERP	77
	J = XX(I, J, K1) / (XX(I, J1, K) - XX(I, J, K1))		INTERP	78
	I = (R - XX(I, J, K1)) / (XX(I, J1, K1) - XX(I, J, K1))		INTERP	79
	O(M) = D(I, M)		INTERP	80
	I = XX(I, J, K1) / (XX(I, J1, K1) - XX(I, J, K1))		INTERP	81
80	2 (R - XX(I, J, K1)) - D(M)		INTERP	82
	4	$(XX(I, K1) - YY(I, K1))$	INTERP	83
	5 * (X - XX(K, I))		INTERP	84
	330 CONTINUE		INTERP	85
85	RETURN		INTERP	86
	END		INTERP	87

LINE	CODE	TEXT	PLUSIG
2		SUBROUTINE PLUSIG	PLUSIG
3			PLUSIG
4		APPARENT SPECTRAL RADIANCES OF PLUMES	PLUSIG
5		REAL L,MU,NFREQ,NOZ,MUING	PLUSIG
6		REAL KH2O,KCO2	PLUSIG
7			PLUSIG
8			PLUSIG
9			PLUSIG
10		INSERT THE FOLLOWING CARD AND REMOVE APPROPRIATE CARD FOR	PLUSIG
11		MULTIPLE WAVELENGTHS	PLUSIG
12			PLUSIG
13			PLUSIG
14		DIMENSION YN2O12(1),GAS(4),MU19,3001,ALPHA(2),	PLUSIG
15		1 TAU1(50),TAUV1(50),TAUVN(50),OMU15,3001,	PLUSIG
16		DIMENSION YN2O12(1),GAS(4),MU13001,ALPHA(2),	PLUSIG
17		1 TAU1(50),TAUV1(50),TAUVN(50),OMU13001,	PLUSIG
18		2 MEAT(3),PA1(50),PA1(50),PB1(50),	PLUSIG
19		3 K1(2),B1(2),IMP1(7),K1(7),B1(7),IMP1(7)	PLUSIG
20			PLUSIG
21		COMMON/BETA1/KH2O(7,439),6M2017,439)	PLUSIG
22		COMMON/BETA1/KCO2(7,176),8C02(7,114)	PLUSIG
23		COMMON/CHJCK/NT,NE,NFREQ,MU,NUFIRST,MUING,DMU	PLUSIG
24			PLUSIG
25		REMOVE COMMENT CARDS FOR SPECTRAL DISTRIBUTION OF SIGNATURES	PLUSIG
26		AT ALL RANGES AND ALL WAVELENGTHS	PLUSIG
27			PLUSIG
28		COMMON/STAN/ALTOBS(5),ALTPM,XRANGE(5),IATMO,TBACK(5),TBACKC	PLUSIG
29		COMMON/ANAL/ITYPE,ITAU,IL,OA,ASB(5)	PLUSIG
30		COMMON/ATMO/NATHM,NRANG,ASPOEG	PLUSIG
31		COMMON/OST/XTTRA(20),NRG,XTTRA1(5),AMI(5),AME(5),YTRA(2)	PLUSIG
32		COMMON/DHLOLO/EXTTRA(250)	PLUSIG
33		COMMON/EXTENS/EXTTRA(20),ETEMP(20),NEXT,XCC,SENT(5,1)	PLUSIG
34			PLUSIG
35		INSERT FOLLOWING CARDS FOR MULTIPLE WAVELENGTHS	PLUSIG
36			PLUSIG
37		COMMON/SSIG/SGAS(5,5),SAM1(5,5),SMTL(5,5),SBSR(5,5)	PLUSIG
38		COMMON/SSIG/SPSIG(5,5,300)	PLUSIG
39			PLUSIG
40		COMMON/SSIG/SPSIG(1,5,300)	PLUSIG
41		COMMON/SSIG/SGAS(5,1),SAM1(5,1),SMTL(5,1),SBSR(5,1)	PLUSIG
42		COMMON/SPAT/ISPAT	PLUSIG
43		COMMON/LOS/DS(50),I(50),PL(50),P2(50),P3(50)	PLUSIG
44		COMMON/FILTER/FILTER,BFILTR(300)	PLUSIG
45		COMMON/FILES/FMP(5),FAMP(5),FGAS(5),FBC(5),FEXT(5)	PLUSIG
46		COMMON/GAS/IRADCK	PLUSIG
47		DATA MEAT/MOBY,4MNOB,3HMET/	PLUSIG
48		DATA EXPO/-9, /	PLUSIG
49		DATA ALPHA(1),ALPHA(2)/0.2,0.769/	PLUSIG
50		DATA GAS/3H2O,3HCO2,2H2,3HN2O/	PLUSIG
51			PLUSIG
52		ROUTINE TO COMPUTE APPARENT SPECTRAL RADIANCES OF THE PLUME	PLUSIG
53		RAY, LOGIC AND A MAJORITY OF DATA BASED ON THE UNIVERSITY	PLUSIG
54		OF MICHIGAN PLUMES MODEL	PLUSIG
55		COMPUTES RADIANT INTENSITY IN WATTS/SR FOR THE 2.0 - 10	PLUSIG
56		EACH OF THE NRG WAVELENGTHS	PLUSIG
57		SUMCS GAS RADIANCE	PLUSIG
58		SUMCG BACKGROUND RADIANCE	PLUSIG

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65	C	SUMP ATTENUATED METALS	PLUSIG	59
66	C	SNAP BLACK BODY RADIANCE	PLUSIG	60
	C	THIS ROUTINE INITIALIZES NU AND OMU FOR EACH WAVELENGTH	PLUSIG	61
	C		PLUSIG	62
	C		PLUSIG	63
	C	REMOVE THE FOLLOWING CARD FOR MULTIPLE WAVELENGTHS	PLUSIG	64
	C		PLUSIG	65
65	C	NRG=1	PLUSIG	66
		IF IRADCK.LE.01 GO TO 151	PLUSIG	67
		NT=1	PLUSIG	68
		IF EAREALLD.GT.0.C.AND. IRADCK.EQ.21 NT=0	PLUSIG	69
		IF EAREALLD.GT.0.C.AND. IRADCK.EQ.21 NT=0	PLUSIG	70
70	151	CONTINUE	PLUSIG	71
	C	98C=1ATMD	PLUSIG	72
	C		PLUSIG	73
75		MOD=ENT	PLUSIG	74
		DO 2000 EQ=1,NRANG	PLUSIG	75
		MT=N*DLT	PLUSIG	76
		PANG=XRANGGET(I)	PLUSIG	77
50		IF (2*USEONE.0,1) GO TO 55	PLUSIG	78
		NA=0	PLUSIG	79
		GO TO 57	PLUSIG	80
85	55	NA=NE	PLUSIG	81
		CALL ATPOS(191	PLUSIG	82
		KCAL=0.	PLUSIG	83
		DO 45 J=1,NA	PLUSIG	84
		KCAL=XCAL+(P1(I)+P2(I)+P3(I))+273.15*OS(11*8.008036/7(I))	PLUSIG	85
		KNOX(I)=KCAL	PLUSIG	86
85	44	CONTINUE	PLUSIG	87
		DO 2000 I=1,NR2	PLUSIG	88
		IF IL.LI.01 GO TO 332	PLUSIG	89
		XXP=XPANGF/1.DE+5	PLUSIG	90
		ALT=ALTPLM/1.DE+5	PLUSIG	91
90		ALC=ALTOS(I)/1.DE+5	PLUSIG	92
		WRITE(6,331) XYRAN,ASPDG	PLUSIG	93
		WRITE(6,333) MEALNTHO	PLUSIG	94
		WRITE(6,334) ALT,ALC	PLUSIG	95
95	332	CONTINUE	PLUSIG	96
	C		PLUSIG	97
	C	SETUP WU AND OMU FOR WAVELENGTH OF CALCULATION (IKI)	PLUSIG	98
	C		PLUSIG	99
	C		PLUSIG	100
100		SUMEX=0.	PLUSIG	101
		SFP=0.	PLUSIG	102
		SFAP=0.	PLUSIG	103
		SFGS=0.	PLUSIG	104
		SFAC=0.	PLUSIG	105
105		SFA=1.	PLUSIG	106
		SUMGS=0.	PLUSIG	107
		SUMBS=0.	PLUSIG	108
		SNAP=0.	PLUSIG	109
		SUMHP=0.	PLUSIG	110
		IF (HURSTINE.0) GO TO 335	PLUSIG	111
110		MEAN=1.0E+4/NI(I)KI	PLUSIG	112
		MBE=1.0E+4/ME(I)KI	PLUSIG	113
		KUC=MBG	PLUSIG	114
		IF (NINIC.GT.0.1) GO TO 42	PLUSIG	115

LINE	CODE	TEXT	PLUSIG
115	C	INCREMENTS BASED ON MAXIMUM RESOLUTION OF DATA INCLUDED IN	116
116	C	THE UNIVERSITY OF MICHIGAN PLUMES PROGRAM	117
117	C		118
118	C		119
119	C		120
120	C		121
121	C		122
122	C		123
123	C		124
124	C		125
125	C		126
126	C		127
127	C		128
128	C		129
129	C		130
130	C		131
131	C		132
132	C		133
133	C		134
134	C		135
135	C		136
136	C		137
137	C		138
138	C		139
139	C		140
140	C		141
141	C		142
142	C		143
143	C		144
144	C		145
145	C		146
146	C		147
147	C		148
148	C		149
149	C		150
150	C		151
151	C		152
152	C		153
153	C		154
154	C		155
155	C		156
156	C		157
157	C		158
158	C		159
159	C		160
160	C		161
161	C		162
162	C		163
163	C		164
164	C		165
165	C		166
166	C		167
167	C		168
168	C		169
169	C		170
170	C		171
171	C		172

118	CALL SETTAU(NT,DS,T,P2,P3,ALPHA(2),PA,PB)	PLUSIG	173
	DO 230 IF=1,NPE2	PLUSIG	174
	CALL KOCAL(NU(11),GAS(1),K1	PLUSIG	175
	CALL KOCAL(NU(11),GAS(2),K	PLUSIG	176
175	NAME=GAS(1)	PLUSIG	177
	NUFE(NU(11))	PLUSIG	178
	CALL TAUCAL(K1	PLUSIG	179
	AT,TYPE,EXP,TAU(1)	PLUSIG	181
	NAME=GAS(2)	PLUSIG	182
188	CALL TAUCAL(K	PLUSIG	183
	TEMP,TAU)	PLUSIG	184
	NAME=GAS(1)	PLUSIG	185
	CALL TAUN2D(NUFREQ,HA,NT,MN2,TAUV)	PLUSIG	186
	SUMS=0	PLUSIG	187
	IF(NA,EG,NT) GO TO 191	PLUSIG	188
	IF(NA,GT,0) GO TO 132	PLUSIG	189
	SUMS=FLA(CK(11),NUFREQ*(1.-TAUV(11)*TAUV(11)*TAUV(11))	PLUSIG	190
	IF(NT,11,21) GO TO 159	PLUSIG	191
	MISS=NA(1	PLUSIG	192
	IF(NA,EG,0) MISS=2	PLUSIG	193
	DO 195 MISS=NT	PLUSIG	194
	TAUCAL=TAUV(11)*TAUV(11)*TAUV(11)*TAUV(11)*TAUV(11)	PLUSIG	195
	IF(TAUCAL,LT,0.1) TAUCW=0	PLUSIG	196
	SUMS=SUMS+PLA(US(11),NUFREQ)*TAUCW	PLUSIG	197
	CONTINUE	PLUSIG	198
	TAUCW=1	PLUSIG	199
	IF(TAUCAL,GT,0.1) IF(US=TAUCW(NA)*TAUV(NA)*TAUV(NA))	PLUSIG	200
	L=SUMS*DA*DN(11)	PLUSIG	201
	NO2=TAUC(11)*NO	PLUSIG	202
	SUMS=0	PLUSIG	203
	IF(TAUCAL,GT,0) SUMS=L,-TAUV(11)*TAUV(11)*TAUV(11)	PLUSIG	204
	FP=0	PLUSIG	205
	FA=0	PLUSIG	206
	FG=0	PLUSIG	207
	FX=0	PLUSIG	208
	SMP=J	PLUSIG	209
	SRO=0	PLUSIG	210
	SEX=J	PLUSIG	211
	IF(KOC,EG,0) GO TO 214	PLUSIG	212
	DO 215 KK=1,NEXT	PLUSIG	213
	SE=PLANC(TEMP(1),NUF	PLUSIG	214
	SEAS(TEMP(1),TAUVS	PLUSIG	215
	CONTINUE	PLUSIG	216
	IF(KOZ,LE,0) GO TO 191	PLUSIG	217
	SMP=PLANC(KOZ,NUFREQ)*DN(11)*AB(1,K)*B(0	PLUSIG	218
	SMP=SMP+TAUV(NT)*TAUV(NT)*TAUV(NT)	PLUSIG	219
	IF(13AKC,LE,0) GO TO 310	PLUSIG	220
	SRO=PLANC(13AKC,NUFREQ)*DN(11)*DA	PLUSIG	221
	IF(L,LT,0) GO TO 210	PLUSIG	222
	WRITE(6,100) NU(11),DN(11),L,SMP,SMP,SBC,DA,AB(1,K),TAUVS	PLUSIG	223
	SUMS=SUMP+SMP	PLUSIG	224
	SUMS=SUMP+SMP	PLUSIG	225
	SUMS=SUMP+S	PLUSIG	226
	SUMS=SUMP+S	PLUSIG	227
	SUMS=SUMP+S	PLUSIG	228
	SUMS=SUMP+S	PLUSIG	229

230	SPSIG(IK,IR,II)=L-SBG*SNP+SPSIG(IK,IR,II)	PLUSIG	230
	SPSIG(IK,IR,II)=SPSIG(IK,IR,II)*SEX	PLUSIG	231
	IF(IFILTER.EQ.0) GO TO 200	PLUSIG	232
	FGS=L*BFILTR(II)	PLUSIG	233
	FK=SEX*BFILTR(II)	PLUSIG	234
	ED=SNP*BFILTR(II)	PLUSIG	235
235	FAP=SNP*BFILTR(II)	PLUSIG	236
	FG=SIC*BFILTR(II)	PLUSIG	237
	SFP=SFAP*FP	PLUSIG	238
	SFAP=SFAP*FAP	PLUSIG	239
	SFGS=SFGS*FGS	PLUSIG	240
240	SFG=SFG*FG	PLUSIG	241
	SFK=SF*FY	PLUSIG	242
	CONTINUE	PLUSIG	243
	200	PLUSIG	244
	ZZZ=SUMHP-SUMBG+SUMGS	PLUSIG	245
245	IF(ISPAT.GT.0) WRITE (0) ZZZ	PLUSIG	246
	IF(ILL.LT.0) GO TO 211	PLUSIG	247
	WRITE(6,212) ZZZ,SUMHP,SNAMP,SUMGS,SUMBG	PLUSIG	248
	IF(YCO.NE.0.) WRITE(6,216) SUMEX	PLUSIG	249
	CONTINUE	PLUSIG	250
250	211	PLUSIG	251
	C IR,IK IMPLIES RANGE AND WAVELENGTH	PLUSIG	252
	C INTEGRATING OVER THE ENTIRE PLUME	PLUSIG	253
	C	PLUSIG	254
255	SGASTR(IK)=SGAS(IR,IK)+SUMGS	PLUSIG	255
	SMTLIR(IK)=SMTL(IE,IK)+SUMHP	PLUSIG	256
	SMTL(IE,IK)=SMTL(IE,IK)+SNAMP	PLUSIG	257
	SBGTR(IE,IK)=SBG(IE,IK)+SUMBG	PLUSIG	258
	SEXT(IE,IK)=SEXT(IE,IK)+SUMEX	PLUSIG	259
260	IF(FILTER.EQ.0) GO TO 401	PLUSIG	260
	ZZZ=SEGS-SFBS*SFAP	PLUSIG	261
260	IF(ISPAT.GT.0) WRITE (0) ZZZ	PLUSIG	262
	FHP(IE)=FHP(IE)+SFP	PLUSIG	263
	FAMPI(IE)=FAMPI(IE)+SFAP	PLUSIG	264
	FGAST(IE)=FGAST(IE)+SEGS	PLUSIG	265
265	FBG(IE)=FBG(IE)+SFBS	PLUSIG	266
	FEXT(IE)=FEXT(IE)+SFX	PLUSIG	267
	CONTINUE	PLUSIG	268
401	IF(IE.NE.NRG) GO TO 2000	PLUSIG	269
	IF(IE.EQ.NRANG) GO TO 2000	PLUSIG	270
270	IF(RANGE.EQ.0.) GO TO 2000	PLUSIG	271
	NT=N*HOLD	PLUSIG	272
	DO 400 I=1,NT	PLUSIG	273
	P1(I)=P1(I)+NA	PLUSIG	274
	P2(I)=P2(I)+NA	PLUSIG	275
275	P3(I)=P3(I)+NA	PLUSIG	276
	DS(I)=DS(I)+NA	PLUSIG	277
	T(I)=T(I)+NA	PLUSIG	278
400	CONTINUE	PLUSIG	279
2000	FORMAT(15,F10.2,2X,F10.3,6(2X,210.4),2X,F10.5)	PLUSIG	280
300	FOR MAT(15,8X,NU*.7X,DELTA (U*.6X,RAY COMPONENT RADIANT INTENSI	PLUSIG	281
300	11V WATTS/SE*.9X,DA*.X,NOT PARTS*.5X,ATMO*2X,CM-1*.8X,CM-1*	PLUSIG	282
	2X,IAS*.8X,METALS*.4X,ATIN METAL*.2X,BACKGROUND*.5X,SD CM*.7X	PLUSIG	283
	3*.50 CM*.6X,TRANS*)	PLUSIG	284
	FORMAT(10,3H***RAY DATA FOR A RANGE OF *.F10.3, KM AND AN ASPE	PLUSIG	285
205	10T ANGLE OF *.F5.1, DEG*EES*,3H***)	PLUSIG	286

333	FORMAT124,2M00,ATMOSPHERIC TYPE = 0,Ab,2M00	PLUSIG	37
212	FORMAT110,3X,RAY TOTALS, APPARENT RADIANCE = 0,F10,5/16X,ATTENU, PLUSIG	PLUSIG	288
	1A10 METAL = 0,F10,5/16X,METALS = 0,F10,5/16X,GAS = 0,F10,5/16X, PLUSIG	PLUSIG	289
298	2*8ACCGROUND = 0,F10,5/16X, PLUSIG	PLUSIG	290
316	FORMAT12X,1M00,VEHICLE ALTITUDE = 0,F6,2,0, K4 AND OBSERVER ALTITUD	PLUSIG	291
	1E = 0,F6,2,0, KM1	PLUSIG	292
216	FORMAT116X,EXTERNAL EMISSIONS = 0,F10,5/16X	PLUSIG	293
	END	PLUSIG	294


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5      SUBROUTINE ATMOS(IZR)
6      DIMENSION NU(300),XA(50),XB(50),XC(50),XD(50),XE(50),DMU(300)
7
8      DIMENSION A(3,3),B(3,3)
9
10     COMMON/DHOL/ZA,XB,XC,XD,XE
11     COMMON/STAN/ALT0B(5),ALTPLM,XRANGE(5),IATMO,TBACK(5),TBACKC
12     COMMON/ATMO/ATMO,NRANG,ASDEG
13     COMMON/CHUCK/NT,NA,NFREQ,NU,MUFST,MUINC,DMU
14     COMMON/LOS/DS(50),T(50),P1(50),P2(50),P3(50)
15     DATA A/-7.515,6.988,22.83,-7.602,6.988,
16           128.49,-5.745,6.996,17.26/,
17           29/-13146,-.00423,-.2221,-.01295,-.084105,
18           3,-.213,-.01307,-.00413,-.2151/
19     DATA PE/6.44E8/
20     RANGE=YRANGE(IPI)
21     ALTOS=ALTC(IPI)
22     IF (NT.EQ.0) GO TO 100
23
24     DO 101 I=1,NT
25       XA(I)=DS(I)
26       XB(I)=T(I)
27       XC(I)=P1(I)
28       XD(I)=P2(I)
29       XE(I)=P3(I)
30
31     OALT=ALTPLM-ALT0BS
32     A02=ALT0BS*ALT0BS
33     RT2=RANGE*RANGE
34     AP2=ALTPLM*ALTPLM
35     DING=RANGE/FLOAT(NAL)
36     DO 150 I=1,NA
37       DS(I)=DING
38       R=DINC*FLOAT(I-1)+DING/2.
39       X=RT2+2*ALT0BS*RE+R*(R/RANGE)*(A02-2*RE*OALT+
40         1*RT2-AP2)/1/(ALT0BS+2*RE)
41       X=X/3.04E3
42       T(I)=273.15+A(I,3,NATMO)+8(I,3,NATMO)*X
43       PTOT=EXPLA(2,NATMO)+8(2,NATMO)*X*1.E-3
44       P1(I)=PTOT*13.01*EXP(A(I,1,NATMO)+8(1,NATMO)*X)
45       P2(I)=PTOT*.80032
46       P3(I)=PTOT-P1(I)-P2(I)
47       CONTINUE
48     IF (NT.EQ.0) GO TO 208
49     DO 132 I=1,NT
50       NH=NA+I
51       OS(NH)=XA(I)
52       T(NH)=XB(I)
53       P1(NH)=XC(I)
54       P2(NH)=XD(I)
55       P3(NH)=XE(I)
56       NT=NT+NA
57       CONTINUE
58     RETURN
59     END
60
61 C ROUTINE TO COMPUTE PATH PARAMETERS
62 C
63

```

SUBROUTINE SETTAUINDIV,DL,TMP,PABSOR,PBROAD,ALPHA,PA,PB)	SETTAU	4
DIMENSION PA(50),PB(50),DL(50),TMP(50),PABSOR(50),PBROAD(50)	SETTAU	5
DO 100 I=1,NDIV	SETTAU	6
PA(I)=273.15*DL(I)*PABSOR(I)/TMP(I)	SETTAU	7
PB(I)=PABSOR(I)*ALPHA*PBROAD(I)	SETTAU	8
CONTINUE	SETTAU	9
RETURN	SETTAU	10
END	SETTAU	11

```

SUBROUTINE TAUCAL(K,8,TEMP,NTEMP,NDIV,PA,PB,TMP,ITYPE,EXPO,TAU)
C
C TRANSMITTANCE CALCULATION
C
5  DIMENSION PA(50),PB(50),TAU(50),TEMP(10),TMP(50),AI(7),
   1  BI(7),DI(7),KI(7),LI(7),RI(7),CI(7),PK(50),FI(50)
   2  TAUCAL
   3  TAUCAL
   4  TAUCAL
   5  TAUCAL
   6  TAUCAL
   7  TAUCAL
   8  TAUCAL
   9  TAUCAL
  10  TAUCAL
  11  TAUCAL
  12  TAUCAL
  13  TAUCAL
  14  TAUCAL
  15  TAUCAL
  16  TAUCAL
  17  TAUCAL
  18  TAUCAL
  19  TAUCAL
  20  TAUCAL
  21  TAUCAL
  22  TAUCAL
  23  TAUCAL
  24  TAUCAL
  25  TAUCAL
  26  TAUCAL
  27  TAUCAL
  28  TAUCAL
  29  TAUCAL
  30  TAUCAL
  31  TAUCAL
  32  TAUCAL
  33  TAUCAL
  34  TAUCAL
  35  TAUCAL
  36  TAUCAL
  37  TAUCAL
  38  TAUCAL
  39  TAUCAL
  40  TAUCAL
  41  TAUCAL
  42  TAUCAL
  43  TAUCAL
  44  TAUCAL
  45  TAUCAL
  46  TAUCAL
  47  TAUCAL
  48  TAUCAL
  49  TAUCAL
  50  TAUCAL
  51  TAUCAL
  52  TAUCAL
  53  TAUCAL
  54  TAUCAL
  55  TAUCAL
  56  TAUCAL
  57  TAUCAL
  58  TAUCAL

C COMPUTE 3E 1 ELEMENTS OF SUMS
81  SUMN=0.
   1  SUMD=0.
   2  DO 62 I=1,NDIV
   3  IF(TMP(I)).GT.300.160 TO 61
   4  PK(I)=KI(I)*PA(I)
   5  FI(I)=PK(I)*BI(I)*PB(I)
   6  GO TO 83
   7  IF(TMP(I)).LT.300.160 TO 84
   8  PK(I)=K(INTERP)*PA(I)
   9  FI(I)=PK(I)*BI(INTERP)*PB(I)
  10  GO TO 43
  11  PK(I)=INTERP*(TEMP,K,TEMP,TMP(I))*PA(I)
  12  FI(I)=PK(I)*INTERP*(TEMP,9,NTEMP,TMP(I))*PB(I)
  13  SUMD=SUMD+PK(I)
  14  SUMN=SUMN+FI(I)
  15  CONTINUE
  16  IF(SUMD.LE.0.160 TO 700
  17  BETEFF=SUMN/SUMD
  18  C BEGINNING OF TAU CALC. LOOP
  19  K=3.
  20  DO 630 I=1,NDIV
  21  C COMPUTE B/BE & DETERMINE WHERE WE ARE IN ETA FAMILY
  22  IF(PK(I).LE.0.)OR.(BETEFF.LE.0.)160 TO 240
  23  BSC=FI(I)/(BETEFF*PK(I))
  24  DI=PK(I)/BETEFF
  25  IF(DI.LE.0.160 TO 240
  26  IF(EXPO.LE.1.)AND.(EXPO.GE.0.1160 TO 120
  27  ARG=X*(10X*(88E+1.1)/2.)
  28  IF(ARG.LE.0.1160 TO 100
  29  IF(18E.LE.1.)AND.(ARG.GE.10.1160 TO 110
  30  IF(139E.LE.1.05)AND.(88E.GE.95)160 TO 100
  31  GO TO 200
  32  C COMPUTATION OF K FOR LIMITING ETA VALUES
  33  X=X*DX
  34  GO TO 240
  35  X=X*DX*83E
  36  GO TO 240
  37  X=X*DX*(88E**EXPO)
  38  GO TO 240
  39  C CALCULATION OF ETA

```

208	XIS=1.+9.185*8BE	TAUCAL	59
	DO 210 J=1,7	TAUCAL	61
68	IF(8BE.LE.8R(J))GO TO 220	TAUCAL	61
210	CONTINUE	TAUCAL	62
	J=6	TAUCAL	63
	RESID=0.	TAUCAL	64
	GO TO 221	TAUCAL	65
65	RESID=(8BE-8R(J-1))/(8R(J)-8R(J-1))	TAUCAL	65
221	IF(ARG.GE.XIS)GO TO 230	TAUCAL	66
	C=CI(J-1)*(1.-RESID)+CI(J)*RESID	TAUCAL	67
	D=DI(J-1)*(1.-RESID)+DI(J)*RESID	TAUCAL	68
	ETA=2*ARG/(XIS+2*ARG)	TAUCAL	69
70	X=X+J*(8BE*ETA)	TAUCAL	70
	GO TO 240	TAUCAL	71
230	A=AI(J-1)*(1.-RESID)+AI(J)*RESID	TAUCAL	72
	9A=9I(J-1)*(1.-RESID)+9I(J)*RESID	TAUCAL	73
	ETA=(ARG+A)/(ARG+B)	TAUCAL	74
75	X=X+J*(9A*ETA)	TAUCAL	75
	CALCULATION OF TAU	TAUCAL	76
240	IF(X.GT.0.)GO TO 242	TAUCAL	77
	TAU(1)=1.	TAUCAL	78
	GO TO 63.	TAUCAL	79
60	8FACT=-8CTEFP*(SORT(1.+1.57879*8X))	TAUCAL	80
242	GO 3 (300,500),TYPE	TAUCAL	81
300	TAU(1)=EXP(8FACT)	TAUCAL	82
	GO TO 630	TAUCAL	83
630	TAU(1)=1.+8FACT	TAUCAL	84
630	CONTINUE	TAUCAL	85
65	RETURN	TAUCAL	86
	UNUSUAL VALUES OF ARGUMENTS TAU IS SET TO 1.	TAUCAL	87
700	DO 710 I=1,NDIV	TAUCAL	88
	TAU(I)=1.	TAUCAL	89
90	CONTINUE	TAUCAL	90
710	RETURN	TAUCAL	91
	END	TAUCAL	92
		TAUCAL	93

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SUBROUTINE KBCAL(MUFREQ,GAS,K,B,TEMP,MTEMP)
COMMON/BETAK/KC02(7),1761,8C02(7),1491
COMMON/BETAK1/KH20(7),4391,8H20(7),6391
DIMENSION WILIM(4),LOLIM(4),TH20(7),TC02(7),NT(14),K(10),B(18)
5 1,13(4),TEMP(10)
REAL LOLIM,MUFREQ, K,KH20,KC02
REAL ID
DATA ID/3MH20,3HC02,2MHF,2HCO/
DATA WILIM/11000,3770,7,LOLIM/50,1900,7
DATA TH20/300,500,1000,1500,2000,2500,3000,7,NT/7,7,7
DATA TC02/300,600,1200,1500,1800,2400,3000,7
C SEE GAS INDEX & CHECK IF MUFREQ IS WITHIN LIMITS OF B. N. PARAMETERS
DO 13 I=1,4
IF(GAS.EQ.ID(I))GO TO 20
15 CONTINUE
GO TO 17
12 MTEMP=NT(I)
GO TO 13(15,17,12),I
20 DO 14 J=1,MTEMP
TEMP(J)=TH20(J)
K(J)=C.
14 R(J)=1.
GO TO 19
15 DO 16 J=1,MTEMP
TEMP(J)=TC02(J)
K(J)=0.
16 R(J)=1.
GO TO 19
17 MTEMP=2
DO 18 I=1,2
K(J)=C.
18 R(J)=1.
TEMP(1)=300.
TEMP(2)=3000.
35 RETURN
21 IF(MUFREQ.GT.WILIM(1),OR,MUFREQ.LT.LOLIM(1))GO TO 12
C
C SET K,B APPAYS FOR APPROPRIATE MUFREQ & GAS
GO TO 30(43,60,70),I
40 FINDEX=((MUFREQ-50.)/25.)*1+1.
INDEX=FINDEX
FRACT=INDEX-FLOAT(INDEX)
FRAC1=1.-FRACT
MTEMP=NT(I)
DO 32 J=1,MTEMP
TEMP(J)=TH20(J)
K(J)=KH20(J,INDEX)*FRAC1+KH20(J,INDEX+1)*FRACT
B(J)=BH20(J,INDEX)*FRAC1+BH20(J,INDEX+1)*FRACT
32 CONTINUE
GO TO 60
50
C
60 IF(MUFREQ.LT.3000.)GO TO 41
FINDEX=45.+(MUFREQ-3000.)/10.
GO TO 43
41 IF(MUFREQ.LT.3000.)GO TO 42
FINDEX=44.+(MUFREQ-3000.)/80.
GO TO 44
55

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42	IF(INUFREQ,LT,2400.)GO TO 43	KBCAL	59
	FINDX=83.+(INUFREQ-2400)/600.)	KBCAL	60
60	GO TO 48	KBCAL	61
43	IF(INUFREQ,LT,2000.)GO TO 44	KBCAL	62
	FINDX=3.+(INUFREQ-2000.)/10.)	KBCAL	63
	GO TO 49	KBCAL	64
65	FINDX=1.+(INUFREQ-1900.)/50.)	KBCAL	65
44	INDEX=FINDX	KBCAL	66
48	FRACT=FINDX-FLOAT(INDEX)	KBCAL	67
	FRAM=1.-FRACT	KBCAL	68
	MEM=INT(1)	KBCAL	69
	DO 59 J=1,NTEMP	KBCAL	70
70	BLJ=3C02(IJ,INDEX)*FRAM+8C02(IJ,INDEX*1)*FRACT	KBCAL	71
	TEMP(IJ)=TC02(IJ)	KBCAL	72
	CONTINUE	KBCAL	73
49	IF(INUFREQ,LT,1500.)GO TO 51	KBCAL	74
	FINDX=13.+(INUFREQ-1500.)/5.)	KBCAL	75
75	GO TO 53	KBCAL	76
51	IF(INUFREQ,LT,2900.)GO TO 52	KBCAL	77
	FINDX=77.+(INUFREQ-2900.)/10.)	KBCAL	78
	GO TO 59	KBCAL	79
52	IF(INUFREQ,LT,2400.)GO TO 53	KBCAL	80
	FINDX=76.+(INUFREQ-2400.)/50.)	KBCAL	81
60	GO TO 59	KBCAL	82
53	IF(INUFREQ,LT,2150.)GO TO 54	KBCAL	83
	FINDX=26.+(INUFREQ-2150.)/5.)	KBCAL	84
	GO TO 59	KBCAL	85
85	FINDX=1.+(INUFREQ-1900.)/10.)	KBCAL	86
82	INDEX=FINDX	KBCAL	87
54	FRACT=FINDX-FLOAT(INDEX)	KBCAL	88
53	FRAM=1.-FRACT	KBCAL	89
	DO 59 J=1,NTEMP	KBCAL	90
90	K(IJ)=K02(IJ,INDEX)*FRAM+K02(IJ,INDEX*1)*FRACT	KBCAL	91
	CONTINUE	KBCAL	92
59	GO TO 80	KBCAL	93
		KBCAL	94
		KBCAL	95
		KBCAL	96
95	GO TO 12	KBCAL	97
70	GO TO 12	KBCAL	98
80	RETURN	KBCAL	99
	END	KBCAL	100

```

FUNCTION PLANK(T,M)
DATA C1,C2/1.1909E-12,1.4388/
IF T.LE.0.160 TO 5
  X=C2*M/T
  IF X.LT.172.160 TO 10
    PLANK=0
  RETURN
  10 PLANK=(C1*M*M*M)/(EXP(X)-1.)
  RETURN
  20 END

```

```

PLANK 2
PLANK 3
PLANK 4
PLANK 5
PLANK 6
PLANK 7
PLANK 8
PLANK 9
PLANK 10
PLANK 11

```

	REAL FUNCTION INTERPOL(V,M,ARG)		
	DIMENSION Y(5),Y(5)		INTERPO 2
	IF(X(1),LT,X(1)) GO TO 9		INTERPC 3
	IF(ARG,LT,X(1)) GO TO 15		INTERPO 4
5	IF(ARG,GT,X(1)) GO TO 16		INTERPO 5
	DO 1 I=1,N		INTERPO 6
	IF(ARG-Y(I)) 1,2,3,30		INTERPO 7
	CONTINUE		INTERPO 8
	GO TO 15		INTERPO 9
10	IF(ARG,LT,X(1)) GO TO 15		INTERPO 10
	DO 10 I=1,N		INTERPO 11
	IF(X(I)-ARG) 10,20,10		INTERPO 12
	CONTINUE		INTERPO 13
	INTERPC=ARG		INTERPO 14
15	RETURN		INTERPO 15
	INTERPC=-ARG		INTERPO 16
	RETURN		INTERPO 17
	INTERPC=Y(I)		INTERPO 18
	RETURN		INTERPO 19
20	INTERPC=Y(1)-10*(Y(1)-Y(1-1))*ARG-X(1-1)		INTERPO 20
	1 / (Y(1)-X(1-1))		INTERPO 21
	RETURN		INTERPO 22
	END		INTERPO 23
			INTERPO 24


```

SUBROUTINE TAUN20(FREQ,NA,NT,XN20,TAU)
C SUBROUTINE TO COMPUTE TRANSMITTANCE DUE TO N2O IN PLUMES
DIMENSION XN20(20),TAU(50),FN20(23),SN20(23)
REAL INTERPO
DATA FN20/2114.,2126.,2146.,2174.,2186.,2208.,2220.,
12230.,2240.,2245.,2250.,2255.,2260.,2265.,2278.,
2275.,2280.,2300.,2340.,2350.,2355.,2360.,2365./
DATA SN20/1.5E-4,9.29E-4,1.035E-2,6.15E-1,6.4E-5,4.
15E-2,7.1E-3,5.15E-3,5.02E-3,7.2E-3,3.5E-3,2.3E-3,1.7E-3,
21.72E-3,1.4E-3,9.4E-4,5.E-4,1.E-4,MFSN20/23/
IF (NA.EQ.0) GO TO 210
IF (FREQ.GT.2355) GO TO 201
IF (FREQ.LT.2114) GO TO 203
CON=INTERPO(FN20,SN20,MFSN20,FREQ)
DO 100 I=1,NA
100 TAU(I)=1.-ERF(SQRT(CON*XN20(I)))
IF (NA.EQ.0) GO TO 210
NR=NA+1
DO 150 I=NR,NT
150 TAU(I)=TAU(NA)
210 CONTINUE
RETURN
C FREQ OUT OF RANGE OR NO ATMOSPHERE
DO 200 DO 250 I=1,NT
200 DO 250 TAU(I)=1.0
250 RETURN
END

```

	FUNCTION ERFIX		
ERF=1.0		ERF	2
IF(X.GT.1.95) RETURN		ERF	1
FACN = 1.		ERF	4
SUM = (1. - X**2)/3.		ERF	5
MMAYN = (1. - X**2)/3.		ERF	6
DO 100 N=2,MMAX		ERF	7
FACN = FACN*N		ERF	8
NN = 2*NN+1		ERF	9
100 SUM = SUM + X**NN/(FACN*MM)		ERF	10
ERF = 1.12637916709471 * SUM		ERF	11
RETURN		ERF	12
END		ERF	13
		ERF	14

[illegible]

	MP=NO=NOFLOW=8		
	REN(1)=.6		DATINIS 59
60	REN(2)=.5		DATINIS 60
	REN(3)=REN(2)		DATINIS 61
	REN(1)=-1.		DATINIS 62
	REN(2)=0.		DATINIS 63
65	NRG=<OATTA=1		DATINIS 64
	XP=PP=0.		DATINIS 65
	DX=PF=XF=0.		DATINIS 66
	NOZ=.		DATINIS 67
	AL=1000.		DATINIS 68
	XCA=21.00033		DATINIS 69
70	ZIST=900.		DATINIS 70
	NEU=2		DATINIS 71
	NDZ=3		DATINIS 72
	NOP=5		DATINIS 73
	AM(13)=2.0		DATINIS 74
75	AM(11)=2.1		DATINIS 75
	NYS		DATINIS 76
	END		DATINIS 77
			DATINIS 78

5	OVERLAY(RRHP,5,0)	PLMDEF3	2
	PROGRAM PLMDEF	PLMDEF1	3
	C PLUM DEFINITION	PLMDEF3	4
	* FEL	PLMDEF3	5
	COMMON/FEL/R2,NO,MNSO,CP(4),RX,P,NS,FZ,	PLMDEF3	6
	1 PPA,RC6,A1,CR,DX,NRO,K,TM,XCOZME,	PLMDEF3	7
	2GNB,PR(5),DPS,AM2,KERR,ORO,X(5,100),Y(5,100),NR,CNST	PLMDEF3	8
	* PLM	PLMDEF3	9
	COMMON/PLM/PLMGD(43),RCN,ST(50),NRO(50),PLN(5,30,50),MFLN,PA,P8,	PLMDEF3	10
10	1 DDDX,KDATA,ISHK,JSNK,TANG,EQR	PLMDEF3	11
	DIMENSION X(5,3,59)	PLMDEF3	12
	EQUIVALENCE (X(1,1,1),PLM(1,1,1))	PLMDEF3	13
	* FL	PLMDEF3	14
	COMMON/FL/UA,TA,XCOZA,XH2OA,BX(50)	PLMDEF3	15
15	* GEO	PLMDEF3	16
	COMMON /GEO/	PLMDEF3	17
	1 AS, AL, BA, DDS, MEN, NP,	PLMDEF3	18
	2 R1, P8, RZ, REN(10), RE, RO,	PLMDEF3	19
	3 R0Z, RP, RPZ, SC, SS, TANA,	PLMDEF3	20
20	4 TNR, TANP, XC, XEN(10), XF, XQ,	PLMDEF3	21
	5 YP, RENQ	PLMDEF3	22
	DATA NSL/0, /	PLMDEF3	23
	DATA CZMIN/.01/	PLMDEF3	24
	DATA CZMAX/.05/	PLMDEF3	25
25	C	PLMDEF3	26
	KERR=0	PLMDEF3	27
	CZMIN=.05	PLMDEF3	28
	CZMAX=.11	PLMDEF3	29
	IP=5	PLMDEF3	30
30	ARX=1,	PLMDEF3	31
	NO=0	PLMDEF3	32
	NR=0	PLMDEF3	33
	CNST=10,	PLMDEF3	34
	AXX=0,	PLMDEF3	35
35	CALL OVERLAY(RRHP,4,1)	PLMDEF3	36
	CALL PLUM	PLMDEF3	37
	IF(R6,NE,0,1) GO TO 11	PLMDEF3	38
	WRITE(6,4000)	PLMDEF3	39
40	FORMAT(/2X,27H***EXHAUST RADIUS NOT GIVEN//)	PLMDEF3	40
	GO TO 401	PLMDEF3	41
41	CONTINUE	PLMDEF3	42
	AMIX=0,	PLMDEF3	43
	QOX = 1,	PLMDEF3	44
	OXPO=.5*(R6-RZ)	PLMDEF3	45
45	ASO=NS*10+1	PLMDEF3	46
	NRX=NSO+2	PLMDEF3	47
	PCODE=FLOAT(MR)/FLOAT(NSO-1)	PLMDEF3	48
	IF(PZ,11,2200,PAI PCODE=1,	PLMDEF3	49
	JNW=1+(NSO-1)*PCODE	PLMDEF3	50
50	X(1,1,53)=AM2	PLMDEF3	51
	XK(2,1,53)=X(1,NRX)/SQRT(2403.*X(2,NRX))	PLMDEF3	52
	PZ=P	PLMDEF3	53
	NSK=5	PLMDEF3	54
	CZAV=(CZMIN+CZMAX)/2,	PLMDEF3	55
55	CZR=(CZMAX-CZMIN)/2,	PLMDEF3	56
	DX = OXPO/5,	PLMDEF3	57
	IG = 0	PLMDEF3	58

		X0=9.			PLNDEF3	59
		K=1			PLNDEF3	60
		CCJN=0.			PLNDEF3	61
		CCPN=8.			PLNDEF3	62
		CCJ=1.			PLNDEF3	63
		CCP=1P-PAI/CC1			PLNDEF3	64
		70 DPX=0FS+2*RG0/2.			PLNDEF3	65
		P=P7*DDPX*XQ			PLNDEF3	66
		C1=DPX/P			PLNDEF3	67
		Q=C1*(X(2,2)/X(1,2))			PLNDEF3	68
		KL=3			PLNDEF3	69
		AK=3			PLNDEF3	70
		CO=Q2**2			PLNDEF3	71
		X(1,2)=AINT(X(1,2))+P/2116216.			PLNDEF3	72
		DO11J=3,M2			PLNDEF3	73
		CO=CO+C*(AK+.3333)			PLNDEF3	74
		IF(J,L,I,M) GO TO 80			PLNDEF3	75
		IF(J,G,I,M) GO TO 80			PLNDEF3	76
		P=P-CCP			PLNDEF3	77
		C1=DPX/P			PLNDEF3	78
		AK=AK+1.			PLNDEF3	79
		Q=C1*(X(2,J)/X(1,J))			PLNDEF3	80
		CO=CO+Q*(AK+.3333)			PLNDEF3	81
		X(2,XL)=30*1/CO			PLNDEF3	82
		X(1,J)=AINT(X(1,J))+P/2116216.			PLNDEF3	83
		KL=KL+1			PLNDEF3	84
		IF(1,3,11,3,11,11,2			PLNDEF3	85
		DPS=DPS+SOR(1,2,2-RZ**2)/(X(5,NSO)**2-RZ**2)			PLNDEF3	86
		PS10=DPS*(NSO-1)*PCODE			PLNDEF3	87
		IG=1			PLNDEF3	88
		GO TO 70			PLNDEF3	89
		113 16=1			PLNDEF3	90
		ADK=(X(5,MR-1)-RX)/2.			PLNDEF3	91
		112 IK=1			PLNDEF3	92
		LM=1			PLNDEF3	93
		X(5,1)=X0			PLNDEF3	94
		X(5,2)=RZ			PLNDEF3	95
		IF(1,4,GE,20)LM=2			PLNDEF3	96
		IF(1,4,GE,55)LM=3			PLNDEF3	97
		IF(1,4,GE,82)LM=4			PLNDEF3	98
		L=MR+LM			PLNDEF3	99
		KL=L+1			PLNDEF3	100
		100 DO 534, IZ=KL,100			PLNDEF3	101
		514 X(5,IZ)=C.			PLNDEF3	102
		DO 127 J=2,L,LM			PLNDEF3	103
		X(1,I,K,K)=X(5,J)			PLNDEF3	104
		X(5,I,K,K)=X(1,J)			PLNDEF3	105
		IF(X(1,J),L,0.) KER2=1			PLNDEF3	106
		DO 126 I=2,4			PLNDEF3	107
		IF(X(1,I),L,0.) KER2=1			PLNDEF3	108
		126 X(1,I,K,K)=X(1,J)			PLNDEF3	109
		127 IK=IK+1			PLNDEF3	110
		NRJ(K)=IK-1			PLNDEF3	111
		IK=NRJ(K)			PLNDEF3	112
		X(1,I,K,K)=X(1,I,K,K)*1.01			PLNDEF3	113
		IF(OPD,EO,0.) DX(K)=PA			PLNDEF3	114
		ST(K)=XC			PLNDEF3	115

115	IF(DPOX,GT,0.1) KERR=200 IF(KERP,GT,0) GO TO 488 K=K+1 IF(K,GT,40) GO TO 400	PLMDEF3 116 PLMDEF3 117 PLMDEF3 118 PLMDEF3 119 PLMDEF3 120 PLMDEF3 121
128	C C EVALUATE ALL PARAMETERS AT N+1 AND STORE	PLMDEF3 122 PLMDEF3 123 PLMDEF3 124 PLMDEF3 125 PLMDEF3 126 PLMDEF3 127
125	AXX = AXX+HXY*DXPO ABX=ABX+.5 NB=1 IF(N,LE,0) GO TO 121 DAJY=JC/PJ*ADR IF(DAJX,LE,0.) GO TO 121 NJ=C 121 CONTINUE IP=2 NC=NP UP=X(I,1) UP=UP-1. UP=UP+1. DO 115 I=3,MR NRX=101 IF(X(I,1),GE,U0) GO TO 119 U0=X(I,1)-1. NC=1 119 IF(X(I,1),LE,U0) GO TO 114 UP=X(I,1) IP=1 114 IF(NRX,GT,NC+1) GO TO 116 115 CONTINUE 116 IF(K,GT,2) GO TO 125 AM2=X(I,1)/S0K7(A,X(2,1P)) GO TO 125 121 X0 = XC-DX 123 OX = OX+O0X 125 X0=X0+DX OO 10 IZ= 6,500 18 Y(I,1) = 0. IF(INSL,GT,1) GO TO 131 IF(MR,LE,NR0) GO TO 131 LO=NR/NR0+1 MR=NR/LO+1 NSQ=(NS0-2)/LO+2 NRX=(NFX-2)/LO+2 O0X=LO ORU=O0X*OPO DPS=O0X*OPS NSL=NSK OO 513 I=1,4 OO 511 J=2,MR L=LO*(J-2)+2 X(I,J)=X(I,1) IZ=NR+1 OO 502 J=17,180 182 X(I,J)=0. 503 X(I,1)=X(I,3) MR=MR+1	PLMDEF3 134 PLMDEF3 135 PLMDEF3 136 PLMDEF3 137 PLMDEF3 138 PLMDEF3 139 PLMDEF3 140 PLMDEF3 141 PLMDEF3 142 PLMDEF3 143 PLMDEF3 144 PLMDEF3 145 PLMDEF3 146 PLMDEF3 147 PLMDEF3 148 PLMDEF3 149 PLMDEF3 150 PLMDEF3 151 PLMDEF3 152 PLMDEF3 153 PLMDEF3 154 PLMDEF3 155 PLMDEF3 156 PLMDEF3 157 PLMDEF3 158 PLMDEF3 159 PLMDEF3 160 PLMDEF3 161 PLMDEF3 162 PLMDEF3 163 PLMDEF3 164 PLMDEF3 165 PLMDEF3 166 PLMDEF3 167 PLMDEF3 168 PLMDEF3 169 PLMDEF3 170 PLMDEF3 171 PLMDEF3 172

Line	Code	Text	PLNDEF3
216	12	MR=DX+5	173
217	12	DO 218 I=MR,12	174
218	12	X(1,1)=AINT(UA)*PA/1000.	175
219	12	X(2,1)=TA	176
220	12	X(3,1)=XCCZA	177
221	12	X(4,1)=XHZOA	178
222	12	CONTINUE	179
223	12	IF(NDY,EO,C.) GO TO 450	180
224	12	GO TO 123	181
225	12	JG=1	182
226	12	CZ=2.	183
227	12	IF(X,LE,D.) GO TO 128	184
228	12	Z2=Z-CX*FF/XF	185
229	12	IF(Z,LT,0.1RZ*B.)	186
230	12	PSI=0.	187
231	12	AX=C.	188
232	12	IF(INY,LT,PR) GO TO 129	189
233	12	NZ=2	190
234	12	NR=NP-1	191
235	12	LS=2	192
236	12	LF=NRX	193
237	12	IF(DPX,EG,2.) GO TO 153	194
238	12	P=Z+DPD*YO	195
239	12	IF(P,PPA152,152,154	196
240	12	P=PPA	197
241	12	DPX=ZC.	198
242	12	P=Z	199
243	12	GC=0.	200
244	12	CT=0.	201
245	12	CU=0.	202
246	12	GO TO 159	203
247	12	GC=DPDY*DY*RG8/P	204
248	12	DR(K)=P/2116.216	205
249	12	CT=GC*X(2,2)	206
250	12	CU=CT*2.17/X(1,2)	207
251	12	CT=CT/778.2/CP(1)	208
252	12	CONTINUE	209
253	12	C1=P/PG8/2.	210
254	12	O=C1*X(2,2)/X(1,2)	211
255	12	CO=(X*P/PG8)**2	212
256	12	JND=NR	213
257	12	CONTINUE	214
258	12	TH=X(2,LS)/X(2,LF+1)	215
259	12	AMH=SDPT(X(1,LS))*2/(X(2,LS)*A11)	216
260	12	IF(J3,GT,1) AMH=AMH*SQR(1/2403.)	217
261	12	J=2*J+JG-2	218
262	12	X(1,1,501)=AMH	219
263	12	AMCH=1.	220
264	12	IF(AMH,GT,.6) AMCH=1.6/(AMH*.0)	221
265	12	AMU=YO*(X(1,LS)-X(1,LF+1))*AMCH/TH**2.	222
266	12	AMU=ABS(AMU/CNST)	223
267	12	LS=LS+1	224
268	12	DO14)J=LS,LF	225
269	12	CO=CO*G*(K+.3333)	226
270	12	PSI=PSI+OPS	227
271	12	GCJ=0.	228
272	12	CP=0.	229

230	IF(J,LT,JNH) GO TO 191 IF(J,GT,JNH) GO TO 192 CCJ=CCJNH CCP=CCPNH GO TO 192	PLMDEF3 230 PLMDEF3 231 PLMDEF3 232 PLMDEF3 233 PLMDEF3 234 PLMDEF3 235
235	191 CONTINUE IF(I,BS,(PSI-PSIO)-DPS/2)* (2-JG).GE.8) GO TO 192 JNH=J CCJ=CC CCP=(P-PPI) CCPNH=CCP CCJNH=CCJ	PLMDEF3 236 PLMDEF3 237 PLMDEF3 238 PLMDEF3 239 PLMDEF3 240 PLMDEF3 241
240	192 CONTINUE P=P-CCP C1=P/RG8/2. Q=C1*(2-J)/X(1,J) AK=AK+1. C=C3+Q*(AK-.3333) CZ=D*(AK+Y(1,J)+CO/(2.*(PSI*X(2,J))**2) IF(C7.LE.C7M) GO TO 193 CZM=CZ LU=J+1	PLMDEF3 242 PLMDEF3 243 PLMDEF3 244 PLMDEF3 245 PLMDEF3 246 PLMDEF3 247
245		PLMDEF3 248 PLMDEF3 249 PLMDEF3 250 PLMDEF3 251 PLMDEF3 252 PLMDEF3 253
250	193 CONTINUE LO=J-1 CC=CC-CCJ CJ=CC*X(2,J) CX=0. DO 190 I=3,6 CX=CX+X(I,LU)-X(I,LO)*CP(I)	PLMDEF3 254 PLMDEF3 255 PLMDEF3 256 PLMDEF3 257 PLMDEF3 258 PLMDEF3 259
255	190 DO 212 I=1,6 Y(I,J-1)=Y(I,J-1)+CZ*(X(I,J)-X(I,LO))/PR(I) Y(I,J)=Y(I,J)+CZ*(X(I,LU)+X(I,LO)- 12.*X(I,J))/PR(I)+X(I,J) 200 Y(I,J+1)=CZ*(X(I,J)-Y(I,LU))/PR(I) Y(I,J)=Y(I,J)-CJ*32.17/Y(I,J) Y(I)=Y(I,J)-XC02A1/(XC02NE-XC02A) CP(I)=.25*(1.-Y(I,XI)+CP(I2)*XIX	PLMDEF3 260 PLMDEF3 261 PLMDEF3 262 PLMDEF3 263 PLMDEF3 264 PLMDEF3 265 PLMDEF3 266 PLMDEF3 267 PLMDEF3 268 PLMDEF3 269 PLMDEF3 270 PLMDEF3 271 PLMDEF3 272 PLMDEF3 273 PLMDEF3 274 PLMDEF3 275 PLMDEF3 276 PLMDEF3 277 PLMDEF3 278 PLMDEF3 279 PLMDEF3 280 PLMDEF3 281 PLMDEF3 282 PLMDEF3 283 PLMDEF3 284 PLMDEF3 285 PLMDEF3 286
260		
265		
270	1250 FA, CX*(X(2,LU)-X(2,LO))/CP(I2)/2./PR(I2) 180 CONTINUE IF(J,GE,2) GO TO 179 X(2,X,1,50)=X(2,X-2,1,50) LS=LF LF=MR JG=2 GO TO 176 179 CONTINUE CCJ=CCJNH CCP=CCPNH NOX=1. CZ=CZNV/CZM CZ=AB5(CZM-CZNV) IF(C7.LT.C7R) GO TO 181 NOX=1.2+.9*QC1/(1.+1*QC2) GO TO 123 181 NSL=NSL-1	
275		
280		
285		

00 215	I=1,4	PLNDEF3	287
00210	J=3,4	PLNDEF3	288
210	X(I,J)=Y(I,J)	PLNDEF3	289
	X(I,2)=X(I,2)+Y(I,2)	PLNDEF3	290
290	X(I,3)=X(I,3)+Y(I,2)	PLNDEF3	291
	X(I,3)=2	PLNDEF3	292
	V(I,2)=C	PLNDEF3	293
215	X(I,1)=X(I,3)	PLNDEF3	294
	X(I,2)=AINT(X(I,2)-CU)	PLNDEF3	295
295	X(I,2)=X(I,2)+CT	PLNDEF3	296
	G=ABS(X(I,2)+NR)-TA-4	PLNDEF3	297
	IF(G,GT,5) NR=NR+1	PLNDEF3	298
	IF(X,LE,NR50) GO TO 250	PLNDEF3	299
	AXX=CO-DY	PLNDEF3	300
300	NR=NR+1	PLNDEF3	301
	DOX=0	PLNDEF3	302
	IF(V(I,1)+NR*(2),LT,0.1) GO TO 216	PLNDEF3	303
	CONTINUE	PLNDEF3	304
305	IF(XO-AXY)I21,I21,78	PLNDEF3	305
	CONTINUE	PLNDEF3	306
	IF(IG,DX,LT,0.0)AND,AN2,LT,1.1 WRITE(6,2280)PA,P6,AN2	PLNDEF3	307
	CONTINUE	PLNDEF3	308
481	WRITE(6,2100) DPOX	PLNDEF3	309
	CONTINUE	PLNDEF3	310
210	FOR=41,112,400X=4F12,6)	PLNDEF3	311
220	FOR=41,114,110X,3MINCOMPATIBLE EXHAUST CONDITIONS//	PLNDEF3	312
310	110X,1=0A=F0,3,3=05=F0,3,0NHACH NO=F0,3)	PLNDEF3	313
	END		

LINE	CODE	TEXT	PLUM
5	C	OVERLAY (XOMP, 4, 1)	PLUM
10	C	PROGRAM FLIMP	PLUM
15	C	FLOW FIELD INPUT	PLUM
20	C	COMMON/LINK2/STAN(3)	PLUM
25	C	COMMON/FFL/R7, XQ, NBSO, CFI(4), RX, P, NS, PZ,	PLUM
30	C	1 PPA, RQ, A1, QP, DX, NRO, 4, TMX, XC02NE,	PLUM
35	C	20MA, PR(5), PES, R42, KERR, DRQ, X15, 100, V(5, 100), MR, CUST	PLUM
40	C	PLM	PLUM
45	C	COMMON/PLN/PLM(3, 43), RCN, ST(50), WRD(50), PLM(5, 30, 50), WFLM, PA, P8,	PLUM
50	C	1 DRY, XGATA, ISHK, JSHK, TANE, EQP	PLUM
55	C	* ATHOS	PLUM
60	C	COMMON/ATHOS/ALT, FLIN, METEC, RREC, RAMP, RANT, DELT2, THET2	PLUM
65	C	* FL	PLUM
70	C	COMMON/FL/UA, TA, XC02A, XH20A, RX(53)	PLUM
75	C	* GEO	PLUM
80	C	COMMON /GEO/	PLUM
85	C	1 A6, AL, BB, DQS, NEM, MP,	PLUM
90	C	2 R1, R83, R87, REM(10), RF, RO,	PLUM
95	C	3 R2, RP, RP2, SO, SS, TANA,	PLUM
100	C	4 TND, TNP, XC, XEN(10), XF, XO,	PLUM
105	C	5 XP, XEND	PLUM
110	C	DIMENSION PS(1, 10), IAT(1, 10), XC02(1, 10), XH20(1, 10), U8(1, 10), TS(1, 10)	PLUM
115	C	EQUIVALENCE (TS(1, 1), PLM(1, 1), IAT(1, 1), U8(1, 1), PLM(2, 1), IAT(1, 1))	PLUM
120	C	EQUIVALENCE (XC02(1, 1), PLM(3, 1), IAT(1, 1), XH20(1, 1), PLM(4, 1), IAT(1, 1))	PLUM
125	C	NAMLIST/PLUMIN/ RPN, RSN, RP, KOATA,	PLUM
130	C	1 TANE, EOP, XC02, XC02A, XH20A,	PLUM
135	C	2 UA, TAT, P8, PG, UA, TA, PA	PLUM
140	C	3 GIVE RPN, RCN, XP, RP, KOATA ONLY IF "INPUT" IS NOT USED.	PLUM
145	C	4 GIVE XC02, UA, ONLY IF XH20, TST, P8, PG, ARE ALSO GIVEN.	PLUM
150	C	5 GIVE UA, TA, PA XC02A, XH20A ONLY IF ALTPM IS NOT GIVEN IN	PLUM
155	C	"INPUT" & DEFAULT IS NOT DESIRED.	PLUM
160	C	IF XC02 ONLY IS OMITTED, XC02 & XH20 WILL BE CALCULATED.	PLUM
165	C	GIVE TANE & OR EOP ONLY IF DEFAULT VALUES ARE NOT DESIRED.	PLUM
170	C	INITIALIZE	PLUM
175	C	00 100 IZ=1, 50	PLUM
180	C	8X(IZ)=0.	PLUM
185	C	ST(1)=XO	PLUM
190	C	00 300 IZ=1, 1000	PLUM
195	C	300 X(IZ, 1)=6.	PLUM
200	C	TA=519.	PLUM
205	C	NBS=200	PLUM
210	C	PQ=P5	PLUM
215	C	KERR=0	PLUM
220	C	XH20A=.00033	PLUM
225	C	XC02A=.00033	PLUM
230	C	EQR=.250	PLUM
235	C	TANE=.9, 0	PLUM
240	C	TMW=.30, 9665	PLUM
245	C	00 311 I=1, 100	PLUM
250	C	XC02(1)=XC02A	PLUM
255	C	XH20(1)=XH20A	PLUM
260	C	RPN=5CN(2)	PLUM
265	C	QSN=5CN(3)	PLUM

Line	Code	Text	PLUM	PLUM
68	RG=53.38		PLUM	59
	GM=1.73		PLUM	60
	PR11=1.		PLUM	61
	PR12=.5		PLUM	62
	PR13=1.		PLUM	63
	PR14=1.		PLUM	64
65	PR15=1.		PLUM	65
	DOS=.025		PLUM	66
	CP(1)=.25		PLUM	67
	CP(2)=0.		PLUM	68
	CP(3)=.31		PLUM	69
	CP(4)=5.14		PLUM	70
70	UA=1.		PLUM	71
	PEAN(6,PLUMIN)		PLUM	72
	IF(PLUM,ED-D) WRITE(6,PLUMIN)		PLUM	73
	NR=SN*10./RPN01,005		PLUM	74
	R0=CON=RON		PLUM	75
75	P=P0		PLUM	76
	CALL THRUST		PLUM	77
	D0 360 J=1,11		PLUM	78
	UB(J)=PLMGD(121)		PLUM	79
80	369 TBT(J)=PLMGD(17)		PLUM	80
	P0=PLMGD(125)		PLUM	81
	D0 361 J=12,48		PLUM	82
	UB(J)=PLMGD(123)		PLUM	83
	TBT(J)=PLMGD(161)		PLUM	84
	MR=NR+1		PLUM	85
85	D0 362 J=MR,100		PLUM	86
	UB(J)=UA		PLUM	87
	362 TBT(J)=RMT		PLUM	88
	302 CONTINUE		PLUM	89
90	IF(P3.E0.0.) P8=PA		PLUM	90
	IF(IN3.GT.400) NBS=600		PLUM	91
	IF(FC02(11).LE.1.1*XC02A) CALL CHEM		PLUM	92
	IF(FC02(11).LE.1.1*XC02A) GO TO 999		PLUM	93
	RX=RCN		PLUM	94
	RX=RP		PLUM	95
95	RZ=RP		PLUM	96
	RF=RP		PLUM	97
	XF=XP		PLUM	98
	A1=G*G+32.17*RG8		PLUM	99
	A=PLMGD(124)		PLUM	100
100	CP(3)=CP(3)*46.01/29.17		PLUM	101
	CP(4)=CP(4)*2.616/29.17		PLUM	102
	IF(UA.LT.(-.01*UB(11))) UA=.01*UB(11)		PLUM	103
	NBSO=NBS		PLUM	104
	IF(IN3.GT.111) NO=1		PLUM	105
105	NP0=NR-1		PLUM	106
	NS=6		PLUM	107
	2 IF(IN3.NS.LT.75) GO TO 6		PLUM	108
	NS=NS-1		PLUM	109
	GO TO 2		PLUM	110
110	6 NR=NR+NS-NS+1		PLUM	111
	NSU=NS+10+1		PLUM	112
	IG=J		PLUM	113
	D0 3 J=1,NBO		PLUM	114
	K=K*11-J-IG		PLUM	115

LINE	CODE	TEXT	PLUME
115		M=K20+2-J	116
		AK=0.	117
		DO 7 L=1,NS	118
		LK=K+1-L	119
		UB(LK)=U5	120
120		UB(LK)=U5*(1.-AK)+AK*UB(M-1)	121
		TAT(LK)=TAT(M)*(1.-AK)+AK*TAT(M-1)	122
		XC02(LK)=XC02(M)*(1.-AK)+AK*XC02(M-1)	123
		XM2C(LK)=XM2C(M)*(1.-AK)+AK*XM2C(M-1)	124
		AK=AK+1/NS	125
125		3 IG=IG+NS-1	126
		PPA=2116.216*PA	127
		P=2116.216*P1	128
		IF (PPA,EO,C,1) PD=PA	129
		PPQ=2116.216*PQ	130
		DPQY=PPQ*P1/12.*R3	131
130		IF (D.*PPA+ARGSDOPQX)/P,ALT,0.81) OPDX=0.0	132
		P1=PPQ	133
		TS(1)=TAT(1)-A*U2(1)**2	134
		AM2=SQRT(U2(1)**2+1/TS(1))	135
		WRITE(6,1020)	136
135		RAD=P2	137
		DX=(PA-P2)/(INS*10.)	138
		DO 4 I=1,NS	139
		RAJ=RAD+DP*NS	140
140		WRITE(6,3200)	141
		3200 FORMAT(1X,21H** AMBIENT CONDITIONS/)	142
		WRITE(6,1000) RAD,UA,TA,XC02A,XM20A	143
		WRITE(6,3300) P,PA,CP(1),R,CB,CM,AM2	144
145		3300 FORMAT(1X,13H** INPUT PARAMETERS//	145
		130X,17HPLUME AMBIENT//	146
		25X,17HPRESSURE, P,2(F13,31,7H ATMOS./	147
		35X,17HSPECIFIC HEAT, CP,F13,3,9H BTU/LB-F/	148
		45X,17HGRAS CONSTANT, R ,F13,3,5H FT/F/	149
		55X,17HMP. HT. RATIO ,F13,3/	150
		65X,17HMECH NUMBER ,F13,3/	151
150		IF (NR,LT,NS*10+2) GO TO 5	152
		WRITE(6,3400) P2	153
3400		FORMAT(5X,17HSECONDARY PRESS.=F13,3,7H ATMOS.)	154
		NRQ=NR/2+5	155
155		ORO=OR	156
		EVALUATE PSI(OR)	157
		Q=U5(1)/TS(1)	158
160		PS(1)=Q.	159
		AX=PPQ/P	160
		DO 11 J=2,NS	161
		IF (J,GT,10*NS+1) A=PLMCO(29)	162
		TS(J)=TAT(J)-UB(J)*2*A	163
165		PS(J)=PS(J-1)+2*13.*DN*OR)	164
		RNE=V*CR	165
		Q=U5(J)/TS(J)	166
		IF (J,GT,NS*10+2) Q=Q*AY	167
170		PS(J)=PS(J)+Q*(1.*KN-OR)	168
		DO 15 J=1,NS	169
		PS(J)=SQRT(PS(1))	170
		18 PS(J)=PS(J)+Q*(1.*KN-OR)	171
		19 PS(J)=SQRT(PS(1))	172

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      OPS=PS(SIN(SO1/(INS*101)
      J1=2
      L=J
      Z=PS(J1)
      Z=Z+OPS
      IF(L,GE,501 GO TO 53
      L=L+1
      DO J1=J1,NP
      IF(PS(J1,GT,7-OPS/1008.) GO TO 48
      CONTINUE
      GO TO 50
40 J1=J
      G=1-PS(J-1)/1/PS(J)-PS(J-1))
      M=L+1
      G1=1-G
      X(1,*)=G*U8(J)+G1*U9(J-1)
      X(2,*)=G*TS(J)+G1*TS(J-1)
      X(3,*)=G*XC2(J)+G1*XC2(J-1)
      X(4,*)=G*XM2(J)+G1*XM2(J-1)
      AJ=J
      TAT(X)=RZ+RR*(G*AJ+G1*(AJ-1.))
      GO TO 20
      NP=L
      M=L+5
      DO 55 NR=NP,M
      X(1,*)=X(1,*)+PA/1000.
      X(2,*)=TA
      X(3,*)=XC2A
      X(4,*)=XM20A
      CONTINUE
55 GO 63 I=1,4
      X(1,*)=X(1,*)
      X(2,*)=0.
      X(3,*)=0.
      X(4,*)=0.
      GAM=TA/(XM2*TS(1))
      CNST=194.
      IF(GAM=5.,1500,500,503
      CNST=10.
      IF(GAM=.21503,503,501
      CNST=(115.*GAM+7.)/3.
      CONTINUE
      CNST=CNST/2.8
      GO TO 403
      FORMAT(1H1/2X,19H** FLOW FIELD INPUT//
      19X,53H RADIUS VELOCITY TEMPERATURE XC2
      29X,32H(FEET) IF1/SEC1 TDEC R0//)
      210 FORMAT(4X,F12.4,12F12.2,3F12.6)
      220 WRITE(6,9999)
      9999 STOP
      FORMAT(10X,40H INCOMPLETE INPUT - CONCENTRATION ERROR. )
      400 CONTINUE
      END

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A-90

PLUME	173
PLUME	174
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PLUME	223
PLUME	224
PLUME	225

SUBROUTINE CHEM					
		SIMPLE CHEMICAL ANALYSIS TO YIELD THE COMPOSITION AND BASIC			
		THERMODYNAMIC PROPERTIES OF THE CORE NOZZLE EXIT PLANE EXHAUST			
		GAS ASSUMING IDEAL COMBUSTION.			
		SET.			
5	C	FUEL		CHEM	2
	C	COMMON/FEL/RZNO,NESQ,CP(4),EX,P,NS,PZ,		CHEM	3
	C	1 PPA,RQ,AL,OR,OX,NPO,K,TM,XCO2NE,		CHEM	4
	C	2GMS,PR(5),DPS,A42,KEFR,DRO,X15,100),Y(5,100),MR,CNST		CHEM	5
10	C	PLM		CHEM	6
	C	COMMON/PLM/PLM2D(43),RCN,ST(5),NEQ(50),PLMIS(31,52),NFLW,PA,PI,		CHEM	7
	C	1 OPGX,PCATA,ISPK,JSHK,TANE,EOR		CHEM	8
	C	A LIGHT KEROSENE FUEL IS ASSUMED TO BE BURNED WITH 800% SET,		CHEM	9
15	C	THEORETICAL AIR FLOW. IE, TANE = 9.8 AND EOR = 0.25,		CHEM	10
	C	DIMENSION SPW(7),SPMH(7),CPE(7),XCO2(100),X420(100)		CHEM	11
	C	EQUIVALENCE XCO2(1),PLMIS(1),PLMIS(1),XCO2(1),PLMIS(1),1,1)		CHEM	12
20	C	DATA SPW/44.013,18.008,20.316,39.944,32.008,12.016,2.016/		CHEM	13
	C	DATA CPE/31.55,29.17,28.40,3.8/		CHEM	14
	C	CHEM ENGR'S HNDOK, 3RD ED, 2ND IMP, 1950		CHEM	15
	C	SPW(1)=XCO2(100)		CHEM	16
	C	SPW(2)=X420(100)		CHEM	17
25	C	SPW(3)=78001		CHEM	18
	C	SPW(4)=609324		CHEM	19
	C	SPW(5)=209495		CHEM	20
	C	TM=1,		CHEM	21
	C	TMV=1,		CHEM	22
30	C	DO 1 I=1,5		CHEM	23
	C	TMV=TMV+SPW(I)		CHEM	24
	C	1 TM=TM+SPMH(I)*SPMH(I)		CHEM	25
	C	DO 1 I=1,5		CHEM	26
35	C	SPW(I)=SPW(I)/TMV		CHEM	27
	C	CH2K=SPW(5)*TANE/(1.5*TANE+.5)		CHEM	28
	C	SPW(1)=CH2K*MAX(1,EOR-1,0)		CHEM	29
	C	SPW(7)=SPW(5)*(TANE+1)/TANE		CHEM	30
	C	SPW(5)=SPW(5)*MAX(1,1-EOR,0)		CHEM	31
	C	SPW(2)=CH2K*(TANE+1)*EOR/TANE+SPW(2)		CHEM	32
40	C	SPW(1)=CH2K*EOR+SPW(1)		CHEM	33
	C	FARW=CH2K*EOR		CHEM	34
	C	FARW=FARW-(SPMH(6)*(TANE+1)*SPMH(7)/TANE)/TMV		CHEM	35
	C	PLMIS(12)=FARW		CHEM	36
45	C	TCPE=0.0		CHEM	37
	C	TMV=1,		CHEM	38
	C	TM=1,		CHEM	39
	C	DO 1 I=1,7		CHEM	40
	C	TMV=TMV+SPW(I)		CHEM	41
50	C	SPW=SPW(I)*SPW(I)		CHEM	42
	C	TM=TM+SPW		CHEM	43
	C	11 TCPE=TCPE+SPW*CP(I)		CHEM	44
	C	TMV=TM+SPW(6)		CHEM	45
	C	TM=TM+TMV		CHEM	46
	C	TCPE=TCPE/TMV		CHEM	47
55	C	DO 1 I=1,7		CHEM	48
	C	100 SPW(I)=SPW(I)/TMV		CHEM	49
	C	TMV=1,		CHEM	50
	C			CHEM	51
	C			CHEM	52
	C			CHEM	53
	C			CHEM	54
	C			CHEM	55
	C			CHEM	56
	C			CHEM	57
	C			CHEM	58

	RG0=1565.8146/TM	CHEM	59
	CP(1)=TCPF/TM	CHEM	60
60	GM0=1.4/1.0-1.98580/TCPFI	CHEM	61
	CP(2)=CP(1)	CHEM	62
	DO 101 J=1,11	CHEM	63
	XC(21,J)=SPV(1)	CHEM	64
	TM20(1)=SPV(2)	CHEM	65
65	XC02=CE=SPV(1)	CHEM	66
	RETURN	CHEM	67
	END	CHEM	68

115	113 TAC=374.7 GO TO 10	THRUST	116
	114 TAC=374.7-31602*(H-12894.)	THRUST	117
	GO TO 10	THRUST	118
	115 TAC=374.7	THRUST	119
	GO TO 10	THRUST	120
120	116 TAC=374.7+00051.3*(H-18587.)	THRUST	121
	GO TO 10	THRUST	122
	117 TAC=365.7-0011355*(H-22229.)	THRUST	123
	GO TO 10	THRUST	124
125	17 TA=3	THRUST	125
	C	THRUST	126
	C	THRUST	127
	C	THRUST	128
	C	THRUST	129
	IF (H-11909.1110.118.106	THRUST	130
130	118 TAC=374.7-31602*(H-12894.)	THRUST	131
	GO TO 10	THRUST	132
	119 TAC=374.7+00051.3*(H-18587.)	THRUST	133
	GO TO 10	THRUST	134
135	120 TAC=374.7+00052019*(H-20200.)	THRUST	135
	GO TO 10	THRUST	136
	C	THRUST	137
	C	THRUST	138
	C	THRUST	139
	C	THRUST	140
140	210 CONTINUE	THRUST	141
	PAGE=PAC	THRUST	142
	DELAM=PA/14.690	THRUST	143
	THLAE=TA/518.648	THRUST	144
	IF (JET-2155.51.50	THRUST	145
145	50 CONTINUE	THRUST	146
	FOR = 1.	THRUST	147
	WASAC = 0.	THRUST	148
	51 RAMTR=1.+(GAMS-1.1)*FLTM*FLTM/2.	THRUST	149
	FCAMS=(GAMS-1.1)/GAMS	THRUST	150
	RAMPR=(RAMTR*(1./FGAMS))*RREC	THRUST	151
150	DEL12=DELAM*RAMPR	THRUST	152
	THE12=THEAM*RAMTR	THRUST	153
	SRHT2=SRHT1*THE12	THRUST	154
	UA=FLTM*SRHT1/(CPS*TA)	THRUST	155
155	RAM1=518.648*DEL12	THRUST	156
	RAMP=14.690*DEL12	THRUST	157
	IF (INOP152.52.53	THRUST	158
	52 TSFC=TSFC/SRT412	THRUST	159
	FN = FN /DEL12	THRUST	160
	FNRT=FNRT/DEL12	THRUST	161
160	EPK=EPK/(PA*PR*PAMB)	THRUST	162
	FPK=FPK/(PA*PR*PAMB)	THRUST	163
	ITPA = ITPA/PA*PR	THRUST	164
	ITSA = ITSA/PA*PR	THRUST	165
165	WAPAC = WAPAC*SRHT2/DEL12	THRUST	166
	WASAC = WASAC*SRHT2/DEL12	THRUST	167
	IF (JET.NE.2) FPR=1.	THRUST	168
	53 CONTINUE	THRUST	169
	WP=WAPAC*DEL12/SRHT2	THRUST	170
	WS=WASAC*DEL12/SRHT2	THRUST	171
170	PNRT = FN*133./FNRT	THRUST	172
	FN = FN*DEL12	THRUST	173

	MF=TSFC*FA*SRMT2	THRUST	173
	FOR=1.	THRUST	174
	CALL CHEM	THRUST	175
175	WSTOIC=WP*3600.*PLMGO(12)	THRUST	176
	FOR=WF/WSTOIC	THRUST	177
	221 CONTINUE	THRUST	178
	CALL CHEM	THRUST	179
180	GAMP=G*5	THRUST	180
	FGAMP=(GAMP-1.)/GAMP	THRUST	181
	ZOPP=CP(1)	THRUST	182
	RP=0.9	THRUST	183
	CP=ZOPP*25.29*26	THRUST	184
	W=WD+WF/3(03)	THRUST	185
185	WPP=EP*WAMP	THRUST	186
	PT=PNR*FAM8	THRUST	187
	CNT=(GAMP+1.)/2.	THRUST	188
	CNPR=CNTP*(1./FGAMP)	THRUST	189
	IF(PNPR.GE.CNPR)PNPR=CNPR	THRUST	190
190	PNTR=PNPR*FGAMP	THRUST	191
	PNMQ=SCOT(2.)*(PNTR-1.)/(GAMP-1.))	THRUST	192
	SNPR=FP*WAMP	THRUST	193
	PTS=SNPR*FAM8	THRUST	194
	CSP=(FGAMP+1.)/2.)*(1./FGAMP)	THRUST	195
195	IF(SNPR.GE.CSP)SNPR=CSP	THRUST	196
	SNP=SNPR*FGAMP	THRUST	197
	SNMCH=SCOT(2.)*(SNR-1.)/(GAMP-1.))	THRUST	198
	PNM=(GAMP-1.)*CSP*TPN*THET2/PNTR	THRUST	199
	IF(PT.NE.PNTSY) = 510.608	THRUST	200
200	SNM=(GAMP-1.)*CSP*TPN*THET2/SNP	THRUST	201
	PNMEL=FN*CH*SCOT(PNM)	THRUST	202
	SNMEL=SNMCH*SCOT(SNTM)	THRUST	203
	TP=TPN*THET2	THRUST	204
	TIS=TPN*THET2	THRUST	205
205	REC=REC*100.	THRUST	206
	DAV(1)=10M	THRUST	207
	DAV(2)=10M	THRUST	208
	DAV(3)=10M	THRUST	209
	WICOW(1)=10M	THRUST	210
210	WICOW(2)=10M	THRUST	211
	WICOW(3)=10M	THRUST	212
	WICOW(4)=10M	THRUST	213
	PA=0.5	THRUST	214
	PS=PTP/PNPR/14.6959	THRUST	215
215	WICOW(5)=10M	THRUST	216
	IF(TI.LT.1600.AND.XH2O.AGT.0.0085) WICOW=1	THRUST	217
	WICOW(6)=10M	THRUST	218
	WICOW(7)=10M	THRUST	219
	WICOW(8)=10M	THRUST	220
220	WICOW(9)=10M	THRUST	221
	WICOW(10)=10M	THRUST	222
	WICOW(11)=10M	THRUST	223
	WICOW(12)=10M	THRUST	224
225	WICOW(13)=10M	THRUST	225
	WICOW(14)=10M	THRUST	226
	WICOW(15)=10M	THRUST	227
	WICOW(16)=10M	THRUST	228
	WICOW(17)=10M	THRUST	229

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230      PLNGJ(15)=PTP      THRUST 230
      PLNGJ(16)=PTS      THRUST 231
      PLNGJ(17)=TTP      THRUST 232
      PLNGJ(18)=TTS      THRUST 233
      PLNGJ(19)=FTS      THRUST 234
      PLNGJ(20)=FNMACH   THRUST 235
      PLNGJ(21)=CNMACH   THRUST 236
      PLNGJ(22)=CNVEL    THRUST 237
      PLNGJ(23)=SNVEL    THRUST 238
      PLNGJ(24)=PB       THRUST 239
      PLNGJ(25)=PTS/SNPR/14.69594 THRUST 240
      PLNGJ(26)=RP       THRUST 241
      PLNGJ(27)=RS       THRUST 242
      PLNGJ(28)=EGAMP/(64.34*RP) THRUST 243
      PLNGJ(29)=EGAMS/(64.34*RS) THRUST 244
      WRITE(16,24)       THRUST 245
      IF(ALT,GE,1.E7) GO TO 23
      WRITE(16,25) ALT,DAY(=ETEC+21.24H20A
      WRITE(16,26) (VICONID),I=NCGM,NCOMI
      23 WRITE(16,27) FLTH,PA45,TA,UA
      WRITE(16,28) EOP
      IF(EOP,GT,1.05) WRITE(16,40) FCR
      24 FORMAT(//23H** FLIGHT CONDITIONS **I
      25 FORMAT(//5X,*,ALTITUDE IS *,F6.0,*, FEET,*,25X,*,WEATHER IS ICAD MIL S
      *TO 210 *,R13,*,AY*,/10X,*, WITH *,F10.6,*, WATER CONTENT,*,I
      26 FORMAT(15X,*,VISIBLE CONTRAIL IS *,2A10)
      27 FORMAT(15X,*,CASE MACH NUMBER IS *,F4.2,*, AT AMBIENT*,*/10X,*,PRESSUR THRUST
      *E OF *,F6.2,*, PSTA,*/10X,*,TEMPERATURE OF *,F5.0,*, DEGR,*/10X,
      *VELOCITY OF *,F5.0,*, FT/SEC,*///)
      28 FORMAT(15X,*,ENGINE IS RUNNING WITH A FUEL EQUIVALENCE RATIO (EOP) O
      *F *,F6.3//)
      50 FORMAT(30X,*SMOKEY ENGINE OPERATION -> EOP. *,G14.4)
      RETURN
      END

```

[illegible]

	00 22 K=1.49	PLM0M3	59
	J=MIN(130,NRO(K))+1	PLM0M3	60
68	NRO(K)=J	PLM0M3	61
	IF(K.EQ.49) NRO(K)=NFO(K-1)	PLM0M3	62
	J=MIN(30,NRO(K))	PLM0M3	63
	00 22 J=J+JE	PLM0M3	64
	PLM(1,J,K)=1.2*PLM(1,NB,49)	PLM0M3	65
65	IF(K.EQ.49) PLM(1,J,K)=PLM(1,J,K-1)	PLM0M3	66
	00 22 I=2.5	PLM0M3	67
	22 PLM(I,J,K)=PLM(I,JREF,1)	PLM0M3	68
	101 CONTINUE	PLM0M3	69
	20 110 K=1.49	PLM0M3	70
70	J=J+N*2(K)	PLM0M3	71
	70111 J=2.5E06	PLM0M3	72
	VEL=PLM(5,1,K)-1.	PLM0M3	73
	VEL=PLM(5,J,K)	PLM0M3	74
	IF(VEL.GE.VEL160 TO 118	PLM0M3	75
75	IF(J.LE.2) GO TO 111	PLM0M3	76
	110 CONTINUE	PLM0M3	77
	111 K=K-1	PLM0M3	78
	XC=ST(K)	PLM0M3	79
	REN(101)=REN	PLM0M3	80
80	RB=REN	PLM0M3	81
	RG=REN	PLM0M3	82
	AL=ST(48)	PLM0M3	83
	NB=N*2(49)-2	PLM0M3	84
	REND=PLM(1,NB,48)	PLM0M3	85
	TN3=(REND-POI)/AL	PLM0M3	86
85	WRITE(16,90111) RB,NC,REND,AL	PLM0M3	87
	90111 FORMAT(5X,4H RB=E8.3,4H NC=E8.3,6H REND=E8.3,4H AL=E8.3)	PLM0M3	88
	C * * PLUME GAS DATA IS IN CORE * *	PLM0M3	89
90	IFILE=KDATA/1030	PLM0M3	90
	KDATA=KDATA-IFILE*1000	PLM0M3	91
	IPNCH=KDATA/100	PLM0M3	92
	KDATA=KDATA-IPNCH*100	PLM0M3	93
95	IPRNT=KDATA/10	PLM0M3	94
	IPLOT=KDATA-IPRNT*10	PLM0M3	95
	IF(IFILE.NE.1) GO TO 1008	PLM0M3	96
	WRITE(19) (PLMGO(I),I=1,7644)	PLM0M3	97
	1008 IF(IPNCH.NE.1) GO TO 1001	PLM0M3	98
100	PUNC=9013.(PLMGO(1),I=1,7644)	PLM0M3	99
	1001 IF(IPRNT.NE.1) GO TO 1010	PLM0M3	100
	CALL PLMPRNT	PLM0M3	101
105	1010 KDATA=IPLOT	PLM0M3	102
	CALL PLMPLOT	PLM0M3	103
	END	PLM0M3	104
		PLM0M3	105
		PLM0M3	106

	C	SUBROUTINE PLMPLT		PLMPLT	2
	C	OBJECTIVE: TO PLOT ON THE PRINTER FROM TABLE PLW ANY ARGUMENT(IPILOT)		PLMPLT	3
	C	FROM 2 THROUGH 5 OR ALL ARGUMENTS 2 THROUGH 5 (IPILOT=0), OR		PLMPLT	4
5	C	NONE AT ALL (IPILOT=1).		PLMPLT	5
	C			PLMPLT	6
	C			PLMPLT	7
	C	PLNST * * * PLUNE STRUCTURE DATA * *		PLMPLT	8
	C	COMMON/PLMP/PLMG(43),RCN,ST(50),NRD(50),PLW(5,30,50),NFLW,PA,PB,		PLMPLT	9
	C	1 OPD,KOATA,ISKK,JSMK,TANE,ZENQ		PLMPLT	10
10	C	INTEGER SYH(133),DM(7),LAB(11)		PLMPLT	11
	C	DIMENSION FMTV(13),AKSF(6),VAR(4),PMS(4)		PLMPLT	12
	C	OATF ENY/LIN(2)*4 > .1H ,1CH,* > P > *.1H ,18H,* > L > *,		PLMPLT	13
	C	.1H ,1OH,* > U > *.1H ,1CH,* > M > *.1H ,1OH,* > E > *.1H ,2H)/		PLMPLT	14
	C	DATA PA,G/4HE5,E,SHE1C,.4,NWF5,O/		PLMPLT	15
15	C	DATA VAR/LSTAT TEMP ,1CH GZ CONC ,1CH H2O CONC ,1CH VELOCITY /		PLMPLT	16
	C	DATA LAB/IPA,1H2,1M3,1ML,1M5,1MF,1H7,1HS,1H9,1HP,1H /		PLMPLT	17
	C	DATA DM/1M ,1HE,1H4,1HU,1HL,1HP,1H /		PLMPLT	18
	C	DATA EXP/1CM(3),13CA1/		PLMPLT	19
20	C	DATA LPX,CAY,LGN/2*,119,11/		PLMPLT	20
	C	IPICT=XDATA		PLMPLT	21
	C	JIG=IPIOT		PLMPLT	22
	C	IF(IPILOT.GT.1) GO TO 0011		PLMPLT	23
	C	JIG=1		PLMPLT	24
22	C	0010 JIG=JIG+1		PLMPLT	25
	C	IF(JIG.GT.5) IPILOT=1		PLMPLT	26
	C			PLMPLT	27
	C	IF(IPILOT.NE.1) GO TO 0011		PLMPLT	28
30	C	GO TO 2302		PLMPLT	29
	C	* FILL & WRITE PLOT HEADER *		PLMPLT	30
	C	CONTINUE		PLMPLT	31
	C	AMX=PLMJG(1,1)		PLMPLT	32
	C	AMN=PLMJG(1,49)		PLMPLT	33
35	C	AINC=(AMX-AMN)/5.0		PLMPLT	34
	C	AMN=AMN+.5*AINC		PLMPLT	35
	C	J=JIG-1		PLMPLT	36
	C	DO 0909 IFILL=2,12,2		PLMPLT	37
	C	I=IFILL/2		PLMPLT	38
	C	ANS(I)=AMN+AINC*(6-I)		PLMPLT	39
40	C	FMTV(IFILL)=RNG(I)		PLMPLT	40
	C	WRITE(6,'2009')		PLMPLT	41
	C	WRITE(6,'0099') VARI(J)		PLMPLT	42
	C	WRITE(6,'9000') RCN		PLMPLT	43
	C	WRITE(6,'FMTVIAN'		PLMPLT	44
45	C	DO 0903 NSF=2,40		PLMPLT	45
	C	AKSF=PLMHJG(1,NSF)		PLMPLT	46
	C	IF(AKSFALE.AMN+.5*AINCI GO TO 0030		PLMPLT	47
	C	CONTINUE		PLMPLT	48
50	C	* SET SCALES L & K *		PLMPLT	49
	C	SOLX=SYINSFI/KMX		PLMPLT	50
	C	SOLL =SCLK/.60		PLMPLT	51
	C	LGN=RCM/SCLL*.1.0		PLMPLT	52
	C	IF(LCN.LE.1) GO TO 0004		PLMPLT	53
55	C	SCLL=RCN/(LCN-1)		PLMPLT	54
	C	SCLK=.P*SCLL		PLMPLT	55
	C	NSF=NSF+1		PLMPLT	56
	C			PLMPLT	57
	C			PLMPLT	58

60	0004	IF(LCM,GE,5) GO TO 0003	PLMPLT	59
		NSF=NSF-2	PLMPLT	60
		GO TO 0030	PLMPLT	61
	0003	IF(NSF,EO,40) GO TO 0100	PLMPLT	62
		IF(LCM,LE,15) GO TO 0300	PLMPLT	63
		NSF=NSF+5	PLMPLT	64
		IF(NSF,GT,40) NSF=40	PLMPLT	65
65		GO TO 0030	PLMPLT	66
	0100	NSF=NSF+1	PLMPLT	67
		IF(LCM,LE,NSF) NSF=1	PLMPLT	68
		GO TO 0030	PLMPLT	69
		IF(LCM,GT,20) GO TO 0100	PLMPLT	70
70		CONTINUE	PLMPLT	71
	0100	CONTINUE	PLMPLT	72
		IF(LCM,LE,20) GO TO 0100	PLMPLT	73
		IF(LCM,LE,20) GO TO 0100	PLMPLT	74
		IF(LCM,LE,20) GO TO 0100	PLMPLT	75
75		IF(LCM,LE,20) GO TO 0100	PLMPLT	76
		IF(LCM,LE,20) GO TO 0100	PLMPLT	77
		IF(LCM,LE,20) GO TO 0100	PLMPLT	78
		IF(LCM,LE,20) GO TO 0100	PLMPLT	79
		IF(LCM,LE,20) GO TO 0100	PLMPLT	80
		IF(LCM,LE,20) GO TO 0100	PLMPLT	81
		IF(LCM,LE,20) GO TO 0100	PLMPLT	82
80		IF(LCM,LE,20) GO TO 0100	PLMPLT	83
		IF(LCM,LE,20) GO TO 0100	PLMPLT	84
		IF(LCM,LE,20) GO TO 0100	PLMPLT	85
		IF(LCM,LE,20) GO TO 0100	PLMPLT	86
		IF(LCM,LE,20) GO TO 0100	PLMPLT	87
		IF(LCM,LE,20) GO TO 0100	PLMPLT	88
		IF(LCM,LE,20) GO TO 0100	PLMPLT	89
		IF(LCM,LE,20) GO TO 0100	PLMPLT	90
		IF(LCM,LE,20) GO TO 0100	PLMPLT	91
		IF(LCM,LE,20) GO TO 0100	PLMPLT	92
		IF(LCM,LE,20) GO TO 0100	PLMPLT	93
		IF(LCM,LE,20) GO TO 0100	PLMPLT	94
		IF(LCM,LE,20) GO TO 0100	PLMPLT	95
		IF(LCM,LE,20) GO TO 0100	PLMPLT	96
		IF(LCM,LE,20) GO TO 0100	PLMPLT	97
		IF(LCM,LE,20) GO TO 0100	PLMPLT	98
		IF(LCM,LE,20) GO TO 0100	PLMPLT	99
		IF(LCM,LE,20) GO TO 0100	PLMPLT	100
95		IF(LCM,LE,20) GO TO 0100	PLMPLT	101
		IF(LCM,LE,20) GO TO 0100	PLMPLT	102
		IF(LCM,LE,20) GO TO 0100	PLMPLT	103
		IF(LCM,LE,20) GO TO 0100	PLMPLT	104
		IF(LCM,LE,20) GO TO 0100	PLMPLT	105
		IF(LCM,LE,20) GO TO 0100	PLMPLT	106
		IF(LCM,LE,20) GO TO 0100	PLMPLT	107
		IF(LCM,LE,20) GO TO 0100	PLMPLT	108
		IF(LCM,LE,20) GO TO 0100	PLMPLT	109
		IF(LCM,LE,20) GO TO 0100	PLMPLT	110
		IF(LCM,LE,20) GO TO 0100	PLMPLT	111
		IF(LCM,LE,20) GO TO 0100	PLMPLT	112
		IF(LCM,LE,20) GO TO 0100	PLMPLT	113
		IF(LCM,LE,20) GO TO 0100	PLMPLT	114
		IF(LCM,LE,20) GO TO 0100	PLMPLT	115

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115	DO 0111 LEV=1.6 AT=AMN+AINC*(LEV-1) IF (A.LT.AT) GO TO 1000 B111 CONTINUE C FALLS OUT WITH A>AMN	PLMPLT 116 PLMPLT 117 PLMPLT 118 PLMPLT 119 PLMPLT 120 PLMPLT 121 PLMPLT 122 PLMPLT 123 PLMPLT 124 PLMPLT 125 PLMPLT 126 PLMPLT 127
120	LEV=7 AT=AT+AINC 1000 IF (KS.GT.1) GO TO 1001 LEVMO=LEV 1001 STAT=STA IF (LEV.EQ.LEVMO) GO TO 1010 IF (LEVMO.LT.LEV) AT=AT+AINC IF (A-AMN)/AINC.LT.0.1) AMO=A-.1*AINC OK=AT-AMO/(A-AMO) IF (LEVMO.EQ.0) OK=0.0 IF (OK.LE.0.0) OK=0.0 IF (OK.GE.1.0) OK=1.0 STAT=STL*OK*(STA-STL) IF (EL.GE.RCN) GO TO 1018 IF (PR=0.LT.RCN/100.1) GO TO 1010 IF (PR.GT. RCN/100.1) STOP=STL*PRMO*(STA-STL)/(PRMO-PR) STAT = MIN1(STOP,STAT)	PLMPLT 128 PLMPLT 129 PLMPLT 130 PLMPLT 131 PLMPLT 132 PLMPLT 133 PLMPLT 134 PLMPLT 135 PLMPLT 136 PLMPLT 137 PLMPLT 138 PLMPLT 139 PLMPLT 140 PLMPLT 141 PLMPLT 142 PLMPLT 143 PLMPLT 144 PLMPLT 145
135	1010 KT=STAT/SOLK*1 KS=MIN(KS,120) KT=MIN(KT,120) MK=0 N=KT LV=LEVMO C C SET UP TO LOAD PRINT LINE	PLMPLT 146 PLMPLT 147 PLMPLT 148 PLMPLT 149 PLMPLT 150 PLMPLT 151 PLMPLT 152 PLMPLT 153 PLMPLT 154 PLMPLT 155 PLMPLT 156 PLMPLT 157 PLMPLT 158 PLMPLT 159 PLMPLT 160 PLMPLT 161 PLMPLT 162 PLMPLT 163 PLMPLT 164 PLMPLT 165 PLMPLT 166 PLMPLT 167 PLMPLT 168 PLMPLT 169 PLMPLT 170 PLMPLT 171 PLMPLT 172
140	1011 CONTINUE IF (M.GT.120) GO TO 1101 DO 1100 K=M,N SYN(K+10)=DYN(LVL) IF (LVL.GT.0) GO TO 1100 SYN(K+10)=1W* SYN(101)=1W* CONTINUE 1100 IF (M.GE.KS) GO TO 1101 SYN(11*KT)=1W M=M+2 N=N+5 LVL=LEV IF (M.LE.N) GO TO 1011 C C * REINITIALIZE K LOOP	PLMPLT 164 PLMPLT 165 PLMPLT 166 PLMPLT 167 PLMPLT 168 PLMPLT 169 PLMPLT 170 PLMPLT 171 PLMPLT 172
150	1101 STL=STA KMO=KS+1 LEVMO=LEV AMO=A PRMO=PR 1110 CONTINUE C C * CLOSE K LOOP	PLMPLT 170 PLMPLT 171 PLMPLT 172
155	OLR=FLCAT(OLR)/(LCM-1) OLT=INT(OLF) OLRT=ABS(OLR-OLT)	

	IF(OLRT.GT.0.01) GO TO 0022		
	NRAD=OLY		
175	SYN(1)=LABINRAD)		PLMPLT 173
	SYN(5)=1MP		PLMPLT 174
	SYN(6)=1MA		PLMPLT 175
	SYN(7)=1MD		PLMPLT 176
	SYN(10)=1M-		PLMPLT 177
	SYN(11)=1M-		PLMPLT 178
180	IF(INRAD.NE.1) GO TO 0020		PLMPLT 179
	SYN(11)=1M-		PLMPLT 180
	SYN(10)=1M-		PLMPLT 181
0020	IF(INRAD.NE.0) GO TO 0022		PLMPLT 182
	SYN(11)=1M-		PLMPLT 183
105	0022 IF(OLG.LE.1.01SYN(9))=1M-		PLMPLT 184
	PRINT FMP,SYN		PLMPLT 185
	1111 CONTINUE		PLMPLT 186
	C CLOSE L COOP		PLMPLT 187
	C		PLMPLT 188
190	LA=1		PLMPLT 189
	OK=2.*RON/SCLK		PLMPLT 190
	IP=1		PLMPLT 191
	IS=1		PLMPLT 192
	IO=11		PLMPLT 193
195	0202 LA=11		PLMPLT 194
	LB=11		PLMPLT 195
	0220 CONTINUE		PLMPLT 196
	IF(17.0E.129) IO=129		PLMPLT 197
	DO 0222 I=IS,IO,2		PLMPLT 198
200	LA=LAB(LA)		PLMPLT 199
	LB=LAB(LB)		PLMPLT 200
	SYN(11)=1M-		PLMPLT 201
	0222 SYN(11)=1M-		PLMPLT 202
	IF(17.0E.129) GO TO 2200		PLMPLT 203
205	GO TO (2000,2002,2020)IP		PLMPLT 204
	C		PLMPLT 205
	2000 IS=IO-1		PLMPLT 206
	IP=2		PLMPLT 207
	LB=LAB(LB-5)-5		PLMPLT 208
210	IF(137.0E.5)LB=10		PLMPLT 209
	GO TO 0220		PLMPLT 210
	C		PLMPLT 211
	2102 IS=IO+1		PLMPLT 212
	IO=12.*OK+LABN		PLMPLT 213
	IP=3		PLMPLT 214
215	GO TO 0202		PLMPLT 215
	C		PLMPLT 216
	2222 CONTINUE		PLMPLT 217
	LB=LABN		PLMPLT 218
	LA=LABN+1		PLMPLT 219
220	IF(LABN.LE.10) GO TO 2000		PLMPLT 220
	LB=L-3-10		PLMPLT 221
	LA=1		PLMPLT 222
	2022 IF(13.17.10) GO TO 2000		PLMPLT 223
	LA=LA+1		PLMPLT 224
225	LB=L-3-10		PLMPLT 225
	GO TO 2022		PLMPLT 226
	C		PLMPLT 227
	2200 PRINT FMP,SYN		PLMPLT 228
			PLMPLT 229

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	OVERLAY(RMP,5,1)		
	PROGRAM FILTER		
	COMMON/FILTER/FILTER,9(FILTER300)		
	COMMON/COMMON/NT,NA,NT,NU(300),NU(300),NU(300),NU(300)		
	COMMON/COMMON/NT,NA,NT,NU(300),NU(300),NU(300),NU(300)		
	DIMENSION F(5,100),F(5,100)		
	DIMENSION F(5,100),F(5,100)		
	REAL N(100)		
	DATA F(1,1)=1.751/3*0.005		
10	*0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20,0.21,0.22,0.23,0.24,0.25,0.26,0.27,0.28,0.29,0.30,0.31,0.32,0.33,0.34,0.35,0.36,0.37,0.38,0.39,0.40,0.41,0.42,0.43,0.44,0.45,0.46,0.47,0.48,0.49,0.50,0.51,0.52,0.53,0.54,0.55,0.56,0.57,0.58,0.59,0.60,0.61,0.62,0.63,0.64,0.65,0.66,0.67,0.68,0.69,0.70,0.71,0.72,0.73,0.74,0.75,0.76,0.77,0.78,0.79,0.80,0.81,0.82,0.83,0.84,0.85,0.86,0.87,0.88,0.89,0.90,0.91,0.92,0.93,0.94,0.95,0.96,0.97,0.98,0.99,1.00	FILTER	2
		FILTER	3
		FILTER	4
		FILTER	5
		FILTER	6
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		FILTER	57
		FILTER	58

60	C	INCREMENTS BASED ON MAXIMUM RESOLUTION OF DATA INCLUDED IN	59	FILTER
	C	THE UNIVERSITY OF MICHIGAN PLUMES PROGRAM	60	FILTER
	C		61	FILTER
		I=1	62	FILTER
		ON=25	63	FILTER
		IF(XUC.LT.2000.) GO TO 602	64	FILTER
65		IF(XUC.GT.2400.) AND XUC.LT.3000.) GO TO 602	65	FILTER
		IF(XUC.GT.3770.) GO TO 602	66	FILTER
		ON=13	67	FILTER
		NUO=INT(12.*WBEG/ON)+1	68	FILTER
682		XUC=FLOAT(NUO)*ON/2	69	FILTER
			70	FILTER
70	C	ONU(1)=XUC-WBEG*ON/2	71	FILTER
	C	NU(1)=XUC	72	FILTER
	C	NU(1)=XUC	73	FILTER
	C	NU(1)=XUC	74	FILTER
	C	DO THE SAME FOR ALL NU AND ONU CARDS IF MULTIPLE WAVELENGTHS TO	75	FILTER
75	C	BE UTILIZED	76	FILTER
	C		77	FILTER
		ONU(1)=XUC-WBEG*ON/2	78	FILTER
		NU(1)=XUC	79	FILTER
		ON=ON	80	FILTER
80		GO TO 41	81	FILTER
		I=I+1	82	FILTER
	58	ONU(1)=ON	83	FILTER
		NU(1)=XUC	84	FILTER
	41	XUC=XUC+ON/2	85	FILTER
		ON=25	86	FILTER
85		IF(XUC.LT.2000.) GO TO 601	87	FILTER
		IF(XUC.GT.2400.) AND XUC.LT.3000.) GO TO 601	88	FILTER
		IF(XUC.GT.3770.) GO TO 601	89	FILTER
		ON=13	90	FILTER
90	601	XUC=XUC+ON/2	91	FILTER
		ON=ON	92	FILTER
		IF(XUC.LT.WEND) GO TO 40	93	FILTER
		MFREQ=I	94	FILTER
		ONU(1)=WEND-NU(1)-0.5*ONU(1)-1	95	FILTER
95		GO TO 58	96	FILTER
	C		97	FILTER
	C	INCREMENTS AND FREQUENCY CENTERS BASED ON NUINC (DEFAULT=50CM-1)	98	FILTER
	C		99	FILTER
	52	MFREQ=INT((WEND-WBEG)/NUINC)+1	100	FILTER
100		XUC=XUC+NUINC/2	101	FILTER
		DO 43 I=1,MFREQ	102	FILTER
		NU(1)=XUC	103	FILTER
		ONU(1)=NUINC	104	FILTER
105	43	XUC=XUC+NUINC	105	FILTER
	44	ONU(MFREQ)=WEND-NU(MFREQ)+NUINC/2	106	FILTER
	50	CONTINUE	107	FILTER
		NUFRST=1	108	FILTER
	C	GO TO (11,12,13,14,15) IFILTER	109	FILTER
110	11	BAND ONE	110	FILTER
		INDEX=3	111	FILTER
		GO TO 15	112	FILTER
	C	BAND TWO	113	FILTER
12		INDEX=37	114	FILTER
		GO TO 16	115	FILTER

115	C	BAND THREE	FILTER	116
	13	INDEX=10	FILTER	117
		GO TO 16	FILTER	118
	C	BAND FOUR	FILTER	119
	16	INDEX=16	FILTER	121
120		GO TO 16	FILTER	121
	C	BAND FIVE	FILTER	122
	15	INDEX=12	FILTER	123
	16	DO 17 11=1,NFREQ	FILTER	124
		FCMK=10000,/MU(11)	FILTER	125
		IK=INT((FCMK-AM(11))/0.05+1.01) + INDEX	FILTER	126
125		AL=31*ARTE(1,02)*FLOAT(IK(11))	FILTER	127
		FRAC=(FCMK-AL)/0.35	FILTER	128
	17	AFILTER(11)=FIFILTER,IK(1)+FRAC*(FIFILTER,IK(1)-FIFILTER,IK(1))	FILTER	129
		END	FILTER	130

Line	Code	Statement	Label
5	01	OVERLAY=RP-11.00	
6	02	PROGRAM REMAIN	
7	03	COMMON /MPACK/ INT(100),MTRV(100),INTS	
8	04	COMMON /CPROG/ CAP	
9	05	COMMON /CONFLW/ NMVCE,MV(2,20),REM(2,1),MPL(2,20),PL(2,1),MPL	
10	06	MPL(2,1),MPL(2,20)	
11	07	COMMON /NODEN/ NODEN(1,2,20), S(2,20)	
12	08	COMMON /OPCR/ TS(2),UAT(2),L(2,2),M(2,2),PTSC(2),TSC(2),RSC(2)	
13	09	M(2,2),M(2,2),M(2,2),M(2,2),M(2,2),M(2,2),M(2,2),M(2,2)	
14	10	COMMON /SMIF/ SMIF(1,4),IN,PAROVE,MUMOVE,KOOLSE	
15	11	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
16	12	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
17	13	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
18	14	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
19	15	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
20	16	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
21	17	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
22	18	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
23	19	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
24	20	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
25	21	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
26	22	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
27	23	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
28	24	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
29	25	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
30	26	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
31	27	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
32	28	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
33	29	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
34	30	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
35	31	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
36	32	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
37	33	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
38	34	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
39	35	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
40	36	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
41	37	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
42	38	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
43	39	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
44	40	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
45	41	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
46	42	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
47	43	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
48	44	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
49	45	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
50	46	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
51	47	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
52	48	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
53	49	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
54	50	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
55	51	DEFINITION V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
56	52	V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1),V(1,1)	
57	53	DEFINITION V(1,1),V(1,1),V(1,1),V	

	IA8C(1)=0		59	RIMAINS
	IA8C(2)=0		60	RIMAINS
68	DO 15 J=1,NM		61	RIMAINS
	READ(5,5) TSYNEM(J),K(J),KX(J),XI(J),XF(J)		62	RIMAINS
	IF(KX(J).EQ.0) GO TO 937		63	RIMAINS
	READ(5,4) A2(1,2)		64	RIMAINS
65	READ(5,1) NM(1,1)		65	RIMAINS
	NU=NM(J)		66	RIMAINS
	READ(5,6,7) INODEN2(J),K(K(J),KX2(J),I=1,MU)		67	RIMAINS
	FORAT(28,212,6X,F10,5)		68	RIMAINS
	DO 41 I=1,2		69	RIMAINS
70	READ(5,6,6) JSURF(J,II),KALJ,III,IMEVA(J,III),MIALJ,III		70	RIMAINS
	DO 41 I=1,1,NM		71	RIMAINS
	IF(JSURF(J,II).EQ. KSURF(III)) GO TO 45		72	RIMAINS
	CONTINUE		73	RIMAINS
41	IF(KCOL(III).GT.0) GO TO 42		74	RIMAINS
45	GO TO 40		75	RIMAINS
75	DO 531 I=1,2		76	RIMAINS
	IF(IA8C(IIA).EQ. JSURF(J,II)) GO TO 40		77	RIMAINS
	CONTINUE		78	RIMAINS
531	IM=IM+1		79	RIMAINS
981	IA8C(II)= JSURF(J,II)		80	RIMAINS
88	READ(5,4) TTSC(IM),RSC(IM),GAMASC(IM),CPSC(IM),MSET(IM),TS(IM),		81	RIMAINS
	YJA(IM)		82	RIMAINS
	IF(MSET(IM).NE.0) GO TO 3000		83	RIMAINS
	READ(5,4) PISOT(IM),K12(IM),M12(IM)		84	RIMAINS
3000	IF(KCOL(III).-2) 932,903,904		85	RIMAINS
902	READ(5,4) K23(IM),N23(IM),FORST(IM)		86	RIMAINS
65	READ(5,1) MA(IM)		87	RIMAINS
	MA=MA(IM)		88	RIMAINS
	READ(5,6,5) (LX(IM),JA),JA=1,MAA)		89	RIMAINS
98	MA=MAA		90	RIMAINS
	READ(5,4)(XN(IM),JA),YN(IM),JA),JA=1,MAA)		91	RIMAINS
	GO TO 40		92	RIMAINS
983	READ(5,1) NM(IM),MA(IM)		93	RIMAINS
	MA=MA(IM)		94	RIMAINS
	READ(5,6,6)(NOEN(IM),JA),JA=1,MAA)		95	RIMAINS
95	READ(5,6,5)(LX(IM),JA),JA=1,MAA)		96	RIMAINS
	NUM1=NUM1+1		97	RIMAINS
	READ(5,4)(S(IM),JA),JA=1,NUM1)		98	RIMAINS
	NUM1=NUM1+1		99	RIMAINS
	READ(5,4)(XN(IM),JA),YN(IM),JA),JA=1,NUM1)		100	RIMAINS
100	READ(5,4) COX(IM)		101	RIMAINS
	GO TO 40		102	RIMAINS
	READ(5,1) NM(IM),MA(IM),MA(IM)		103	RIMAINS
986	JA=NM(IM)+1		104	RIMAINS
	READ(5,94)(XN(IM),I),YN(IM),I),S(IM),I),K5(IM),I),I=1,JA)		105	RIMAINS
105	FORAT(15,10,5)		106	RIMAINS
	JB=MA(IM)		107	RIMAINS
	READ(5,6,5) INODEN(IM),I=1,JB)		108	RIMAINS
	READ(5,6,6)(LX(IM),I),I=1,JB)		109	RIMAINS
	IF(KX .LC. 1) GO TO 40		110	RIMAINS
110	KMX=1		111	RIMAINS
	READ(5,1) ANI		112	RIMAINS
	READ(5,93) (113	RIMAINS
	READ(5,4) I MYT,AR,SVHX,MD		114	RIMAINS
99	FORAT(15,10,5)		115	RIMAINS

115	40	CONTINUE	RIMAIN3	116
	18	CONTINUE	RIMAIN3	117
		NNAT=3	RIMAIN3	118
		DO 11 I=1,NM	RIMAIN3	119
	11	NNAT=NNAT+NNAT(I)	RIMAIN3	120
120		READ(5,1) ICS	RIMAIN3	121
	502	IF(IICS) 501,501,502	RIMAIN3	122
	503	READ(5,500) (ICSORF(IJJA),JJA=1,ICS)	RIMAIN3	123
	501	FOR-MAT(24,S12)	RIMAIN3	124
		READ(5,4) PTP,TP,RP,GAMMAP,MP	RIMAIN3	125
		READ(5,4) PIS,TIS,RS,GAMMAS,MS	RIMAIN3	126
125		READ(5,1) PAM3	RIMAIN3	127
		FOR-MAT(8,F12.5)	RIMAIN3	128
		DO 700 I=1,NMN	RIMAIN3	129
		MSAT=2.0	RIMAIN3	130
		AT=0.0	RIMAIN3	131
		FPAT=0.0	RIMAIN3	132
130		FFP=1.1	RIMAIN3	133
		CALL STORE(GCAT,AT,1.0)	RIMAIN3	134
		CALL STORE(FPAT,FFI,1.0)	RIMAIN3	135
135	701	CONTINUE	RIMAIN3	136
		IM=0	RIMAIN3	137
	001	DO 500 JUU=1,ICS	RIMAIN3	138
		NH(JUU)=0	RIMAIN3	139
		LLI=3	RIMAIN3	140
140		READ(5,6C6) (NODEM(I),NODEF(I),I=1,MTOT)	RIMAIN3	141
		DO 15 I=1,NM	RIMAIN3	142
		READ(5,1) IA	RIMAIN3	143
		IF(IA) 17,17,16	RIMAIN3	144
	15	READ(5,7) (V(I),AREAM(I),J=1,IA)	RIMAIN3	145
	17	FOR-MAT(6F10.2)	RIMAIN3	146
		CALL ACPLV(X1,V1,X2,V2),F=NOPI,ISURF,JSURF,XU1,VU1,XU2,VU2,M1	RIMAIN3	147
		IN2=XK(I1)	RIMAIN3	148
		CALL AXAPFA(X1(I1),Y(I1),XA,AREAM,IA,N1,N2,X1,VU1,XU2,VU2)	RIMAIN3	149
		IF(K(I1-1) 20,21,22	RIMAIN3	150
150	20	PIP1=PI5	RIMAIN3	151
		TP1=TP5	RIMAIN3	152
		GAMM2=GAMMAS	RIMAIN3	153
		RP1=RS	RIMAIN3	154
		MS1=MS/2.	RIMAIN3	155
155		NP1=MS1	RIMAIN3	156
		CALL COFLW(PIP1,PT5,TP1,TIS,GAMM2,GAMMAS,RP1,RS,NP1,MS1,PAMB,	RIMAIN3	157
		1A(ICT(I),K(I1))	RIMAIN3	158
		GO TO 23	RIMAIN3	159
160	21	PT51=PTP	RIMAIN3	160
		TIS1=TP	RIMAIN3	161
		GAMM1=GAMMAP	RIMAIN3	162
		RS1=RP	RIMAIN3	163
		NP1=NP/2.	RIMAIN3	164
		MS1=AP1	RIMAIN3	165
165		CALL CO -X(PTP,PT51,TP,TIS1,GAMM1,GAMMAS,RP,RS,NP1,MS1,PAMB,	RIMAIN3	166
		1A(ICT(I),K(I1))	RIMAIN3	167
		GO TO 23	RIMAIN3	168
170	22	CALL COFLW(PTP,PT5,TIS1,GAMM1,GAMMAS,RP,RS,NP1,PAMB,	RIMAIN3	169
		1A(ICT(I),K(I1))	RIMAIN3	170
	23	DO 25 J=1,IL	RIMAIN3	171
		CALL FENOTL(TPR(J),PMB)	RIMAIN3	172

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[illegible]

[illegible]

287	IFINODE1(I9) .EQ. NODEM(I8)) GO TO 952	REMAINS	287
288	CONTINUE	REMAINS	288
289	WRITE(6,1081) NODE1(I9)	REMAINS	289
290	FORMAT(9,9999) CHECK INPUT FOR NODE-I4)	REMAINS	290
291	IS=NIOT1	REMAINS	291
292	952 IM=INT5+1	REMAINS	292
293	INT5=INT5+1	REMAINS	293
294	INT5=INT5+1	REMAINS	294
295	INT5=INT5+1	REMAINS	295
296	CONTINUE	REMAINS	296
297	DO 750 KUU=1,NNM	REMAINS	297
298	IF(KSURF(I,II) .EQ. KSURF(KUU)) GO TO 751	REMAINS	298
299	CONTINUE	REMAINS	299
300	GO TO 30	REMAINS	300
301	IF(COOL(KUU) .GT. 0) GO TO 752	REMAINS	301
302	GO TO 30	REMAINS	302
303	DO 753 JUU=1,ICS	REMAINS	303
304	IF(KSURF(KUU) .EQ. ICSURF(JUU)) GO TO 755	REMAINS	304
305	CONTINUE	REMAINS	305
306	IM=IM+1	REMAINS	306
307	INDIC(IM)=KSURF(KUU)	REMAINS	307
308	DO 756 IWM=1,L	REMAINS	308
309	XX(IIM,IWM)=XL(IWM)	REMAINS	309
310	XXP(IIM,IWM)=PT(IWM)	REMAINS	310
311	XX(IIM,IWM)=TPT(IWM)	REMAINS	311
312	XXV(IIM,IWM)=VPT(IWM)	REMAINS	312
313	XXH(IIM,IWM)=HT1(IWM)	REMAINS	313
314	XXDEN(IM,IWM)=DENPT(IWM)	REMAINS	314
315	IND(IIM)=L	REMAINS	315
316	GO TO 30	REMAINS	316
317	IF(NOD(JUU) .GT. 0) GO TO 818	REMAINS	317
318	IM=IM+1	REMAINS	318
319	INDIC(IM)=KSURF(KUU)	REMAINS	319
320	DO 758 IWM=1,L	REMAINS	320
321	XX(IIM,IWM)=XL(IWM)	REMAINS	321
322	XXP(IIM,IWM)=PT(IWM)	REMAINS	322
323	XX(IIM,IWM)=TPT(IWM)	REMAINS	323
324	XXV(IIM,IWM)=VPT(IWM)	REMAINS	324
325	XXH(IIM,IWM)=HT1(IWM)	REMAINS	325
326	XXDEN(IM,IWM)=DENPT(IWM)	REMAINS	326
327	IND(IIM)=L	REMAINS	327
328	NOD(JUU)=L-1	REMAINS	328
329	GO TO 30	REMAINS	329
330	DO 820 IM=1,2	REMAINS	330
331	IF(KSURF(KUU) .EQ. INDIC(IM)) GO TO 821	REMAINS	331
332	CONTINUE	REMAINS	332
333	IO=NOD(JUU)+1	REMAINS	333
334	IO=1	REMAINS	334
335	LJ=L-IO-1	REMAINS	335
336	DO 830 IWM=IO,LJ	REMAINS	336
337	XX(IIM,IWM)=XL(IOI)	REMAINS	337
338	XXP(IIM,IWM)=PT(IOI)	REMAINS	338
339	XX(IIM,IWM)=TPT(IOI)	REMAINS	339
340	XXV(IIM,IWM)=VPT(IOI)	REMAINS	340
341	XXH(IIM,IWM)=HT1(IOI)	REMAINS	341
342	XXDEN(IM,IWM)=DENPT(IOI)	REMAINS	342
343	IOI=IOI+1	REMAINS	343
344	IND(IIM)=LJ	REMAINS	344

400	GO TO 2810	RIMAINS 401
	1817 CALL OVERLAY(NHXHP,9,2,5NRECALL)	RIMAINS 402
	0813 CALL FILMOL	RIMAINS 403
	GO TO 2019	RIMAINS 404
402	1314 CALL OVERLAY(NHXHP,9,3,5NRECALL)	RIMAINS 405
	0814 CALL COMFLM	RIMAINS 406
	2818 KOOLY=KOOLY+KOOL(ITAB)	RIMAINS 407
	1910 CONTINUE	RIMAINS 408
	1899 CONTINUE	RIMAINS 409
410	SWPRTNTO .EQ. 0) GO TO 18880	RIMAINS 410
	CALL OVERLAY(NHXHP,9,6)	RIMAINS 411
	CALL CALEDG	RIMAINS 412
	18889 CONTINUE	RIMAINS 413
	END	RIMAINS 414

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	SUBROUTINE AVERIA,TM,EX,NODE,M,IX,PRINTS)		
	DIMENSION A(1),TM(1),LY(1),NODE(2,10)	2	2
	COMMON/CC/ NODEN(10),MT(10),LUU,KODLT	3	3
	INTEGER PRINTS	4	4
5	K=1	5	5
	K=1	6	6
	DO 110 I=1,M	7	7
	K=LY(I)+K	8	8
	AT=3.0	9	9
10	TAOX=D.0	10	10
	DO 51 J=K,K	11	11
	TAOX=TAOX+(A(I,J)*TM(I,J))	12	12
	AT=AT+TAOX	13	13
	CONTINUE	14	14
15	MT=TAOX/AT	15	15
	K=K+1	16	16
	IF (PRINTS .GT. 8) WRITE(6,101) NODE(I,M),MT	17	17
	LU=LUU(I)	18	18
20	NODEN+(LUU)=NODE(I,M,IT	19	19
	MT*(LUU)=MT*450.0	20	20
	FORCAT(I,13),34MAVERAGE WALL TEMPERATURE FOR NODE ,I2.4H IS ,F7.2,	21	21
	15H DEG. R.)	22	22
	CONTINUE	23	23
	RETURN	24	24
25	END	25	25

	SUBROUTINE FLOWND(PTEZ,PS3A,XX,L,KOOL)	
	DIMENSION PS3A(3),XX(1)	2 FLOWND
	K=0	3 FLOWND
	KK=0	4 FLOWND
5	M=1	5 FLOWND
	IF(KOOL.EQ.5) M=2	6 FLOWND
	GO 2,1=M,L	7 FLOWND
	IF(PTEZ-PS3A(1)) 3,3,4	8 FLOWND
	IF(K) 2,2,5	9 FLOWND
10	IF(K) 6,6,7	10 FLOWND
	XLOC1=XX(1)	11 FLOWND
	IF(1-L) 8,8,9	12 FLOWND
	K=1	13 FLOWND
	GO 10 2	14 FLOWND
15	IF(1-L) 2,9,9	15 FLOWND
	XLOC2=XX(1)	16 FLOWND
	IF(K) 2,2,20,21	17 FLOWND
	WRITE(6,1)	18 FLOWND
20	IF(KOOL.GT.1) GO 10 25	19 FLOWND
	WRITE(6,2) XLOC1,XLOC2	20 FLOWND
	FORMAT(5X,20HFROM AXIAL LOCATION ,F5.1,40H THRU END OF COOLING SUR	21 FLOWND
	FACE LOCATED AT ,F5.1,1H,,//)	22 FLOWND
	GO 10 2	23 FLOWND
25	WRITE(6,23) XLOC1,XLOC2	24 FLOWND
	FORMAT(6X,21HFROM SLOT LOCATED AT ,F5.1,35H THRU LAST COOLING SLOT	25 FLOWND
	LOCATED AT ,F5.1,1H,,//)	26 FLOWND
	GO 10 2	27 FLOWND
	XLOC2=XX(1)	28 FLOWND
	IF(K) 11,11,12	29 FLOWND
31	WRITE(6,11)	30 FLOWND
	KK=1	31 FLOWND
	IF(KOOL.GT.1) GO 10 15	32 FLOWND
	WRITE(6,15) XLOC1,XLOC2	33 FLOWND
	GO 10 16	34 FLOWND
35	WRITE(6,17) XLOC1,XLOC2	35 FLOWND
	K=2	36 FLOWND
	FORMAT(5X,21HFROM SLOT LOCATED AT ,F5.1,40H TO (BUT NOT INCLUDING)	37 FLOWND
	SLOT LOCATED AT ,F5.1,1H,,//)	38 FLOWND
	CONTINUE	39 FLOWND
40	FORMAT(//,21X,30HPROGRAM PREDICTS REVERSE COOLANT FLOW,,/28X,2	40 FLOWND
	18HPROGRAM UTILIZES ZERO FLOW,,//)	41 FLOWND
	FORMAT(15X,28HFROM AXIAL LOCATION ,F5.1,19H TO AXIAL LOCATION ,F5.	42 FLOWND
	11,1H,,//)	43 FLOWND
	RETURN	44 FLOWND
45	END	45 FLOWND
		46 FLOWND


```

FUNCTION STRATE(X1,X2,Y1,Y2,M)
  STRATE=((Y2-Y1)/(X2-X1))*(X-X1))+Y1
RETURN
END

```

```

  STRATE 2
  STRATE 3
  STRATE 4
  STRATE 5

```

[illegible]

60	VSS(I)=VS TPP(I)=TP IF(8TAL) LE. 0.) GO TO 1000 IF(F-STOP) 1000, 340, 340 1000 IF(KX) 998, 998, 1001 998 IF(8TAL) LE. 0.1) I=I-1 GO TO 999	COFLOW	59
65	1001 IF(8TAL) -0.1) 1003, 1003, 1002 1003 CALL TABLE(8TA, AA, 0.0, AAA, OUM, I) J=I-1	COFLOW	60
70	1012 CALL TABLE(PP, AA, PAMB, AAA, OUM, I) J=I 1010 CF2=AAA/AACT DO 1017 I=1, J 1017 AA(I)=AA(I)/CF2 I=J PPN=SQRT(AA/13.1415927*CF2)*REF**2) PTE=RPN*1.1 RPN=SQRT(AP/13.1415927*CF2)*RPN**2) P8=P/14.7 RETURN END	COFLOW	61
75		COFLOW	62
80		COFLOW	63
		COFLOW	64
		COFLOW	65
		COFLOW	66
		COFLOW	67
		COFLOW	68
		COFLOW	69
		COFLOW	70
		COFLOW	71
		COFLOW	72
		COFLOW	73
		COFLOW	74
		COFLOW	75
		COFLOW	76
		COFLOW	77
		COFLOW	78
		COFLOW	79
		COFLOW	80
		COFLOW	81

	SUBROUTINE STORE(FP,FF,I,M)		STORE1	2
	DIMENSION FPI(5),FFI(5)		STORE1	3
	IFEN .GT. 0) GO TO 50		STORE1	4
5	FPI(I)=FP		STORE1	5
	FFI(I)=FF		STORE1	6
	GO TO 100		STORE1	7
58	FP=FFI(I)		STORE1	8
	FF=FFI(I)		STORE1	9
100	RETURN		STORE1	10
10	END		STORE1	11

A-124

SUBROUTINE STORE(HGAT,AT,I,N)

DIMENSION HG(5),A(5)

IF(N.GT.0) GO TO 50

A(I)=AT

HG(I)=HGAT

GO TO 100

HGAT=HG(I)

AT=A(I)

RETURN

END

STORE 2

STORE 3

STORE 4

STORE 5

STORE 6

STORE 7

STORE 8

STORE 9

STORE 10

STORE 11

		SUBROUTINE AAREAT(XI,XF,XA,AREAM,IA,KK,KKK,XU1,YU1,XU2,YU2)	
		DIMENSION XA(1),AREAM(1),XU1(1),YU1(1),XU2(1),YU2(1)	AXAREA 2
		COMMON XL(100),ACROSS(100)	AXAREA 3
5		1YLI 80,YL2 90,PI(150),AA(150),XMH1(150),XMH2(150),TRS(150),	AXAREA 4
		2DENP(150),VPP(150),TRP(150),DENST(150),VSS(150),PT(100),	AXAREA 5
		3XVSTL 60,1STL 60,DENST(00),VSTL 60,XVPTL 60,1STPT(60),	AXAREA 6
		4DENP(100),VPT(100)	AXAREA 7
		COMMON L,LL	AXAREA 8
		KCH=IXF-XI	AXAREA 9
10		KCH=K	AXAREA 10
		IF(XCH1.EQ. KCH) GO TO 50	AXAREA 11
		K=K+2	AXAREA 12
15	53	GO TO 51	AXAREA 13
	51	K=K+1	AXAREA 14
		L=3	AXAREA 15
		YL(1)=YL	AXAREA 16
		DO 22 I=1,K	AXAREA 17
		DO 3 J=1,KK	AXAREA 18
20		IF(XL(I).EQ.XU1(J)) GO TO 9	AXAREA 19
		IF(XL(I).GT.XU1(J)) GO TO 10	AXAREA 20
		YL(I)=STRATE(XU1(J)-1,XU1(J),YU1(J)-1,YU1(J),XL(I))	AXAREA 21
		GO TO 11	AXAREA 22
	9	YL(I)=YU1(J)	AXAREA 23
25		GO TO 11	AXAREA 24
	10	CONTINUE	AXAREA 25
	11	DO 23 J=1,KKK	AXAREA 26
		IF(XL(I).EQ.XU2(J)) GO TO 19	AXAREA 27
		IF(XL(I).GT.XU2(J)) GO TO 20	AXAREA 28
30		YL2(J)=STRATE(XU2(J)-1,XU2(J),YU2(J)-1,YU2(J),XL(I))	AXAREA 29
		GO TO 21	AXAREA 30
	19	YL2(J)=YU2(J)	AXAREA 31
		GO TO 21	AXAREA 32
	20	CONTINUE	AXAREA 33
35	21	L=L+1	AXAREA 34
		ACROSS=3.14159*(A05(YL(I)+YL(I))-YL2(J)+YL2(J))	AXAREA 35
		IF(IA.EQ. 0) GO TO 15	AXAREA 36
		IF(XL(I)-YA(I)) 15,16,16	AXAREA 37
		IF(XL(I)-XA(I)) 17,17,15	AXAREA 38
40	15	AMINUS=0.0	AXAREA 39
		GO TO 16	AXAREA 40
	17	CALL TABL(ETA,AREA4,XL(I),AMINUS,DUM,IA)	AXAREA 41
	18	ACROSS(I)=ACROSS-AMINUS	AXAREA 42
		IF(IA1.GE.K) GO TO 23	AXAREA 43
45		XL(I+1)=XL(I)+1.0	AXAREA 44
		GO TO 22	AXAREA 45
	23	XL(K)=XF	AXAREA 46
	22	CONTINUE	AXAREA 47
		RETURN	AXAREA 48
50		END	AXAREA 49
			AXAREA 50
			AXAREA 51

	SUBROUTINE CPAGNA (MO, TIO, CP, GM)		
	REAL MO		CPAGNA 2
	DIMENSION TT(16), CPT(16), GMT(16)		CPAGNA 3
	DATA TT/100., 250., 500., 600., 700., 800., 900., 1000., 1150., 1300., 1500., 1800., 2000.,		CPAGNA 4
5	1, 2500., 3500., 4500., 4520., /		CPAGNA 5
	DATA CPT/1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, /		CPAGNA 6
	DATA GMT/1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, /		CPAGNA 7
	DATA GMT/1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, /		CPAGNA 8
10	15, 1, 12, 3, 1, 315, 1, 305, 1, 295, 1, 285, 1, 275, 1, 265, 1, 255, 1, 245, 1, 235, 1, 225, 1, 215, 1, 205, 1, 195, 1, 185, 1, 175, 1, 165, 1, 155, 1, 145, 1, 135, 1, 125, 1, 115, 1, 105, 1, 95, 1, 85, 1, 75, 1, 65, 1, 55, 1, 45, 1, 35, 1, 25, 1, 15, 1, 5, 1, /		CPAGNA 9
	NCP=16		CPAGNA 10
	GM=1, 4		CPAGNA 11
	SM=10, 0, 0, 0		CPAGNA 12
	DO 5 I=1, NCP		CPAGNA 13
15	GM=GM		CPAGNA 14
	GM=GM-1, 0, 1, 2, /		CPAGNA 15
	TO=TIO/11, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, /		CPAGNA 16
	CALL TABLELFTI, GM, TO, GM, DUM, NCP		CPAGNA 17
	IF (ABS(IG-C-GM)/GM) > .001, 5, 9, 5		CPAGNA 18
20	5 CONTINUE		CPAGNA 19
6	CALL TABLELFTI, CPT, TIO, CP, DUM, NCP		CPAGNA 20
	RETURN		CPAGNA 21
	END		CPAGNA 22
			CPAGNA 23

SUBROUTINE PRNOTL (I,PR)

IF (I-900.) 1,1,2

1 PR=.76-.0001*I

GO TO 3

2 IF (I-1400.) 4,4,5

4 PR=.705-.0001*I

GO TO 3

5 PR=.65

3 CONTINUE

RETURN

END

PRNOTL 2
PRNOTL 3
PRNOTL 4
PRNOTL 5
PRNOTL 6
PRNOTL 7
PRNOTL 8
PRNOTL 9
PRNOTL 10
PRNOTL 11
PRNOTL 12

	OVERLAYINRHP,11,11	TRANCL	2
	PROGRAM TRANCL	TRANCL	3
	COMMON /CDPCG/ CPG	TRANCL	4
	COMMON /SMIT/ IS,UA,K12,K13,P11,T11,DUM1,K23,N23,NSET,CPC,DUM2	TRANCL	5
5	DUM3,P05,M1,M,DUM4,K00L	TRANCL	6
	* DIMENSION A(96),TM(63),LX(181),	TRANCL	7
	MZ(MD),KX(61),XX(180),PSI(180),TANOA(180),TISE(180),	TRANCL	8
	3 XMT(3),XMTF(3),XP(3)	TRANCL	9
10	COMMON/CC/ NODEM(110),MT(110),LUU,KOOLY	TRANCL	10
	COMMON /LINKS/ HOT(100), NM2,201, YMT2,201, NODE(2,20), IM, IABC	TRANCL	11
	COMMON X1(11840),PSI(500),TAKOT(1100),RHOT(1100),VGT(1100)	TRANCL	12
	COMMON /PRINT/ PRINT1, PRINT2, PRINT3, PRINT4, PRINT5,	TRANCL	13
	PRINT6, PRINT7, PRINT8, PRINT9, PRINT0	TRANCL	14
15	* INTEGER PRINT1,PRINT2,PRINT3,PRINT4,PRINT5,PRINT6,PRINT7,PRINT8	TRANCL	15
	1,PRINT9,PRINT0	TRANCL	16
	REAL K12,K23 *M2,N23	TRANCL	17
	IJK=1	TRANCL	18
	LEV	TRANCL	19
20	J=1	TRANCL	20
	JU=J	TRANCL	21
	XX11=XX(1M,1)	TRANCL	22
	DO 400 I=1,M	TRANCL	23
	XL=SQRT(((XN(1M,I)-XN(1M,I+1))*XN(1M,I)-XN(1M,I+1)))+(YN(1M,I)-	TRANCL	24
25	YN(1M,I+1))*Y(1M,I)-YN(1M,I+1))	TRANCL	25
	LX(I)=XL	TRANCL	26
	L=L+LX(I)	TRANCL	27
	LL=LX(I)	TRANCL	28
	COST=(XN(1M,I+1)-XN(1M,I))/XL	TRANCL	29
30	Z=(Y(1M,I+1)-Y(1M,I))/(XN(1M,I+1)-XN(1M,I))	TRANCL	30
36	DX=X/LLX(I)	TRANCL	31
	M=1	TRANCL	32
	DO 401 K=1,LL	TRANCL	33
	J=J+1	TRANCL	34
35	XX(J)=XN(1M,I)+(M*DX+COSTM)	TRANCL	35
	M=M+1	TRANCL	36
	CONTINUE	TRANCL	37
	DO 402 K=1,LL	TRANCL	38
	JJ=JJ+1	TRANCL	39
40	YY=Z*(X(JJ)-XN(1M,I))+Y(1M,I)	TRANCL	40
	YYV=Z*(X(JJ+1)-XN(1M,I))+Y(1M,I)	TRANCL	41
	A(JJ)=3.14159*DX*(YY+YYV)	TRANCL	42
	XX(JJ)=(YX(JJ)+XX(JJ+1))/2.	TRANCL	43
	CONTINUE	TRANCL	44
482	CONTINUE	TRANCL	45
488	CONTINUE	TRANCL	46
45	PSI=0.0	TRANCL	47
	DO 12 J=1,L	TRANCL	48
	CALL TABLE(X1,PSGT,XXX(J),PSI(J),DUM,M)	TRANCL	49
	CALL TABLE(X1,IANO1,XXX(J),TANOA(J),DUM,M)	TRANCL	50
50	PSI=PSI+PSI(J)	TRANCL	51
	TISE(J)=(TANOA(J)+T11)/2.	TRANCL	52
54	CONTINUE	TRANCL	53
	AL=L	TRANCL	54
	PSIAT=PSI/AL	TRANCL	55
55	PT2E=PI-(C.25*(PI-PSIAT))	TRANCL	56
	SMALL=10000.0	TRANCL	57
	DO 70 I=1,L	TRANCL	58
	SMALL=AMIN1(SMALL,PSI(I))	TRANCL	59

A-130

115	206	CALL PSOLNINT,INT,XP,MT,DUW,3)	116
		MEM	TRANCL 117
		PTZ=PT1-(1K12/SIGM12)*(M*N12))	TRANCL 118
		LL=1	TRANCL 119
		GO TO 13	TRANCL 120
120	22	DO 10 J=1,L	TRANCL 121
		CALL TABLE(XTI,HGT,XX(XJ),HGO,DUW,M1)	TRANCL 122
		CALL TABLE(XTI,RMOT,XX(XJ),RMC,DUW,M1)	TRANCL 123
		CALL TABLE(XTI,VGT,XX(XJ),VG,DUW,M1)	TRANCL 124
		STO=HGO/(RMO*VG*CPC*3600.)	TRANCL 125
125		IFM(XJ) 173,170,171	TRANCL 126
	171	INTJ=IACDARIJ	TRANCL 127
		GO TO 10	TRANCL 128
	171	F=(M2(J)/(4J)*POR5)/(RMO*VG)	TRANCL 129
		Z=F/SIO	TRANCL 130
130		F=S3*(1.5*Z)*(0.5*Z2+1.)-8.5*Z2	TRANCL 131
		ETRA=(F*HGO*AI(J))/(W7(J)*CPC*144.*3600.)	TRANCL 132
		INTJ=((1.15*144*AI(J))+(12E7/ETRA*1.))	TRANCL 133
	30	CONTINUE	TRANCL 134
		IFELL=1.24,25	TRANCL 135
135	24	LL=1	TRANCL 136
		DO 35 J=1,L	TRANCL 137
		TYPE(J)=(INTJ)+TYPE(J)/2.	TRANCL 138
	35	CONTINUE	TRANCL 139
		W=1	TRANCL 140
		K=1	TRANCL 141
		LL=0	TRANCL 142
		KK=0	TRANCL 143
		IFWSET=.01,13,13,451	TRANCL 144
	25	IFPRINT5,GT,3) WRITE(6,160) MT	TRANCL 145
	70	FORMAT1M1,/,23X,21HTRANSPIRATION COOLING,/,27X,12HSURFACE NO.,*12	TRANCL 146
		1,/,)	TRANCL 147
		CALL 'CPRIA,TM,IN,NOCE,M,IN,PRINT5)	TRANCL 148
		IFPRINT5,GT,3) WRITE(6,160) MT	TRANCL 149
	163	FORMAT1,/,22X,22HTOTAL COOLANT FLOW IS ,F6.2,8H LB/SEC.)	TRANCL 150
		IFPRINT5,GT,3) WRITE(6,165) PTZ	TRANCL 151
152	165	FORMAT1,/,20X,26HTOTAL COOLANT PRESSURE IS ,F6.2,9H LB/SQIN.)	TRANCL 152
		CALL FLOWNOPTZ,PSJA,XX,L,KCCL)	TRANCL 153
	993	CONTINUE	TRANCL 154
		END	TRANCL 155

A-132

		SUBROUTINE SETFLO(IJK,L,PS3MIN,MT,UA,CPC,TT1,TS,PTZE,TTZE,K23,N23, 1A,PSJA,WZ,FR,TTZE) DIMENSION WTI(16),PTZE(16),PSJA(1),A(1),TTZE(1),WZ(60) REAL K23,N23 J=1 K=1 MT=0 WZ=EXP(UA/MT)*CPC*(600.1) TTZE=TS-(TTTS-TT1)/ZEJ PTZE=PSJMIN PTZE=PTZE*(1./J) MTI=0.0 IF(IJK-2) 40,61,81 DO 100 I=1,L Z2=PSJA(I)/PTZE IF(I77-1) 101,102,102 WZ(I)=0.0 GO TO 103 101 SQ4CH=12./(K23-1.1)*(177*(11.-K23)/(K23)-1.1) ZA=(PTZE*A(I)*N23*144.0)/SORT(TTZE) WZ=11.+(11*(K23-1.1)/2.1)*SQ4CH)**(11*(K23-1.1)/(K23-1.1) WZ(I)=SORT(132.174*K23*SQ4CH)/IRR*Z6)*ZA WZ=MTI*WZ(I) CONTINUE GO TO 110 100 DO 50 I=1,L IF(PTZE-PSJA(I)) 51,51,52 MOA=0.0 GO TO 53 51 S12=N23=117.6415*PSJA(I)/(1172E*TTZE(I)) MOA=(S12*23*(PTZE-PSJA(I))/(K23*(1./H23) WZ(I)=(MOA*WZ(I))/144.0 WZ=MTI*WZ(I) CONTINUE IF(ABS(WZ-MTI))-.01) 55,55,56 IF(ABS(JI)-101.57,50,55) MT=MT+1 WZ(MT)=WZ PTZE(MT)=PTZE IF(MT-WZ) 58,55,59 IF(ABS(JI)-101.60,61,60 IF(ABS(JI)-1) 63,63,5 J=J-3 GO TO 5 K=1 IF(MT-4) 5,64,64 IF(K-1) 5,65,65 CALL TABLE(WTI,PTZE,MT,PTZE,DUM,MT) J=1 GO TO 6 59 IF(ABS(JI)-101.65,5,66 65 IF(ABS(JI)-1) 5,5,67 J=J+6 GO TO 5 55 RETURN END	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57
--	--	--	--

2=7,30X, (SUBROUTINE FILMCL1=)		
	KOOL=0	FILMCL 59
68	GO TO 999	FILMCL 61
933	IF(MSET=0.0) 450,452,451	FILMCL 62
451	CALL SETFLOIDJ(N,SMALL,MSET,UA,CPC,TT1,TS,PT,TC,GAMMA,CDX,A,PS,	FILMCL 63
	1N2,R3,X11	FILMCL 64
	MT=MSET	FILMCL 65
65	GO TO 285	FILMCL 66
458	N=1.	FILMCL 67
	KM=0	FILMCL 68
	L1L=9	FILMCL 69
	KKA=2	FILMCL 70
70	KKA=0	FILMCL 71
13	ZE=EXP(UA/(M*CPC*3600.0))	FILMCL 72
	TC=TS-((TS-TT1)/ZE)	FILMCL 73
	SIGM12=(70.55*PT1)/(TC*TT1)	FILMCL 74
	WT=(SIGM12*(PT1-PT)/K12)**(1./N12)	FILMCL 75
75	IF(KKA=0) 51. 01 GO TO 237	FILMCL 76
	KKA=1	FILMCL 77
	M=MT	FILMCL 79
	GO TO 13	FILMCL 79
237	MTT=0.0	FILMCL 80
88	GO 232 I=1,N	FILMCL 81
	ZZ=PS11/PT	FILMCL 82
	IF(ZZ-1.) 300,381,301	FILMCL 83
381	NZ11=0.0	FILMCL 84
85	GO TO 302	FILMCL 85
380	SQACH=(2./(GAMMA-1.))*(ZZ**((1.-GAMMA)/GAMMA))-1.1	FILMCL 86
	ZA=(PT*AL1)*CDX*144.01/SQRT(TC)	FILMCL 87
	ZB=11.+(1/(GAMMA-1.))*(2.-SQACH)**((1-GAMMA)/GAMMA)-1.1	FILMCL 88
	WT11=SQRT((32.174*GAMMA*SQACH)/(RR*ZB))**ZA	FILMCL 89
302	MTT=ATT*WT11	FILMCL 90
282	CONTINUE	FILMCL 91
98	IF(L1L) 180,180,205	FILMCL 92
180	KM=KM+1	FILMCL 93
	IF(KM-3) 181,181,182	FILMCL 94
182	KM=1	FILMCL 95
95	KMT(KM)=MT	FILMCL 96
181	KMT(KM)=MT	FILMCL 97
	KPI(KM)=PT	FILMCL 98
	IF((ABS(KMT-MT))-0.1) 205,205,185	FILMCL 99
185	IF(KK) 402,402,400	FILMCL 100
402	IF(MT-MT) 400,40,60	FILMCL 101
60	MTMAX=(SIGM12*(PT1-SMALL)/K12)**(1./N12)	FILMCL 102
	IF(MT-MTMAX) 401,401,61	FILMCL 103
61	MT=MTMAX	FILMCL 104
481	N=0.25*MTT+.75*WT	FILMCL 105
105	PT=PT1-((K12/SIGM12)*(N**N12))	FILMCL 106
	GO TO 13	FILMCL 107
480	PCR=1.1	FILMCL 108
805	PT=XP(KM)+PCR	FILMCL 109
	IF(PT .LT. PT1) GO TO 804	FILMCL 110
110	PCR=PCR/10.0	FILMCL 111
	GO TO 405	FILMCL 112
884	KK=KK+1	FILMCL 113
	N=(SIGM12*(PT1-PT)/K12)**(1./N12)	FILMCL 114
	IF(KK-2) 13,13,405	FILMCL 115

115	485	IF(MTI-MT) 13,13,106	FILMCL	116
	406	CALL PSOLW(XMT,XMTI,XD,MT,DU,M,3)	FILMCL	117
		M=MT	FILMCL	118
		PT=PT1-(K12/5.0M2)*(M**N22)	FILMCL	119
		LL=1	FILMCL	120
120		GO TO 13	FILMCL	121
	285	RHO1=(144.*PT)/(R*TC)	FILMCL	122
		DO 3 I=1,N	FILMCL	123
		LL=0	FILMCL	124
		IF(V2(I).LE.0.1) GO TO 601	FILMCL	125
		RHO5=RHO1*(RPS(I)/PT)**1./GAMMA(I)	FILMCL	126
125		WC=Z(I)/(A(I)*RHO5)	FILMCL	127
		CALL TABLE(X1,XVC,XL(I),V,DU,M,K)	FILMCL	128
		IF(V2-VOL,4,5	FILMCL	129
		FV=1.+4.*AFAN(WG/VCI-1.0)	FILMCL	130
130		GO TO F	FILMCL	131
		FV=(V3/WG)**41.5*(WG/C)-1.01	FILMCL	132
		PAR12=1.+(RHO5*WC*OPC*51W,11/360R,1	FILMCL	133
	681	DO 11 K=1,N	FILMCL	134
		IF(ILL-0) 20,21,60	FILMCL	135
135		JA=1	FILMCL	136
		GO TO 22	FILMCL	137
	20	JA=2	FILMCL	138
		TRG(K,1)=TRG(K-1,3)	FILMCL	139
	22	DO 7 J=1,9	FILMCL	140
		XX=XL(KJ)*X(K,J)*COSTH(K)	FILMCL	141
		CALL TABLE(X1,XMG,XR,MG,DU,M,K)	FILMCL	142
		IF(I-1) 6,9,8	FILMCL	143
		CALL TABLE(X1,XTRG,XX,TRG,DU,M,K)	FILMCL	144
		TRG5=TRG	FILMCL	145
		GO TO 25	FILMCL	146
		TRG6=TRG1(K,J)	FILMCL	147
		IF(JA-1) 27,26,27	FILMCL	148
		XX=X(I,J)	FILMCL	149
		GO TO 10	FILMCL	150
		XX=(XX-XL(I))/COSTH(K)	FILMCL	151
		IF(MZ(I)-0.0) 602,602,683	FILMCL	152
		TRG6=TRG6	FILMCL	153
		GO TO 604	FILMCL	154
		PAR11=TRG6/TC**0.6667	FILMCL	155
		PAR13=PAR11*PAR12*FV	FILMCL	156
		TRG6=TRG6-TRG6/(1.0+3.6*(PAR13*XX*HQ1))+TRG6	FILMCL	157
		TRG1(K,J)=TRG6	FILMCL	158
		IF(K-1) 12,7	FILMCL	159
		TRG6=TRG6	FILMCL	160
		R(I)=((XX-XL(I))*(YU(I,M,1+J)-VL(I)))/(XU(I,M,1+J)-VL(I))	FILMCL	161
		CONTINUE	FILMCL	162
		IF(K-1) 11,15,11	FILMCL	163
		LL=1	FILMCL	164
		DO 14 M=1,8	FILMCL	165
		LL=1	FILMCL	166
		DVA(L)=PI*DX(I)*(R(M)*R(M+1))	FILMCL	167
		TA(I,1)=((TRG6/I,M)*TRG6/I,M+1)/2.0)	FILMCL	168
		CONTINUE	FILMCL	169
		CONTINUE	FILMCL	170
		CONTINUE	FILMCL	171
		DO 5 J I=1,M,N	FILMCL	172

175	LXLX(1)=LX(1M,I)*8 CONTINUE FORCE=0.0 SEC1=(GAMMA-1.0)/GAMMA SEC2=(RR*TT1)/(32.174*166.0) DO 720 I=1,N PRATE=(PSII)/PT I**SEC1 FORCE=FORCE+(INZ(I)*WZ(I))/(AI1I*PS(1I))*SEC2*PRAT*COSTH(1I) CONTINUE	FILMCL 173 FILMCL 174 FILMCL 175 FILMCL 176 FILMCL 177 FILMCL 178 FILMCL 179 FILMCL 180 FILMCL 181 FILMCL 182 FILMCL 183 FILMCL 184 FILMCL 185 FILMCL 186 FILMCL 187 FILMCL 188 FILMCL 189 FILMCL 190 FILMCL 191 FILMCL 192 FILMCL 193 FILMCL 194 FILMCL 195
180	IFIPRINTS .GT. 0) WRITE(6,733) IABC FORMAT(1H1,/,20X,12H FILM COOLING,/,27X,12H SURFACE NO. ,I2,/) CALL AVE(10X,1AI,1XLY,MODE=MM,1H,PRINT5) IFIPRINTS .GT. 0) WRITE(6,160) M FORMAT(//,22X,22HTOTAL COOLANT FLOW IS ,F6,2.0H LB/SEC,1	
185	IFIPRINTS .GT. 0) WRITE(6,165) PT FORMAT(//,20X,26HTOTAL COOLANT PRESSURE IS ,F6,2.0H LB/SQIN,1	
190	IFIPRINTS .GT. 0) WRITE(6,735) FORCE FORMAT(//,13X,12HTOTAL RESULTANT SLOT COOLANT MOMENTUM FLUX IS ,F7,2.0H LB,1 CALL FLOWNC(PT,PS,XL,N,KOOL) FS(1)=FORCE 999 CONTINUE END	

Line	Code	Statement	Address
5		SUBROUTINE SETFLOUT(L,K,L,PS3MIN,WT,UA,CPC,TTL,TS,PTZE,TTZE,K23,N23, IA,PS1A,W2,RN,TTZE) DIMENSION WTI(10),PTZE(10),PS3A(1),A(1),TTZE(1),W2(10) REAL K23,N23 J=1 K=1 N=0 Z=EXP(UA/WT+CPC*360.1) TTZE=TS-(TTT-TTL)/ZE PTZE=PS3MIN PTZE=PTZE+(1./J) WTL=J*U IF(J,K-2) 60,61,61 DO 100 I=1,L Z2=PS3A(I)/PTZE IF(I77-1) 101,102,102 W2(I)=Z*Z GO TO 103 101 SOMACH=Z/(K23-1.)*(127+111*(K23/K231)-1.) ZA=PTZE+3.11*(N23+44.C)/SQRT(TTZE) ZB=11.+(11*(K23-1.)/2.)*SOMACH*(11*(K23+1.)/(K23-1.)) W2(I)=S23*(132.17*(K23+SOMACH)/100+ZB1)*ZA WTL=WT+W2(I) 103 CONTINUE GO TO 113 102 DO 50 I=1,L IF(PTZE-PS3A(I)) 51,51,52 W0A=Z*.C GO TO 51 51 S13=C23=(17.6+15*PS3A(I))/(TTZE+TTZE(I)) W0A=S13*W23*(PTZE-PS3A(I))/(K23)*(11*(K23+1.)) W2(I)=(W0A+PTZE)/144.C WTL=WT+W2(I) CONTINUE IF(I(ABS(WT-WTL))-10) 55,55,56 IF(I(ABS(JJ)-10) 57,56,55 N=NT+1 WTL=WT+1 WTL=NT+1 WTL=NT+1 PTZE(N)=PTZE IF(WT-WTL) 59,55,59 IF(I(ABS(JJ)-10) 60,61,60 IF(I(ABS(JJ)-1) 63,63,5 J=-J+3 GO TO 5 GO TO 5 K=1 IF(WT-4) 5,5,6,6 IF(K-1) 5,6,6,6 CALL LABEL(L,WTL,PTZE,L,WT,PTZE,DWR,MT) J=1 GO TO 6 IF(I(ABS(JJ)-10) 66,5,66 IF(I(ABS(JJ)-1) 5,5,67 J=-J+6 GO TO 5 RETURN END	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57

[illegible]

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      ASI(J) = 3.14159*(R(IW,J)-SH(IW,J)*COS(ANG(J)*(RIW,J+1))*SL(J)
      ASI = ASI + ASI(J)
      DO 71 I=1,NM1
        REN(I) = ALOG(REN(I))
        FL(I) = ALOG(FL(I))
        WPL(I) = ALOG(WPL(I))
      71 * * * COCLANT FLOW BALANCE * * *
      M1=1
      PMAX=PS(I1)
      PMIN=PS(I1)
      DO 262 I=2,N
        IF(PS(I1)-PMIN) 265,263,261
        IF(PS(I1)-PMAX) 262,262,264
      265 PMIN=PS(I1)
      263 IF(PS(I1)-PMAX) 262,262,264
      264 PMAX=PS(I1)
      262 CONTINUE
      IF(PS(I1)-GT,0.01) GO TO 1300
      IF(PI,LT,PMIN) GO TO 203
      IF(PI,LT,4) GO TO 275
      DO 271 J=1,M2
        SH(IW,J) = SH(IW,J+1)
      271 KSH(IW,J) = KSH(IW,J+1)
      275 K=1
      M=0
      L=1
      J=1
      * * * SOURCE FLOW PRESSURE-FLOW BALANCE * * *
      IF(PS(I1)-GT,0.1) GO TO 219
      IF(PI,GT,1) GO TO 201
      KKK=J
      M=10
      PI2(I1)=PI1-0.2*(PI1-PMIN)
      201 M=M+3
      KKK=KKK+1
      IT2=IS-(IS-IT1)/EXP(UAS/(864.0*MA))
      SI2=SI*(PI1-PI2(I1))/(IT1+IT2)
      M3=(SI2*(PI1-PI2(I1))/K12)*((I1/N12)
      CX=(I49-MA)/M3
      IF(ASSTOCK)-01) 204,204,202
      202 IF(KKK,LT,20) GO TO 201
      207 WRITE (6,117)
      STOP
      100 213 WRITE(6,116)
      MTC=0
      GO TO 70
      214 MTC(J)=M3
      KKK=J
      105 MAXX=(SI2*(PI1-PMIN)/K12)*((I1/N12)
      * * * DISCHARGE PRESSURE-FLOW BALANCE * * *
      254 MCT(J)=0.0
      DO 225 I=1,M3
        K1=J
      110 IF(PI2(J)-PS6(I)) 206,206,207
      206 MCT(I)=0.0
      IF(M1,EO,1) TSS(I)=T12
      GO TO 213

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CONFLM 59
CONFLM 60
CONFLM 61
CONFLM 62
CONFLM 63
CONFLM 64
CONFLM 65
CONFLM 66
CONFLM 67
CONFLM 68
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CONFLM 70
CONFLM 71
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CONFLM 109
CONFLM 110
CONFLM 111
CONFLM 112
CONFLM 113
CONFLM 114
CONFLM 115

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115	207 IF(M1-1) 208,209,209	CONFIRM	116
	208 IF(K-1) 210,210,209	CONFIRM	117
	210 MCO=WT(J)*AS(I)/AST	CONFIRM	118
	TS5(I) = Y12	CONFIRM	119
	GO TO 211	CONFIRM	120
121	209 IF(WCII,GI,0,00W1) GO TO 256	CONFIRM	121
	WCII = 0.1	CONFIRM	122
	256 MCO=WC(I)	CONFIRM	123
	211 S5=35.31*PS6(I)/TS5(I)	CONFIRM	124
125	255 FM=MCO*SORT(TT2)/(AHX(I)*AP*PT2(J))	CONFIRM	125
	K1J=K10+1	CONFIRM	126
	CALL TABLE(MCF1,MN1,FM,MN,QU,MN3)	CONFIRM	127
	TR=1/(1+.2*MN**2)	CONFIRM	128
	PR=TR**3.5	CONFIRM	129
	PEN=ALCG(51840C,HD*MCO/(AHX(I)*.0005336*(TT2*Y12)**.70411)	CONFIRM	130
130	IF(PEN,GT,FENL(MN1)) REN=REN(MN1)	CONFIRM	131
	IF(PEN,LT,RENLI)) REN=RENLI)	CONFIRM	132
	CALL TABLE(PEML,FL,PEN,FF,QU,MN1)	CONFIRM	133
	WFS=SL(I)*Y12*TR*EXPIFFI/(3.621*WD*PT2(J)*PR*(AHX(I)*AR)**2)	CONFIRM	134
135	WCII=SO*Y12*PT2(J)-PS6(I)/(HMF+K5(MN,II/S5))	CONFIRM	135
	CK=WC(I)-MCO/MC(I)	CONFIRM	136
	IF(M3SICK)-.005) 213,213,261	CONFIRM	137
	MCO = MCO(I)	CONFIRM	138
	261 MCO = MCO(I)	CONFIRM	139
	IF(X1C-20) 255,307,307	CONFIRM	140
140	213 MCT(I) = MCT(J)+MCT(I)	CONFIRM	141
	205 CONTINUE	CONFIRM	142
	IF(K-2) 214,214,215	CONFIRM	143
145	214 CK=(MCT(J)-WT(J))/MCT(J)	CONFIRM	144
	IF(M3SICK)-0.003) 215,215,216	CONFIRM	145
	216 IF(MSET,GT,0.0) GO TO 218	CONFIRM	146
	IF(K-1) 220,220,221	CONFIRM	147
	220 K=2	CONFIRM	148
	IF (MCT(J)-WT(J)) 222,222,223	CONFIRM	149
	222 LO=2	CONFIRM	150
	GO TO 224	CONFIRM	151
150	223 LO=1	CONFIRM	152
	234 IF (MCT(J)-WMAX) 224,224,225	CONFIRM	153
	224 W9=14*Y12*(J)/2.	CONFIRM	154
	GO TO 235	CONFIRM	155
155	225 W9=14*Y12*(J)+WMAX)/2.	CONFIRM	156
	235 J=J+1	CONFIRM	157
	IF(J-4) 226,227,227	CONFIRM	158
	227 GO 228 JJ=1,2	CONFIRM	159
	WT(J)=WT(JJ+1)	CONFIRM	160
	PT2(JJ)=PT2(JJ+1)	CONFIRM	161
160	228 MCT(JJ)=MCT(JJ+1)	CONFIRM	162
	J=3	CONFIRM	163
	226 IF(LL,GT,1) GO TO 240	CONFIRM	164
	PT2(J)=PT1-K12*(M8*M12)/S12	CONFIRM	165
	GO TO 201	CONFIRM	166
165	240 PT2(J)=PT2(J-1) + 7	CONFIRM	167
	IF(PT2(J).LT. P11) GO TO 231	CONFIRM	168
	Z=Z+.0	CONFIRM	169
	GO TO 240	CONFIRM	170
170	221 IF (LO-1) 229,229,230	CONFIRM	171
	229 IF(MCT(J)-WT(J)) 231,231,232	CONFIRM	172
	232 IF(LL-1) 234,234,235	CONFIRM	173

233	IF(LJ-3) 231,236,236	CONFLM	173
236	DO 933 JA=313	CONFLM	174
	MT50(JA)=MT(JA)	CONFLM	175
175	MT53/JA=MT(JA)	CONFLM	176
933	PS(JA)=PT2(JA)	CONFLM	177
	CALL PSOL(MT50,MT53,PSA,PSB,PS3)	CONFLM	178
	PT2(J)=P	CONFLM	179
	K=3	CONFLM	180
180	GO TO 254	CONFLM	181
	Z=C+1	CONFLM	182
231	LL=2	CONFLM	183
	Z=C+1	CONFLM	184
	M=MT(J)	CONFLM	185
185	GO TO 235	CONFLM	186
230	IF (LL-1) 237,237,238	CONFLM	187
237	IF(LJ-1) KCT(J) 238,239,224	CONFLM	188
239	LL=2	CONFLM	189
	Z=C+1	CONFLM	190
	M=MT(J)	CONFLM	191
190	GO TO 235	CONFLM	192
239	IF(LJ-1) KCT(J) 235,235,241	CONFLM	193
241	IF(LJ-3) 235,236,236	CONFLM	194
243	IF(LJ-1) 242,242,243	CONFLM	195
	MT(J)=MCT	CONFLM	196
195	ITZ=IS-ITL/EXP(JNSC(864,9)SETI)	CONFLM	197
	PT2(J) = PHAX + 1.	CONFLM	198
	GO TO 254	CONFLM	199
240	IF(LJ-1) 242,242,243	CONFLM	200
242	K=2	CONFLM	201
243	IF(LJ-1) 242,242,243	CONFLM	202
	Z=J+249	CONFLM	203
246	IF(J-EO,4) GO TO 267	CONFLM	204
	J = J + 1	CONFLM	205
205	GO TO 269	CONFLM	206
267	DO 269 I=2,4	CONFLM	207
	MT(J)=13-MCT(J)	CONFLM	208
268	PT2(I-10=PT2(I)	CONFLM	209
269	MT(J)=ASET	CONFLM	210
210	PT2(J)=PT2(J-1)+2	CONFLM	211
	GO TO 254	CONFLM	212
245	LO=1	CONFLM	213
	Z=-0,249	CONFLM	214
	GO TO 246	CONFLM	215
215	IF(LJ-1) 247,247,248	CONFLM	216
247	IF(MCT(J)-MSET) 249,249,250	CONFLM	217
249	LL=2	CONFLM	218
	Z=C+05	CONFLM	219
220	GO TO 246	CONFLM	220
220	IF(LJ-1) 246,246,251	CONFLM	221
251	IF(MJ-3) 270,252,252	CONFLM	222
249	IF(MCT(J)-MSET) 250,250,260	CONFLM	223
263	IF(LJ-1) 253,253,270	CONFLM	224
225	LL=2	CONFLM	225
253	Z=C+05	CONFLM	226
	GO TO 246	CONFLM	227
252	IF(LJ-1) 252,252,259	CONFLM	228
	GO TO 259	CONFLM	229

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238      DO 257 I=1,N
          JJ = 5-I
          TA(I)=WCT(JJ)
257      A(I)=PT2(JJ)
          DO 258 I=1,N
              WCT(I)=TA(I)
235      P12(I)=A(I)
259      CALL TABLE(WCT,PI2,HSET,P,DUM,N)
          PT2(I)=P
          K=3
          GO TO 254
241      215 WCT(I)=WCT(J)
          PT2(I)=PT2(J)
          DO 242 J=1,M
              DO 241 I=1,INC
245      281 TG(J,I) = TRG(J,I)
          282 CONTINUE
          MYE=0
          DO 21 J=1,NC
              IF(MC(J).GT. 0.0003) GO TO 295
              DO 296 I=1,INC
                  296      TN(J,I)=TG(J,I)
                  GO TO 21
295      ASHX=SVHX*AMX(J)*SL(J)/12
          CALL TABLE(TN,MCL,XIM,J),MG,DUM,MN4)
          KKS = 0
          C * * * BRANCH FOR TYPE CONFIGURATION - PARALLEL OR COUNTERFLOW * *
          IF (NTC=1) 2,3,3
          C * * * PARALLEL FLOW THERMAL ANALYSIS * * * * *
          3      TC(J,I) = TCS
          IF(J.GT.1) GO TO 4
          IF(J,1) = TG(J,1)
          4      SX=0.0
          DO 7 I=2,INC
              VIS = 0.005536*TC(J,I-1)**.7861
              REN=ALOG(518400./WD*MC(J)/VIS)*AMX(J)*AR(I)
              IF(IPEN.GT.PENL(MN3)) REN=RENL(MN3)
              IF(IPEN.LT.PENL(1)) REN=RENL(1)
              CALL TABLE(REN,MXP,REN,MXP,DUM,MN3)
              CALL PRDNT(TC(J,I-1),PR)
              MHX=.24*MC(J)*EXP(MXP)/(AMX(J)*AR*(PR)**.6667)
              UA = 1./((1/(MHX*AEFF*ASHX)) + 518400./VHX*AS(J))
              C=UA*OSL(J)/(.24*SL(J)*MC(J))
              IF(J.GT.1) GO TO 10
              TFC(J,I) = TG(J,I)
          10      TFB = (TFC(J,I)+TFC(J,I-1))/2.
              TC(J,I) = TFB-(TFB-TC(J,I-1))/(EXP(DI))
              TM(J,I) = UA*(TFC(J,I)/(MHX*AEFF*ASHX)+518400./VHX*AS(J))
              IF(I.GT.2) GO TO 7
              TM(J,I)=UA*(TFC(J,I)/(MHX*AEFF*ASHX)+518400./VHX*AS(J))
          7      CONTINUE
          IF(MC.GT.J) GO TO 8
          IF(M.GT.MC) GO TO 8
          ANG(J,I) = 0.0
          8      ACD= 78310*(PI(M,J)-.5*SH(M,J)*COS(ANG(J,I)))*SH(M,J)
              TFC(J,I)=TFC(J,I)+ACD*PS(J)
              MCF=MC(J)*CONT(TFC(J,I,1))/1.93*ACD*PS(J)

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Line	Code	Text	Variable
297	CONF	CALL TABLE(MCF1,MN1,FM,MN,DUM,MN3)	CONF
298	CONF	TR=1/(1+2*MN**2)	CONF
299	CONF	TS(1)=TR	CONF
300	CONF	VCO = 53.35*MC*TR*SORT(TF(1),1)	CONF
301	CONF	W=MC*VCO*MC(1)*COS(TANG(1))/32.176	CONF
302	CONF	IF(MC(1).GT.1) GO TO 5	CONF
303	CONF	IF(MN.EQ.NC) GO TO 21	CONF
304	CONF	5 CALL TABLE(X1,VG1,X(1),J(1),VC,DUM,MN4)	CONF
305	CONF	IF(VG-VCO) 2,299,299	CONF
306	CONF	GO TO 10	CONF
307	CONF	298 FV=1+4*ATAN(VG/VCO-1.)	CONF
308	CONF	299 FV=VCO/21*(1.5*(VCO/VG-1.))	CONF
309	CONF	310 CG=MG*ACQ/(MCD(1)*SH(1),J(1),244,16.)	CONF
310	CONF	SX=0.0	CONF
311	CONF	JJ=J(1)	CONF
312	CONF	CALL TABLE (X1,MG1,X(1),JJ,VC,DUM,MN4)	CONF
313	CONF	DO 9 M=JJ,N	CONF
314	CONF	DO 299 I=2,INC	CONF
315	CONF	SX=SX+DCL(I)	CONF
316	CONF	EFF=1/(1+3.65*SX*(TGM(1)/TF(1),1))**6667*V*CC)	CONF
317	CONF	TFM(1)=TGM(1)-EFF*(TGM(1)-TF(1),1)	CONF
318	CONF	TFM(1) GO TO 9	CONF
319	CONF	TGM(1)=TFM(1,INC)	CONF
320	CONF	DO 298 I=2,INC	CONF
321	CONF	TGM(1)=TFM(1)	CONF
322	CONF	9 CONTINUE	CONF
323	CONF	GO TO 21	CONF
324	CONF	C * * * CCOUNTS FLOW THERMAL ANALYSIS * * * * *	CONF
325	CONF	2 IF(M1-1) 277,277,25	CONF
326	CONF	277 IF(1,1)=TG(1,1)/12+11CS)*.6667	CONF
327	CONF	TC(1,1)=TF(1,1)	CONF
328	CONF	CALL T	CONF
329	CONF	ACQ=6.261A*(TC(1,1)-.5*SH(1,1)*COS(TANG(1)))*SM(1,1)	CONF
330	CONF	MC=MCD(1)*SORT(TF(1),1)/(6.960*ACQ*PS(1))	CONF
331	CONF	CALL TABLE(MCF1,MN1,MCF,MN,DUM,MN3)	CONF
332	CONF	IRE=1/(1+2*MN**2)	CONF
333	CONF	TS(1)=IRE*TF(1,1)	CONF
334	CONF	VCO = 53.35*MC*TR*SORT(TF(1),1)	CONF
335	CONF	W=MC*VCO*MC(1)*COS(TANG(1))/32.176	CONF
336	CONF	IF(V5-VCO) 302,312,311	CONF
337	CONF	IF(V5-VCO) 302,312,311	CONF
338	CONF	GO TO 301	CONF
339	CONF	302 FV=VCO/VG1*(1.5*(VCO/VG-1.))	CONF
340	CONF	313 CC = MG*ACQ/(MC(1)*SH(1,1)*1244,16.)	CONF
341	CONF	SX = 0.0	CONF
342	CONF	DO 19 I=2,INC	CONF
343	CONF	SX = SX + DCL(I)	CONF
344	CONF	EFF = 1/(1+3.65*SX*(TGM(1)/TF(1),1))**6667*V*CC)	CONF
345	CONF	TF(1,1)=TG(1,1)-EFF*(TG(1,1)-TF(1,1))	CONF
346	CONF	TF(1,1)=TG(1,1)-EFF*(TG(1,1)-TF(1,1))/2.	CONF
347	CONF	VIS = 6.0355336*TC(1,1)-11**7641	CONF
348	CONF	CALL PRN(1,TC(1,1),PR)	CONF
349	CONF	REN = ALOG(518.00-4*MC(1)/VIS*AN(XJ)*ARI)	CONF
350	CONF	IF(REN.GT.REN(1,N1)) REN=REN(1,N1)	CONF
351	CONF	IF(REN.LT.REN(1,1)) REN=REN(1,1)	CONF
352	CONF	CALL TABLE(REN,HYP,REN,HYP,DUM,MN1)	CONF
353	CONF	HMX = 26*MC(1)*EXP(HYP)/(14HXJ)*AR*(PP)**.6667)	CONF

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345      UA = 1./I1/(IMX*AEFF*ASHX) + 510400./(HGP*AS(J))
      C = UA*DSL(J)/I1.24*SL(J)*WC(J)
      TC(J,I)=TFB - (TFB-TC(J,I-1))*EXP(C)
      19  TC(J,I) = UA*(TF(J,I)/(IMX*AEFF*ASHX) + 510400./(HGP*AS(J)))
      DTCS = TC(J,INC)-TCS
      KKK = KKK + 1
      IF (ABS(DTCS) - J.123.23.24
350      TF(J,I) = TC(J,I) - .0*DTCS
      TC(J,I) = TC(J,I)
      IF (KKK-20) 25,62,62
      62  WRITE (6,101)
      STOP
355      23  TMI(J,I) = TF(J,I)
      TC(J,INC) = TCS
      IF (N-J) 21,21,41
      41  SXX = SX
      JJ = J+1
      DO 34 M=JJ,M
360      SXX = SXX - DSL(M)
      DO 34 K = 1,INC
      SXX = SXX + DSL(M)
      EFF = 1./I1.43.5*5XX*(TG(M,K)/(TF(J,I))*.6667*FY*CC)
365      34  TG(M,K) = TG(M,K) - EFF*(TG(M,K) - TF(J,I))
      21  CONTINUE
      M2=5*NC
      IF (MTC,LT,4) GO TO 293
      JK1=1
      JK2=NC
      GO TO 294
      293  JK1=2
      JK2=NC+1
      294  IF (M1-1) 273,273,276
      276  DO 272 I=JK1,JK2
      IF (ABS(TF(I,1)-TCX(I,1))-5.1 272,272,273
      272  CONTINUE
      GO TO 283
      273  M1=M1+1
      DO 274 I=JK1,JK2
      274  TCX(I)=TF(I,1)
      IF (M1-M2) 279,279,288
      279  GO TO 275
      280  WRITE (6,101)
      STOP
      385      283  IF (MTC-4) 35,13,13
      35  IF (MTC-EO,N) GO TO 36
      TMIN,1) = TM (N-1,INC)
      DO 37 K=2,INC
      37  TMIN,K) = TG(M,K)
      GO TO 36
      13  IF (MTC-EO,N) GO TO 36
      DO 6 I=1,INC
      6  TMIN,I)=TF(M,I)
      C * * * SURFACE TEMPERATURE AVERAGING * * * * *
      36  K = INC - 1
      DO 17 J=1,M
      TSUM=C.C
      DO 15 I=2,K

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400	18	TSM=TSUM+T(W(J,I)+R(W,J+1)+SL(W)-DSL(W)*I-1)*SIN(W(J,I))	CONF.LM	401
		T(W(J,I))+R(W,J)+SL(W)-DSL(W)*I/4)*SIN(W(J,I))	CONF.LM	402
		T(W(J,I))+R(W,J)+SL(W)-DSL(W)*SIN(W(J,I))/4)	CONF.LM	403
		A(W)=SL(W)*R(W,J+1)+SL(W)*SIN(W(J,I))/2)*6.28	CONF.LM	404
405	17	T(W(J,I))+SL(W)-DSL(W)*I+2)*SIN(W(J,I))/4)	CONF.LM	405
		I(W(J,I))+R(W,J)+SL(W)-DSL(W)*I/4)	CONF.LM	406
		FORMAT(IH,/,2X,23HCONVECTION-FILM COOLING,27X,12HSPACE NO. ,	CONF.LM	407
		A12,/))	CONF.LM	408
		DO 410 I=1,N	CONF.LM	409
410	433	LC(W)=L(W,I)	CONF.LM	410
		CALL AVER(LA,LC,W,MODE,MAB,IN,PRINT9)	CONF.LM	411
		IF(PRINTS.GT.0) WRITE(5,115) W(I),PT(2),W	CONF.LM	412
		105 FORMAT(//,22X,22HCOOLANT FLOW IS ,F6.2,8H LB/SEC.	CONF.LM	413
		2 /,20X,26HCOOLANT PRESSURE IS ,F5.2,9H LB/SQIN.	CONF.LM	414
		3 /,13X,17HCOOLANT RESULTANT SLOT COOLANT MOMENTUM FLUX IS ,	CONF.LM	415
415		F5.2,7H LB-FT	CONF.LM	416
		PSI(W)=W	CONF.LM	417
		DO 431 I=1,N	CONF.LM	418
		T(W(I))+R(W,I)	CONF.LM	419
420	434	IF(W(I).GT.0) GO TO 433	CONF.LM	420
		DO 436 I=1,N	CONF.LM	421
		PS(W(I))+R(W,I)	CONF.LM	422
		CALL FLOW(W(I),Z(I),PS(W,I),W(NIC))	CONF.LM	423
		72 CONTINUE	CONF.LM	424
425		END	CONF.LM	425
			CONF.LM	426

SUBROUTINE PRND11 (T,PR)

IF (T-900.1) 1,1.2

1 PR=.76-.000157

GO TO 3

2 IF (T-1400.1) 4,5

4 PR=.705-.000041

GO TO 3

5 PR=.65

3 CONTINUE

RETURN

END

PRND11 2
PRND11 3
PRND11 4
PRND11 5
PRND11 6
PRND11 7
PRND11 8
PRND11 9
PRND11 10
PRND11 11
PRND11 12

	OVERLAYIRNO,11,N1	CALFOR	2
	PROGRAM CALFOR	CALFOR	3
	COMMON/ALL/ H,NM,NM,ISURF(50),NODE(55),JSURF(5,20),X(15),NTOT(1,	CALFOR	4
5	NO,NPID(1), AREA(80)	CALFOR	5
	COMMON /LINK6/ A(11100), K(12,20), V(12,20), L(12,20), IM, IABC	CALFOR	6
	COMMON /KOC/ KOC(12)	CALFOR	7
	COMMON /RAB/ NODE(15(50),FT(150),LUI	CALFOR	8
	COMMON /CCG/ FS(2)	CALFOR	9
	FORCE=0.0	CALFOR	10
10	J=1	CALFOR	11
	WRITE(6,1)	CALFOR	12
	FORMAT(14,1,7,20X,"SYSTEM SURFACE FORCE FACTORS"/,7,20X,"NODE NO,"	CALFOR	13
	1,15X,"FORCE FACTOR (LB,")	CALFOR	14
15	FORMAT(23,12,21X,F9.3)	CALFOR	15
	LINE=6	CALFOR	16
	DO 5 I=1,LUI	CALFOR	17
	IF(I,FO, NODE(15(I)) GO TO 10	CALFOR	18
	CONTINUE	CALFOR	19
20	IF(LINE,50,59) GO TO 3	CALFOR	20
	WRITE(6,2) NODE(15(I),FT(11)	CALFOR	21
	FORCE=FORCE+FT(11)	CALFOR	22
	J=J+1	CALFOR	23
	LINE=LINE+1	CALFOR	24
25	IF(J,GT,LUI) GO TO 58	CALFOR	25
	GO TO 7	CALFOR	26
	WRITE(6,11)	CALFOR	27
	LINE=6	CALFOR	28
	GO TO 11	CALFOR	29
	DO 61 K=1,NM	CALFOR	30
	IF(KO,L(K),GT,1) GO TO 51	CALFOR	31
	CONTINUE	CALFOR	32
	GO TO 70	CALFOR	33
	FORMAT(16,"COOLANT SLOT DISCHARGE FLOW FACTOR")	CALFOR	34
	WRITE(6,N)	CALFOR	35
35	DO 65 K=1,IM	CALFOR	36
	WRITE(6,3) FS(K)	CALFOR	37
	FORMAT(45X,F9.3)	CALFOR	38
	FORCE=FORCE+FS(K)	CALFOR	39
	WRITE(6,9) FORCE	CALFOR	40
40	FORMAT(15,"TOTAL NET SURFACE FORCE FACTOR",BY,F9.3)	CALFOR	41
42	END	CALFOR	42

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OVERLAY(XRHP,11,3)
PROGRAM HOTPT
COMMON XL(100),ACROSS(80),
1YLI( 80),YLC( 80),PPI(50),AA(150),XMM1(150),XMM2(150),TRS(150),
5 2DEMP1(150),VPP(150),TRP(150),DEMS1(150),VSS(150),PT(100),
3XMSI( 80),ISI( 80),DENSEI( 80),VSEI( 80),XMPI( 80),TPI(100),
4DEMP(100),VPT(100),L,LL
COMMON/ALL/ N,MN,NN,XSURF(50),MODE(50),JSURF(5,2),XF(5),XTOTA,
NOP,NP(10), AREA(80)
10 COMMON /LINK6/ MII(100), YN(2,20), YN2(20), LY(2,20), IW, IABG
COMMON /PRINT/ PRINT1, PRINT2, PRINT3, PRINT4, PRINT5, PRINT6,
PRINT7, PRINT8, PRINT9, PRINT10, PRINT11, PRINT12, PRINT13, PRINT14,
PRINT15, PRINT16, PRINT17, PRINT18, PRINT19, PRINT20, PRINT21, PRINT22,
PRINT23, PRINT24, PRINT25, PRINT26, PRINT27, PRINT28, PRINT29, PRINT30,
PRINT31, PRINT32, PRINT33, PRINT34, PRINT35, PRINT36, PRINT37, PRINT38,
PRINT39, PRINT40, PRINT41, PRINT42, PRINT43, PRINT44, PRINT45, PRINT46,
PRINT47, PRINT48, PRINT49, PRINT50, PRINT51, PRINT52, PRINT53, PRINT54,
PRINT55, PRINT56, PRINT57, PRINT58
COMMON /MOT/ AT,CF(1100),CHIA(15),CTHIA(15),FFT,FPAT,MGAT,MIA(5,2),
1ICS,ICSUFF(15),II,IKJ,ISTREM(15),KK(15),KCSURF(15),MODEN(5,20),M1,M2,
15 2PTP,PTS,THETA(5,2),TTP,TT5,XF1,XI(5),YU1(20),YU2(20),X11(60),
3YU1(20),YU2(20),Y11(20),I,KAI(5,2)
INTEGER PRINT1,PRINT2,PRINT3,PRINT4,PRINT5,PRINT6,PRINT7,PRINT8
1,PRINT9,PRINT10
IF(KAI(1,1)) 31,31,32
IF(II-1) 33,33,34
31 CALL HEAT(XI(1),XF(1),TTS,PTS,THETA(1,1),MIA(1,1),YL,Y11,XMST,
33 1TST,CTHETA,CHIA,X11,Y11,MT11,IKJ,
2ICSURF,ICS,PRINT2,II,CF(1)
CALL AVER(XI(1),Y11,MT11,YU1,YU2,ICS,ICSURF,M1,IKJ,JSURF(1,1),
25 1KSURF,MODEN,MN,PRINT3,MGAT,AT)
IF(PRINTO .EQ. 0) GO TO 450
CALL AVER(XI(1),Y11,CF(1),YU1,YU2,ICS,ICSURF,M1,IKJ,JSURF(1,1),
1KSURF,MODEN,MN,XMST,PT,1,4,II,FPAT,FFT)
GO TO 850
31 34 CALL HEAT(XI(1),XF1 ,TTS,PTS,THETA(1,1),MIA(1,1),YL,Y12,XMST,
1TST,CTHETA,CHIA,X11,Y11,MT11,IKJ,
2ICSURF,ICS,PRINT2,II,CF(1)
CALL AVER(XI(1),Y11,MT11,YU2,YU2,ICS,ICSURF,M2,IKJ,JSURF(1,1),
35 1KSURF,MODEN,MN,PRINT3,MGAT,AT)
IF(PRINTO .EQ. 0) GO TO 850
CALL AVER(XI(1),Y11,CF(1),YU2,YU2,ICS,ICSURF,M2,IKJ,JSURF(1,1),
1KSURF,MODEN,MN,XMST,PT,1,4,II,FPAT,FFT)
GO TO 450
32 IF(II-1) 35,35,360
32 35 CALL HEAT(XI(1),XF(1),TTP,PTP,THETA(1,1),MIA(1,1),YL,Y11,XMPI,
1TPI,CTHETA,CHIA,X11,Y11,MT11,IKJ,
2ICSURF,ICS,PRINT2,II,CF(1)
CALL AVER(XI(1),Y11,MT11,XU1,YU1,ICS,ICSURF,M1,IKJ,JSURF(1,1),
45 1KSURF,MODEN,MN,PRINT3,MGAT,AT)
IF(PRINTO .EQ. 0) GO TO 850
CALL AVER(XI(1),Y11,CF(1),XU1,YU1,ICS,ICSURF,M1,IKJ,JSURF(1,1),
1KSURF,MODEN,MN,XMPI,PT,1,35,II,FPAT,FFT)
GO TO 850
360 IF(NOP .EQ. N) GO TO 36
51 IF(KK(1) .EQ. 0) GO TO 36
M2=N2-1
IF(XI(1) .GE. YU2(N2)) GO TO 850
XF1=YU2(N2)
35 36 CALL HEAT(XI(1),XF1 ,TTP,PTP,THETA(1,1),MIA(1,1),YL,Y12,XMPI,
1TPI,CTHETA,CHIA,X11,Y11,MT11,IKJ,
2ICSURF,ICS,PRINT2,II,CF(1)
CALL AVER(XI(1),Y11,MT11,YU2,YU2,ICS,ICSURF,M2,IKJ,JSURF(1,1),
58 1KSURF,MODEN,MN,PRINT3,MGAT,AT)

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SUBROUTINE AVERHT(X,Y,HC,KU,YU,ICS,ICSURF,M,KP,IRF,KSURF,
1MODE,NNN,PRINTS,HGAT,AT)
DIMENSION X(1),Y(1),HC(1),YU(1),KSURF(1),NCOE(15,20),
1ICSURF(1)
INTEGER PRINTS
COMMON/AA/ NMODE(150),NII(150),LU
LU=0
IF(P=INT3.EQ. 0) GO TO 300
WRITE(6,101)
FORMAT(1H1,/,/,2X,3HAY=,E,5AT TRANS, R COEFFICIENTS,/,31X,10H10
1TU/SOFT,HR,DEGL,/)
KP=KP-1
300
KK=1
DO 73 JJJ=1,NNN
IF(KSURF(JJJ).EQ. JSURF) GO TO 71
CONTINUE
73
71
IF(ICS .GT. 0) GO TO 200
M=J
GO TO 72
200
DO 201 KU=1,ICS
IF(ICSURF(KU).EQ. JSURF) GO TO 202
CONTINUE
201
M=0
GO TO 72
25
202
CALL STORE(HGAT,AT,JJJ,1)
M=1
72
DO 6 J=1,N
IF(X(1).LT. XU(J)) GO TO 7
CONTINUE
6
7
J=J-1
DO 13 JJ=J,N
IF(M.GT. 0) GO TO 2
HGAT=0.0
AT=0.0
35
2
DO 12 K=K,KP
IF(X(K+1).GT. XU(JJ+1)) GO TO 13
XL=STRT((X(K)-X(K+1))*(X(K)-X(K+1)))+(Y(K)-Y(K+1))*Y(K+1))
13
A=3.14159*XL*(Y(K)+Y(K+1))
MGA=(MG(K)+MG(K+1))/2.0
HGAT=HGAT+(MGA*A)
AT=AT+A
DIFF=ABS(X(K+1)-XU(JJ+1))
IF(DIFF.LT. 0.01) GO TO 50
GO TO 11
50
HGAT=HGAT/AT
IF(PRINTS.EQ. 0) GO TO 301
WRITE(6,100) NMODE(JJJ,JJJ),HGAT,AT
100
F=HAT(13X,9HNODE NO. ,12,/,29X,15HNT COEFFICIENT ,F0.3,/,26X,13HSUR
1LU=LU+1
50
301
NMODE(1,LU)=NMODE(JJJ,JJ)
HT(LU)=HGAT/144.0
M=J
55
IF(K.EQ. KP) GO TO 59
KK=MIN(KK+1,KP)
GO TO 10
59

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13	KL=SQRT(((X(K)-XU(JJ+1))*(X(K)-XU(JJ+1))+(Y(K)-YU(JJ+1))*(Y(K)-YU(JJ+1)))	AVERHT	59
66	1YU(JJ+1))	AVERHT	60
	A=3.14159*XL*(Y(K)+YU(JJ+1))	AVERHT	61
	HGAT=HGAT+(HG(K+1))/2.0	AVERHT	62
	HGAT=HGAT+(HG(K+1))	AVERHT	63
	AL=AL+A	AVERHT	64
65	HGAT=HGAT/AT	AVERHT	65
	IF(PRINTS.EQ.0) GO TO 302	AVERHT	66
	WRITE(6,100) NODE(JJ,JJ),HGAT,AT	AVERHT	67
302	LU=LU+1	AVERHT	68
	MODEL(LU)=NODE(JJ,JJ)	AVERHT	69
	HILLU)=HGAT/ALAN.0	AVERHT	70
70	HGAT=D.3	AVERHT	71
	AT=D.0	AVERHT	72
	KL=SQRT((X(K+1)-XU(JJ+1))*(X(K+1)-XU(JJ+1))+(Y(K+1)-YU(JJ+1))*(Y(K+1)-YU(JJ+1)))	AVERHT	73
	1Y(K+1)-YU(JJ+1))	AVERHT	74
75	A=3.14159*KL*(Y(K+1)+YU(JJ+1))	AVERHT	75
	HGAT=HGAT+(HG(K+1))	AVERHT	76
	AT=AT+A	AVERHT	77
	M=1	AVERHT	78
	KX=HILLU*(K+1,KP)	AVERHT	79
80	GO TO 10	AVERHT	80
	IF(X(KP+1).LT.XU(JJ+1)) GO TO 40	AVERHT	81
	GO TO 12	AVERHT	82
40	M=1	AVERHT	83
	CALL STORE(HGAT,AT,JJ,0)	AVERHT	84
	IF(X.EQ.KP) GO TO 60	AVERHT	85
	CONTINUE	AVERHT	86
10	CONTINUE	AVERHT	87
59	AT=D.0	AVERHT	88
	HGAT=D.0	AVERHT	89
	CALL STORE(HGAT,AT,JJ,0)	AVERHT	90
50	RETURN	AVERHT	91
	END	AVERHT	92

```

SUBROUTINE HEAT(XI,XF,ITO,PTO,THET,MI,XI,XT,YT,XMT,TMT,CTHETA,CHIA,
1 XI,VT,MT,IK,J, ISTRM,JSURF,ICS,IPRNT2,II,CF11)
2
3 HEAT
4
5 DIMENSION CTHETA(11),CHIA(11)
6
7 DIMENSION XI(11),VT(11),MT(11),CF11(11)
8
9 DIMENSION XT(11),YT(11),XMT(11),TMT(11),ICSURF(11)
10
11 REAL MU,MUO,M1,MUO
12
13 MU=MI*XT(11)
14
15 IF(TNET) 50,51,53
16
17 DO 51 J=1,ICS
18
19 IF(JSURF-ICSURF(J)) 53,55,53
20
21 CONTINUE
22
23 THET=CTHETA(J)
24
25 MI=CHIA(J)
26
27 VMT=TNET/12.0
28
29 CHK=XF-XI
30
31 KKP=CHK
32
33 CHK1=KKP
34
35 IESCHK=159, CHK1) 60 TO 300
36
37 KP=KKP+2
38
39 GO TO 301
40
41 KP=KKP+1
42
43 KK=KP
44
45 DO 100 I=1,KK
46
47 XI=XI(11)/12.0
48
49 VT=VT(11)/12.0
50
51 XF=XF/12.0
52
53 DX=C.0633333333333333
54
55 L=1
56
57 XI=XT(11)-DX
58
59 KKK=0
60
61 KKKK=-1
62
63 GO=15M-1.1/2.
64
65 HO=CP*TTG
66
67 AO=41.4266*SORT(16M*TTG)
68
69 RHOO=2.7*PTO/ITO
70
71 MUO=(7.31E-07*ITO**1.51)/(ITO+198.6)
72
73 MUO=MUO/RHOO
74
75 SM1=XMT(11)*XMT(11)
76
77 H=MI*(1.0+CG*SM1)*CG*SM1
78
79 CALL TURBL(XI,VT,XMT,TMT,XI,XFIN,ITO,PTO,AG,MUO,CG,MG,GM,DX,
1 MI,CP,THET,MI,H,CTHETA,CHIA,XI,YT,MT,IPRNT2,II,IK,KK,
2 KKK,KL,ISTRM,JSURF,ICS,IKJ,CF11)
3
4 IF(KKK)200,201,201
5
6 IF(TNET=0.0001)
7
8 MI=1.3
9
10 MU=MI
11
12 GO TO 1000
13
14 DO 500 I=1,KK
15
16 XT(11)=XI(11)*12.0
17
18 RETURN
19
20 END

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SUBROUTINE TURBL(TX,VT,XMT,MT,MT,M, XF,TID,PTD,AD,MUO, MUO, TURBLT 2
1CG, NO, SM,DX,M,CP, TMT,M,M, TURBLT 1
2 CMTA,CHIA,XI,VI,MTI,PRINTZ,II,T,KK,KP,KKK, TURBLT 4
3 KKKK,L,ISIREK,JSURF,ISUPF,ICG,IK,CALLI TURBLT 5
4 DIMENSION CMTA(11),CHIA(1) TURBLT 6
5 DIMENSION XI(11),VI(11),MTI(11),CELL(11) TURBLT 7
6 DIMENSION XT(11),VT(11),XMT(11),MT(11),ISORF(11) TURBLT 8
7 REAL MUO,M1,LAM3D,MU1,MUO,M2,MUR,MU2 TURBLT 9
8 INTEGER PRINT TURBLT 10
9 FORMAT(///6X,"BOUNDARY LAYER FLAT PLATE SHAPE FACTOR ITERATION PA TURBLT 11
10 LLED TO CONVERGE,"//425X,"PROGRAM EXECUTION IS STOPPED,"//30X,"IS TURBLT 12
11 20300 LINE 702BLT") TURBLT 13
12 FORKAT(1),7X,114,9X,14V,7X,4MACH,7X,3DEL,10X,4MSKIN,13X,2MT,5 TURBLT 14
13 X,SMIN,1,5X,SMIN,1,6X,2MNO,7X,SMIN,1,7X,BHFRICION,4X,18H19U/5 TURBLT 15
14 2FT,4R,DEFT,1,7 TURBLT 16
15 FORMAT(11,1,22,1,16,"FLOW STREAM NO. 11,26M HEAT TRANSFER INFORMATI TURBLT 17
16 10N,43V,12,32FACE NO. 11,7) TURBLT 18
17 FORKAT(1,7),14X,3X,11MT,7X,4MACH,7X,3DEL,13X,4MSKIN,13X,2MT,5 TURBLT 19
18 X,SMIN,1,5X,SMIN,1,6X,2MNO,7X,SMIN,1,7X,BHFRICION,4X,18H19U/SOFT TURBLT 20
19 2HRS,DEFT,1,7) TURBLT 21
20 FORMAT(12,4X,16,3),4X,15,3,214V,19,61,10V,19,3/1) TURBLT 22
21 CEL=0,1 TURBLT 23
22 X2=X1 TURBLT 24
23 VZ=VT(11) TURBLT 25
24 IF(KKKK)5021,5021,5001 TURBLT 26
25 5001 KKKK=3 TURBLT 27
26 GO TO 5002 TURBLT 28
27 5021 IF(PRINTZ.EQ.1) GO TO 7001 TURBLT 29
28 WRITE(6,7) ISIREN,JSOF TURBLT 30
29 WRITE(5,10) TURBLT 31
30 IKJ=5 TURBLT 32
31 LINE=7 TURBLT 33
32 7001 TURBLT 34
33 5002 J=0 TURBLT 35
34 KKK=1 TURBLT 36
35 EI=IGM+1,1/12,*(GM-1,01) TURBLT 37
36 DO 25 I=L,MP TURBLT 38
37 121 M2=CJD TURBLT 39
38 123 DO 25 I=L,MP TURBLT 40
39 IM=M TURBLT 41
40 XI=XI+DX TURBLT 42
41 IF(XI-XF)131,50,50 TURBLT 43
42 XI=VF TURBLT 44
43 50 1=XI+1 TURBLT 45
44 CALL TABLE (XT,XMT,XI,M1,M1,DMDX,KK) TURBLT 46
45 CALL TABFL (XT,VT,XI,YI,DOYX,KK) TURBLT 47
46 IF(II.EQ.1) DTEX=-DYDX TURBLT 48
47 IF(KKKK)3001,3021,3001 TURBLT 49
48 3001 IF(IV-M1)3002,3002,3000 TURBLT 50
49 3002 L=1 TURBLT 51
50 XI=XI-DX TURBLT 52
51 KKKK=-1 TURBLT 53
52 GETC TURBLT 54
53 SMI=XI*M TURBLT 55
54 VLA=1,5*(V2+V1) TURBLT 56
55 IF (VLA) 131,132,133 TURBLT 57
56 132 VLA=L,6 TURBLT 58
57 133 TEL=IV/V1,0,CG*SM1) TURBLT 59
58 CALL ENCTL (TEL,PR) TURBLT 59

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IF(KKK)3006,3007,3007
3007 CALL HEATP(MT,CP,CF,PR,HI,M1,TTO,TEL,PTO,GM)
LINE=LINE+2
IF(LINE-60)3008,3009,3009
3009 WRITE(6,4000)
LINE=3
3008 XI=VI/12.0
VI=VI/12.0
DEL=DEL/12.0
WRITE(6,11) XI,VI,M1,DEL,CF,MT
IKJ=IKJ+1
XII(IKJ)=XI
VI(IKJ)=VI
MT(IKJ)=MT
CF(IKJ)=CF
XI=VI/12.0
VI=VI/12.0
DEL=DEL/12.0
GO TO 25
3006 XI=CP*TEL
NAME (1,CG*PP*,333* SM1)*HX1
CALL TABLEL (XT,MT,XI,TM1,DTMOX,KK)
IF(TT)14,14,15
14 HM1=HAM
TM1=HM1/CP
GO TO 16
15 HM1=CP*TM1
16 TER=0.5*TM1+.22*PR*,333*TTO+(0.5-.22*PR*,333)*TEL
TER=TER
LAMBDA=TTTO+198.8*SORT(TM1/TTTO)/(TM1+198.8)
MU=LAMBDA*TEL+MUO/TTO
MUR=LAMBDA*TER+MUO/TTO
W2=.5*(M1+M2)*AO/ MUO
W31=(TEL/TTTO)*EL
W41=MUR/ MUO+.268
M1=TTTO/TER)*W31
C1=SORT(TEL/TTTO)
AE=W1.4266*SORT(GM*TEL)
U1=W1*AE
CU1=(.5*(U1+U2))/(.5*(C1+C2))
IF (U-1) 101,19,19
101 J=1
IF (TMFT) 102,102,103
103 IF (DEL) 103,103,103
1035 THELM=THEL
STRUN=DIR
OO 1033 II=1.2
VPLF=DIR
OO 1031 III=1.50
VPLF=DIR-3.0-2.5/VPLF
IF (AGC(VPLF-VPLF)/VPLF)-.001 1032,1032,1031
1031 VPLF=VPLF
1032 NT=(2.5*VPLF)/VPLF
0-01*(1.0*TM1*(M1+1.))
THEL=DEL/O
DIR=OTPLM*THEL/THELM
1033 H=CG*SM1*HM1*HJ*(1.0+CG*SM1)/HO

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1812	KKKK=0	TURBLT	173
	THRL=THTR	TURBLT	174
	MIC=111.00	TURBLT	175
172	GO TO 252	TURBLT	176
1810	01=HIA*(HIA+1.0)*(HIA+1.0)*(HIA-1.0)	TURBLT	177
	Q2=1.0*(WE-1.0)*(HIA*(HIA+1.0)/(HIA+1.0))	TURBLT	178
	Q3=HIA*(HIA-1.0)*(HIA-1.0)*A1*TER/TTO/THTRA	TURBLT	179
180	Q4=(HIA*(HIA-1.0)*(HIA+1.0)*(TER/TTO)*(0.003075*(HIA-0.003352)/THTRA	TURBLT	180
	Q4=HIA*(HIA-1.0)	TURBLT	181
	Q5=0.5*(HIA+1.0)	TURBLT	182
	Q6=0.3*(HIA+1.0)	TURBLT	183
	MIC=HIA*(HIA+1.0)	TURBLT	184
185	IF (MIC) 245,245,246	TURBLT	185
	MIC=1.0	TURBLT	186
	GO TO 249	TURBLT	187
246	IF (IC-2.5) 1002,1002,248	TURBLT	188
1802	KKK=-1	TURBLT	189
248	GO TO 247	TURBLT	190
249	IF (K) 1000,247,247	TURBLT	191
1833	KKK=1	TURBLT	192
247	IF (A) 35((HIC-MI)/MI)-.005) 250,250,249	TURBLT	193
249	HI=HIC	TURBLT	194
	WRITE (6,5)	TURBLT	195
195	STOP	TURBLT	196
250	IF (A) 35((THRL-THTR)/THTR)-.005) 252,252,251	TURBLT	197
251	THRL=THTR	TURBLT	198
252	THTR=THTR/W31	TURBLT	199
	MI=HIC	TURBLT	200
200	CF=0.246*(TER/TERI)*H1/EXP(1.561*(H1)/((CUI*(THTR/NUO))*.8.268)	TURBLT	201
	AMSQA=.5*(M1+M2)	TURBLT	202
	H=CG*(AMSQA*(H1+1.0)*CG*(AMSQA)	TURBLT	203
	THTR=THTR	TURBLT	204
	DSTAR=H*THTR	TURBLT	205
205	AM=2.0/(H1-1.0)	TURBLT	206
	OTR=(2.0*(AM)*H1.0*(AM)/AM	TURBLT	207
	DEL=THTR*(OTS*CG*(AMSQA*(H1+1.0))	TURBLT	208
26	X2=Y1	TURBLT	209
	CALL HEATTR(HT,CP,CF,PR,HI,MI,TTOT,TE1,PTOT,GM)	TURBLT	210
210	Y2=Y1	TURBLT	211
	M2=M1	TURBLT	212
	TE2=TE1	TURBLT	213
	H2=H1	TURBLT	214
215	TER2=TER1	TURBLT	215
	THTR2=THTR	TURBLT	216
	MI2=MI	TURBLT	217
	A2=A1	TURBLT	218
	C2=C1	TURBLT	219
	U2=U1	TURBLT	220
220	CU2=CU1	TURBLT	221
	MU2=MU1	TURBLT	222
	M12=M11	TURBLT	223
	M4=M41	TURBLT	224
	IF (PRINT2.EQ. 0) GO TO 502	TURBLT	225
225	LINE=LINE+2	TURBLT	226
	IF (LINE-60) 501,502,501	TURBLT	227
	501 WRITE (6,5000)	TURBLT	228
	LINE=3	TURBLT	229

230	582	X1=X1/12.0	TURBLT	232
		V1=V1/12.0	TURBLT	231
		IF(P1=12.0, EQ, 1) GO TO 7801	TURBLT	232
		DEL=DEL/12.0	TURBLT	233
		WRITE(6,11) X1,V1,W1,DEL,CF,WT	TURBLT	234
		DEL=DEL/12.0	TURBLT	235
235	7001	KJ=1/KJ+1	TURBLT	235
		X111(KJ)=X1	TURBLT	237
		V111(KJ)=V1	TURBLT	238
		W111(KJ)=W1	TURBLT	239
		CF111(KJ)=CF	TURBLT	240
240		X1=X1/12.0	TURBLT	241
		V1=V1/12.0	TURBLT	242
		IF(L,GT, KP) GO TO 731	TURBLT	243
	25	CONTINUE	TURBLT	244
	731	KKK=-1	TURBLT	245
245		I=1	TURBLT	246
		IF(DOS) 703,703,705	TURBLT	247
	785	DO 701 JAA=1,ICS	TURBLT	249
		IF(DOS)-ICS=CF(JAA) 701,702,701	TURBLT	250
	702	CTHETA(JAA)=THET+12.0	TURBLT	251
250		CHIA(JAA)=HI	TURBLT	252
		GO TO 703	TURBLT	253
	701	CONTINUE	TURBLT	254
	703	RETURN	TURBLT	255
		END	TURBLT	255

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SUBROUTINE	WEATTR(HT,CP,CF,PR,MI,NI,ITO,TEL,PTO,GM)	WEATTR	2
REAL MI		WEATTR	3
GM1=ICM+1.0/(12.0*GM)-2.1		WEATTR	4
GM2=-GM/(CM-1.1)		WEATTR	5
TR=ITO/TEL		WEATTR	6
SOR1=MI*MI		WEATTR	7
EXP=1.561*(MI-(1.3*TR))-150MI/5.1)		WEATTR	8
PRND=PR*(1-5557)		WEATTR	9
WT=231428.972*CF*PTO*MI*CP*PRND*(TEL*GM1)+(ITO*GM2)*EXP(EXPP)		WEATTR	10
RETURN		WEATTR	11
END		WEATTR	12

		SUBROUTINE AVERFS(X,Y,CF,XU,YU,ICS,ICSURF,M,KP,JSURF,KSURF,NODE, 1NMN,XMN,P,GAM,IT,CPAT,FTI DIMENSION X(1),Y(1),CF(1),KU(1),YU(1),KSURF(1),NODE(5,20), 1ICSURF(1),XMN(1),P(1) COMMON/BB3/ NODE(500),FT(150),LUI K=1	AVERS	2
5		DO 71 J=1,NMN IF(KSURF(J)) .EQ. JSURF GO TO 71 CONTINUE IF(ICS .GT. 0) GO TO 200 M=J	AVERS	3
10	71	GO TO 72	AVERS	4
		DO 201 KU=1,ICS IF(ICSURF(KU)) .EQ. JSURF GO TO 202 CONTINUE M=J	AVERS	5
15	201	GO TO 72	AVERS	6
		CALL STGE1(CPAT,FTI,JU,1)	AVERS	7
20	72	M=1 DO 5 J=1,N IF(X(J)) .LT. XU(J) GO TO 7 CONTINUE J=J-1 DO 12 J=J,N IF(M .GT. 0) GO TO 514 CPAT=0.0 FFT=0.0 DEL=VU(J+1)-VU(J) IM=AIAN(IARSIDEL)/IXU(J+1)-XU(J+1) STM=JNIMTH CIN=COS(TH) IF(11 .EQ. 2) GO TO 500 IF(DEL-0.0) 501,502,503 COEL=+1.0 GO TO 2 COEL=0.0 GO TO 2 COEL=-1.0 GO TO 2 IF(DEL-0.0) 503,502,501 DO 12 K=K,KP IF(X(K+1) .GT. XU(J+1)) GO TO 33 X1=5*PT((X(K)-X(K+1))/(X(K)-X(K+1)))+(Y(N)-Y(K+1))*(Y(K)-Y(K+1)) 11)	AVERS	8
25	501	A=3.14159*X1*(Y(K)+Y(K+1)) CPAT=(CPAT)+CF(X(K+1))/2.0 PAV=(P(K)+P(K+1))/2.0 XNAV=(XMN(K)+XMN(K+1))/2.0 FPAV=(CPAT)+(PAV*A) FFI=FFT+(PAV*A*CPAT*XNAV*XNAV*GAM/2.0) DIFF=ABS(X(K+1)-XU(J+1)) IF(DIFF .LT. 0.01) GO TO 56 GO TO 11 FOATAV=FOAT*CTH FPAV=FFI*CTH FPAV=FPATAV*COEL FT=FTAV*FPAV	AVERS	9
30	502		AVERS	10
35	503		AVERS	11
40	500		AVERS	12
45	2		AVERS	13
50			AVERS	14
55			AVERS	15
60			AVERS	16
65			AVERS	17
70			AVERS	18
75			AVERS	19
80			AVERS	20
85			AVERS	21
90			AVERS	22
95			AVERS	23
100			AVERS	24
105			AVERS	25
110			AVERS	26
115			AVERS	27
120			AVERS	28
125			AVERS	29
130			AVERS	30
135			AVERS	31
140			AVERS	32
145			AVERS	33
150			AVERS	34
155			AVERS	35
160			AVERS	36
165			AVERS	37
170			AVERS	38
175			AVERS	39
180			AVERS	40
185			AVERS	41
190			AVERS	42
195			AVERS	43
200			AVERS	44
205			AVERS	45
210			AVERS	46
215			AVERS	47
220			AVERS	48
225			AVERS	49
230			AVERS	50
235			AVERS	51
240			AVERS	52
245			AVERS	53
250			AVERS	54
255			AVERS	55
260			AVERS	56
265			AVERS	57
270			AVERS	58
275			AVERS	59

68	LUI=LUI+1 JN=MODE(JJJ,JJ) MODE15(JN)=JN FT1(JN)=FT M=0 IFIK .EQ. KPI GO TO 59 KK=HING(KK+1,KPI) GO TO 10	59 AVERFS 60 AVERFS 61 AVERFS 62 AVERFS 63 AVERFS 64 AVERFS 65 AVERFS 66 AVERFS 67 AVERFS 68 AVERFS 69 AVERFS 70 AVERFS 71 AVERFS 72 AVERFS 73 AVERFS 74 AVERFS 75 AVERFS 76 AVERFS 77 AVERFS 78 AVERFS 79 AVERFS 80 AVERFS 81 AVERFS 82 AVERFS 83 AVERFS 84 AVERFS 85 AVERFS 86 AVERFS 87 AVERFS 88 AVERFS 89 AVERFS 90 AVERFS 91 AVERFS 92 AVERFS 93 AVERFS 94 AVERFS 95 AVERFS 96 AVERFS 97 AVERFS 98 AVERFS 99 AVERFS 100 AVERFS 101 AVERFS 102 AVERFS 103 AVERFS 104 AVERFS
65	13 XL=SQRT((X(K)-XU(JJ+1)) ² +Y(K)-YU(JJ+1)) ² *(Y(K)-YU(JJ+1)) ² +Y(K)-YU(JJ+1)) ² YU(JJ+1)) ² A=J.14159*XL*(Y(K)+YU(JJ+1)) CPAV=(CP(K)+CF(K+1))/2.0 PAV=(P(K)+P(K+1))/2.0 XNAV=(X(N(K)+XN(K-1))/2.0 FPAT=FPAT+(PAV*1) FFT=FFT+(PAV*A*CFAY*XNAV*GAM/2.0) FPATAY=FPAT+STM M=FFT*CTN FPATAY=FPATAY*COEL FT=FTAY*FPATAY LUI=LUI+1 JN=MODE(JJJ,JJ) MODE15(JN)=JN FT1(JN)=FT FPAT=0.0 FFT=0.0	
70	XL=SQRT((X(K+1)-XU(JJ+1)) ² +Y(K+1)-YU(JJ+1)) ² *(Y(K+1)-YU(JJ+1)) ² +Y(K+1)-YU(JJ+1)) ² YU(JJ+1)) ² A=J.14159*XL*(Y(K+1)+YU(JJ+1)) CPAT=CPAT+(PAV*A) FFT=FFT+(PAV*A*CFAY*XNAV*GAM/2.0) M=1 KK=HING(KK+1,KPI) GO TO 10 IFIK(KPI) .LT. XU(JJ+1) GO TO 48 GO TO 12	
85	CALL STORE1(FPAT,FFT,JJJ,3) IFIK .EQ. KPI GO TO 60 CONTINUE CONTINUE FPAT=0.0 FFT=0.0 CALL STORE1(FPAT,FFT,JJJ,0) RETURN END	
90	11 48 12 18 59 60	

68	1188	CALL PICMIN(YDUCT,LOUHHY,MVERD,YMINO)	VIENS	59
		IF (YU(1)-YU(2)) 1188,1188,1185	VIENS	60
		YMIN= YU(1)	VIENS	61
		GO TO 1189	VIENS	62
	1189	YMIN= YU(2)	VIENS	63
	1189	IF (YU(1)-YU(2)) 1115,1115,1172	VIENS	64
	1115	YMIN= YU(2)	VIENS	65
		GO TO 1125	VIENS	66
65		YMIN= YU(1)	VIENS	67
	1128	CALL TEST2(YMIN,YMAX,YMINO,IF)	VIENS	68
	1125	IF (IFY-1) 1130,1130,1135	VIENS	69
	1135	CALL TEST2(YMIN,YMAX,YMAXO,IF)	VIENS	70
		IF (IFY-1) 1130,1130,1135	VIENS	71
70		CALL TEST2(YMINO,YMAXO,YMINO,IF)	VIENS	72
	1145	IF (IFY-1) 1130,1130,1150	VIENS	73
	1150	SMAO=2.0	VIENS	74
		GO TO 15	VIENS	75
75	1130	SMAO=1.0	VIENS	76
		PHIL= 2.0*PIE/DUCT	VIENS	77
		OPHIL = PHIL/COIV	VIENS	78
		PHIL = (2.5-5*CK1)*OPHIL	VIENS	79
		ANGDUC(1) = PHIL	VIENS	80
80		DOUC= DOUC-1	VIENS	81
		DC 1155 JON=11DOUC	VIENS	82
		FJON = JON	VIENS	83
1155		ANGDUC(JON+1) = 2.0*PIE*(FJON+1.0)/DOUC	VIENS	84
15		J=1	VIENS	85
85		A(J) = PIE*(RU(J) + RD(J))*SORT((RD(J)-RU(J))**2 + (YD(J) -	VIENS	86
		YU(J))**2)	VIENS	87
		B1 = (YD(J)-YU(J))/SORT((YD(J)-YU(J))**2 + (RD(J)-RU(J))**2)	VIENS	88
		A1 = -(RD(J)-RU(J))/SORT((YD(J)-YU(J))**2 + (RD(J)-RU(J))**2)	VIENS	89
		IF (VECT(J) 1 20,30,30	VIENS	90
90	20	B1 = -B1	VIENS	91
		A1 = -A1	VIENS	92
30		IF (YD(J) - YU(J)) 32,34,32	VIENS	93
34		DR1 = (RD(J) - RU(J))/DIV(J)	VIENS	94
		GO TO 36	VIENS	95
32		E1 = (RU(J)*YD(J)-RD(J)*YU(J))/(YD(J)-YU(J))	VIENS	96
95		H1 = (RD(J)-RU(J))/(YD(J)-YU(J))	VIENS	97
		DY1 = (YD(J)-YU(J))/DIV(J)	VIENS	98
36		NYD1 = DIV(J)	VIENS	99
		NYL = DIV(J)	VIENS	100
361		K=2	VIENS	101
		A(K) = PIE*(RU(K)+RD(K))*SORT((RD(K)-RU(K))**2 + (YD(K)-	VIENS	102
1		YU(K))**2)	VIENS	103
		B2 = (YD(K)-YU(K))/SORT((YD(K)-YU(K))**2 + (RD(K)-RU(K))**2)	VIENS	104
		A2 = -(RD(K)-RU(K))/SORT((YD(K)-YU(K))**2 + (RD(K)-RU(K))**2)	VIENS	105
105		IF (VECT(K) 1 50,50,50	VIENS	106
80	82	-82	VIENS	107
	A2	-A2	VIENS	108
		IF (YD(K) - YU(K)) 52,54,52	VIENS	109
94		DR2 = (RD(K) - RU(K))/DIV(K)	VIENS	110
		GO TO 56	VIENS	111
52		F2 = (YU(K)*YD(K)-RU(K)*YU(K))/(YD(K)-YU(K))	VIENS	112
		F2 = (RD(K)-RU(K))/(YD(K)-YU(K))	VIENS	113
		DY2 = (YD(K) - YU(K))/DIV(K)	VIENS	114
56		FF=3.0	VIENS	115

115		NVD2 = DIV(K)			VIEW5	116
		LV = 1			VIEW5	117
		LP = 1			VIEW5	118
120	77	SPI = SIN(PHIL)			VIEW5	119
		CPI = COS(PHIL)			VIEW5	120
		DO F03 L=1,NY01			VIEW5	121
		PL = L			VIEW5	122
125	88	IF(B1) 01,02,00			VIEW5	123
		VJ = VU(J) + (PL-1)*DY1			VIEW5	124
		V1 = OV1*(.5-.5*CK1)+VJ			VIEW5	125
		R1 = E1 + Y1*H1			VIEW5	126
		GO TO 87			VIEW5	127
		RJ = RU(J) + (PL-1)*DR1			VIEW5	128
		R1 = RJ+DR1*(.5-.5*CK1)			VIEW5	129
		V1 = VU(J)			VIEW5	130
130	87	X1 = R1+CPI			VIEW5	131
		Z1 = R1*SPI			VIEW5	132
		CAL = B1*SPI			VIEW5	133
		CBI = A1			VIEW5	134
135		CG1 = B1*SPI			VIEW5	135
		R=0.0			VIEW5	136
		M=1			VIEW5	137
		DO 50C M=1,NY02			VIEW5	138
		P1 = M			VIEW5	139
		IF(B2) 08,09,06			VIEW5	140
		VK = YU(K)+(PM-1)*DY2			VIEW5	141
		V2 = YK+DY2*(.5-.5*CK1)			VIEW5	142
		R2 = E2 + F2*V2			VIEW5	143
		GO TO 405			VIEW5	144
		RK = RU(K)+(PM-1)*DR2			VIEW5	145
		R2 = RK+DR2*(.5-.5*CK1)			VIEW5	146
		V2 = YU(K)			VIEW5	147
		IF(B2*R1) 66,65,66			VIEW5	148
		IF(1 B2*R2 + (V2-Y1)*A2) 6605,6610,6605			VIEW5	149
		CP2PI = P2/3.14 + A2*(V2-Y1)/(B2*R1)			VIEW5	150
		CAL = ARCCOS(CP2PI,AP201,ITAI)			VIEW5	151
		IF(ITAI-1170,70,6605			VIEW5	152
		6605 X2=R2+COS(PHIL+PIE/3.1)			VIEW5	153
		Z2=R2*SIN(PHIL+PIE/3.1)			VIEW5	154
		RH02 = (R2-X1)*2+(V2-Y1)*2+(Z2-Z1)*2			VIEW5	155
		IF(RH021,6610,6610,6615			VIEW5	156
		6610 GT=0.0			VIEW5	157
		GO TO 409			VIEW5	158
		6615 RH0=SQRT(RH02)			VIEW5	159
		CST = (B2*R1)*.5-.5-R2*R2+A2*(V1-Y2)/RH0			VIEW5	160
		IF(CST) 6610,6610,6620			VIEW5	161
		6620			VIEW5	162
		IND1 = 1			VIEW5	163
		GO TO 7001			VIEW5	164
		70 IF (-R2*SIN(AP2PI)) 601,603,602			VIEW5	165
		603 CST = R2*F1+COS(AP2PI + 0.174) -B2*R2 + A2*(V1-Y2)			VIEW5	166
		IF(CST) 6610,6610,6620			VIEW5	167
		661			VIEW5	168
		IND1 = 1			VIEW5	169
		GO TO 7001			VIEW5	170
		IND1 = 2			VIEW5	171
		IF(B1*R2) 72,7010,72			VIEW5	172
		IF((V2-Y1)*A1 -R1*B1) 7030,7040,7030			VIEW5	173
		7010			VIEW5	174
		7010			VIEW5	175
		7010			VIEW5	176
		7010			VIEW5	177
		7010			VIEW5	178
		7010			VIEW5	179
		7010			VIEW5	180
		7010			VIEW5	181
		7010			VIEW5	182
		7010			VIEW5	183
		7010			VIEW5	184
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		7010			VIEW5	190
		7010			VIEW5	191
		7010			VIEW5	192
		7010			VIEW5	193
		7010			VIEW5	194
		7010			VIEW5	195
		7010			VIEW5	196
		7010			VIEW5	197
		7010			VIEW5	198
		7010			VIEW5	199
		7010			VIEW5	200

173	72	DP2P1 = R1/R2 - A1*(Y2-Y1)/(R1*R2) CALL APCOS(DP2P1, BP2P1, ITA1) IF (ITA1 - 1) 90, 90, 7030	VIEM3	173
174	730	R2=R2-COS(PH11+PIE/3.) Z2=R2*SIN(PH11+PIE/3.) RHO2 = (Z2-X1)*2+(Y2-Y1)*2+(Z2-Z1)*2 IF (RHO2) 7045, 7045, 7050	VIEM3	174
175			VIEM3	175
176			VIEM3	176
177			VIEM3	177
178			VIEM3	178
179			VIEM3	179
180			VIEM3	180
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223			VIEM3	223
224			VIEM3	224
225			VIEM3	225
226			VIEM3	226
227			VIEM3	227
228			VIEM3	228
229			VIEM3	229

	KIL= NP(II)-1	VIEWS	287
	GO TO 1308	VIEWS	288
1288	IF(V1-Y2) 1310,1318,1315	VIEWS	289
1318	KI=NY1	VIEWS	290
298	KIL = NY2	VIEWS	291
	GO TO 1302	VIEWS	292
1315	KI= NY2	VIEWS	293
	KIL= NY1	VIEWS	294
1295	GO TO 1308	VIEWS	295
	KI= NY2	VIEWS	296
1318	KIL= NP(II)-1	VIEWS	297
	CALL CAUSEE(Y1,R1,Y2,R2,YF,RF,KI,KIL,IJ,ISEE)	VIEWS	298
	GO TO (1295,1399,1699,7138,1399), ISEE	VIEWS	299
1399	LUM= C	VIEWS	300
300	DO 1460 LOLA= KI-KIL	VIEWS	301
	IF(V1-Y2) 1428,1420,1418	VIEWS	302
1418	KILE=KIL-(LOLA-KI)	VIEWS	303
	KILEP = KILE+1	VIEWS	304
305	RFU=RF(JJ,KILE)	VIEWS	305
	RFD = RF(JJ,KI-EP)	VIEWS	306
	YFU= YF(JJ,KILE)	VIEWS	307
	YFO= YF(JJ,KI-EP)	VIEWS	308
	GO TO 1540	VIEWS	309
1428	RFU=RF(JJ,LOLA)	VIEWS	310
318	RFD= RF(JJ,LOLA+1)	VIEWS	311
	YFU= YF(JJ,LOLA)	VIEWS	312
	YFO= YF(JJ,LOLA+1)	VIEWS	313
	IF(LOLA-KI) 1430,1430,1440	VIEWS	314
1430	IF(V1-YFO) 1450,1450,1460	VIEWS	315
1450	CALL PING(Y1,R1,Y2,R2,YFU,RFU,ANG,LOIS)	VIEWS	316
	IF(LOIS-3) 1450,1455,1470	VIEWS	317
1470	LUM= LUM+1	VIEWS	318
	PHEQ(LUM)= ANG	VIEWS	319
	GO TO 1460	VIEWS	320
1465	WRITE(6,1467)	VIEWS	321
1467	FORMAT(1M1,/,/,/,9X,"THE ANGLE FOR THE LIMIT OF INTEGRATION IS UND	VIEWS	322
	DEFINED.,/,25X,"THE COSINE IS GREATER THAN 1.",/,25X,"PROGRAM EXEC	VIEWS	323
	UTION IS STOPPED.",/,30X,="(SUBROUTINE RING)")	VIEWS	324
	STOP	VIEWS	325
325	IF(LOLA-KIL) 1450,1450,1460	VIEWS	326
1460	IF(V2-YFO) 1450,1450,1452	VIEWS	327
1452	CALL PING(Y1,R1,Y2,R2,YFO,RFU,ANG,LOIS)	VIEWS	328
1495	GO TO(1430,1430,1495,1500),LOIS	VIEWS	329
	WRITE(6,1467)	VIEWS	330
330	STOP	VIEWS	331
1500	LUM=LUM+1	VIEWS	332
	PHEQ(LUM)= ANG	VIEWS	333
1492	CALL 90DY(Y1,Y2,R1,R2,YFU,RFU,PHEQ,PHI,I,ION)	VIEWS	334
1525	IF(ION-2) 1450,1510,1460	VIEWS	335
1510	LUM=LUM+1	VIEWS	336
	PHEQ(LUM)= PHI	VIEWS	337
	GO TO 1400	VIEWS	338
1480	IF(V2-YFO) 1515,1515,1520	VIEWS	339
1520	CALL PING(Y1,R1,Y2,R2,YFU,RFU,ANG,LOIS)	VIEWS	340
	GU TO(1515,1400,1495,1530),LOIS	VIEWS	341
1530	LUM=LUM+1	VIEWS	342
	PHEQ(LUM)= ANG	VIEWS	343

1515	CALL BODY(V1,V2,R1,R2,YFU,RFU,YFD,RFD,PHIO,PHIL,ION)	VIEW#	344
	GO TO 1525	VIEW#	345
345	IF(LOLA-KI) 1550,1550,1545	VIEW#	345
1550	IF(V1-YFU) 1560,1560,1555	VIEW#	347
1555	CALL SING(V1,R1,Y2,R2,YFU,RFD,ANG,LOIS)	VIEW#	343
	IF(LOIS-3) 1560,1565,1565	VIEW#	349
358	LUM=LUM+1	VIEW#	350
1565	PHIO(LUM)=ANG	VIEW#	351
1560	IF(V2-YFU) 1562,1560,1560	VIEW#	352
1562	CALL SING(V1,R1,Y2,R2,YFU,RFD,ANG,LOIS)	VIEW#	351
	GO TO(1560,1400,1495,1570),LOIS	VIEW#	354
1572	LUM=LUM+1	VIEW#	355
355	PHIO(LUM)=ANG	VIEW#	356
1562	CALL BODY(V1,V2,R1,R2,YFU,RFU,YFD,RFD,PHIO,PHIL,ION)	VIEW#	357
	GO TO 1525	VIEW#	358
1545	IF(LOLA-KI) 1562,1565,1565	VIEW#	359
1545	IF(V2-YFU) 1590,1595,1595	VIEW#	360
1532	CALL SING(V1,R1,Y2,R2,YFU,RFD,ANG,LOIS)	VIEW#	361
	GO TO(1535,1400,1495,1600),LOIS	VIEW#	362
1535	LUM=LUM+1	VIEW#	363
1535	PHIO(LUM)=ANG	VIEW#	364
365	CALL BODY(V1,V2,R1,R2,YFU,RFU,YFD,RFD,PHIO,PHIL,ION)	VIEW#	365
	GO TO 1525	VIEW#	366
1593	CONTINUE	VIEW#	367
A-168	IF(LUM-1) 1295,1601,1601	VIEW#	368
1601	IF(SEE-5) 1623,1602,1602	VIEW#	369
1602	CALL PICMIN(PHIO,LUKE,LUW,PHIL)	VIEW#	370
372	PHIO(LUKE)=PHIL	VIEW#	371
	LUKE=LUKE-1	VIEW#	372
	CALL PICMIN(PHIO,LUKE,LUW,PHIL)	VIEW#	373
375	PHIO(LUKE)=PHIL	VIEW#	374
1603	GO TO 1295	VIEW#	375
	CALL PICMIN(PHIO,LUKE,LUW,PHIL)	VIEW#	376
	PHIL(LUKE)=PHIL	VIEW#	377
	GO TO 1295	VIEW#	378
1699	LUM=LUM+1	VIEW#	379
380	DO 1700 NELL=KI,KIL	VIEW#	380
	IF(V1-Y2) 1720,1720,1710	VIEW#	381
1710	NELL=KIL-NELL-KI	VIEW#	382
	NELL=NELL+1	VIEW#	383
385	RFU=RFU+MILE	VIEW#	384
	RFD=RFU+MILE	VIEW#	385
	YFU=YFU+MILE	VIEW#	386
	YFD=YFU+MILE	VIEW#	387
	GO TO 1690	VIEW#	388
1720	RFU=RFU+MILE	VIEW#	389
	RFD=RFU+MILE	VIEW#	390
	YFU=YFU+MILE	VIEW#	391
390	YFD=YFU+MILE	VIEW#	392
	IF(NELL-KI) 1730,1730,1760	VIEW#	393
1730	IF(V1-YFU) 1750,1760,1760	VIEW#	394
1750	CALL SING(V1,R1,Y2,R2,YFU,RFD,ANG,LOIS)	VIEW#	395
	IF(LOIS-3) 1700,1765,1770	VIEW#	396
1770	LUM=LUM+1	VIEW#	397
	PHIO(LUM)=ANG	VIEW#	398
	GO TO 1760	VIEW#	399
1765	WRITE(6,14,17)	VIEW#	401

600	STOP	IF(Y2-YFD) 1700,1700,1762	VIEW\$	401
1700		CALL BING(Y1,X1,Y2,R2,YFD,ANG,ANG,LOIS)	VIEW\$	402
1702		GO TO(1780,1760,1795,1880,LOIS	VIEW\$	403
1705	WRITE(6,1667)		VIEW\$	404
STOP			VIEW\$	405
605	STOP		VIEW\$	406
1800	LIM=LIM+1		VIEW\$	407
	PHIS(LIM) = ANG		VIEW\$	408
	GO TO 1731		VIEW\$	409
1800	IF(NEILL-K1) 1850,1850,1860		VIEW\$	410
1850	IF(Y1-YFD) 1860,1860,1855		VIEW\$	411
1855	CALL RING(Y1,X1,Y2,R2,YFD,ANG,ANG,LOIS)		VIEW\$	412
	IF(LOIS-J) 1800,1765,1865		VIEW\$	413
1865	LIM=LIM+1		VIEW\$	414
	PHIS(LIM) = ANG		VIEW\$	415
1869	IF(Y2-YFD) 1862,1700,1700		VIEW\$	416
1862	CALL RING(Y1,X1,Y2,R2,YFD,ANG,ANG,LOIS)		VIEW\$	417
	GO TO(1700,1720,1795,1870,LOIS		VIEW\$	418
1870	LIM=LIM+1		VIEW\$	419
	PHIS(LIM) = ANG		VIEW\$	420
1780	CONTINUE		VIEW\$	421
	IF(LIM-1) 1295,1875,1875		VIEW\$	422
1875	CALL PICMAX(PHIS,LARRY,LIM,PHI6)		VIEW\$	423
	PHAM(LARRY) = PHI6		VIEW\$	424
1295	CONTINUE		VIEW\$	425
	IF(LUKF-1) 2100,2110,2110		VIEW\$	426
2110	CALL PICMIN(PHIM,LUKE,LUKE,PHIOUT)		VIEW\$	427
	IF(LAPRY-1) 2120,2130,2130		VIEW\$	428
2120	PHISL=8.0		VIEW\$	429
	PHISU=PHIOUT		VIEW\$	430
430	GO TO 2140		VIEW\$	431
2130	CALL PICMAX(PHAM,LARRY,LARRY,PHIIM)		VIEW\$	432
	IF(PHIOUT-PHIIM) 7130,7130,2150		VIEW\$	433
2150	PHISL=PHIIM		VIEW\$	434
	PHISU=PHIOUT		VIEW\$	435
635	GO TO 2140		VIEW\$	436
2100	IF(LAFRY-1) 2225,2160,2160		VIEW\$	437
2100	CALL PICMAX(PHAM,LARRY,LARRY,PHIIM)		VIEW\$	438
	PHISL=PHIIM		VIEW\$	439
2160	PHISU=PIE		VIEW\$	440
2160	IF(PHIU-PHISL) 7130,7130,2100		VIEW\$	441
2100	IF(PHISU-PHIL) 7130,7130,2100		VIEW\$	442
2100	IF(PHISL-PHIL) 2210,2210,2200		VIEW\$	443
2200	PHIL=PHISL		VIEW\$	444
2210	IF(PHISU-PHIU) 2220,2225,2225		VIEW\$	445
2220	PHIU=PHISU		VIEW\$	446
2225	IF(SHAD) 2230,2230,2240		VIEW\$	447
2240	PHON=1		VIEW\$	448
2270	JACVL= NVEPD-1		VIEW\$	449
	DOUCANG= ANGDOC(JON)		VIEW\$	450
650	LOUC= 8		VIEW\$	451
	DO 2600 JACX=1,JACKL		VIEW\$	452
	Y501= YDUCT(JACK)		VIEW\$	453
	Y102= YDUCT(JACK+1)		VIEW\$	454
	ROU1= PDUCT(JACK)		VIEW\$	455
	ROU2= PDUCT(JACK+1)		VIEW\$	456
655	IF(1-1) 1,1 IF(PHOUTUI)=1		VIEW\$	457

Line	Code	Text	Address	View
458	IF FIRENE-11	2610,2610,2600	VIEW3	458
459	LDUC= LDUC+1		VIEW3	459
460	PHCU(LDUC) = PHIX		VIEW3	460
461	CONTINUE		VIEW3	461
462	YDU2= YDUCT(INVERP)		VIEW3	462
463	YDU2= YDUCT(11)		VIEW3	463
464	RDUI= RDUCT(INVERP)		VIEW3	464
465	RDUI= RDUCT(11)		VIEW3	465
466	IF FIRENE, EO, 11	1CFYD(11)=1	VIEW3	466
467	IF FIRENE-11	2620,2620,2630	VIEW3	467
468	LDUC= LDUC+1		VIEW3	468
469	PHCU(LDUC) = PHIX		VIEW3	469
470	IF LDUC-11	2640,2650,2650	VIEW3	470
471	CALL PICMAX(PHOU,LUCK,LDUC,PHI7)		VIEW3	471
472	PHCU(LUCK) = PHI7		VIEW3	472
473	LUCK=LUCK-1		VIEW3	473
474	CALL PICMIN(PHOU,LUCK,LDUC,PHI7)		VIEW3	474
475	PHCU(LUCK) = PHI7		VIEW3	475
476	IF PHCU(LUCK) = PHUI		VIEW3	476
477	IF PHCU(LUCK) = PHUI	2640,2650,2650	VIEW3	477
478	IF JON=JON+1	2660,2660,2660	VIEW3	478
479	IF JON=JON+1		VIEW3	479
480	IF LDUC-11	2250,2260,2260	VIEW3	480
481	ICINE=1		VIEW3	481
482	PHCU(11) = PHIL		VIEW3	482
483	PHCU(11) = PHUI		VIEW3	483
484	GO TO 2270		VIEW3	484
485	LUCK= LUCK-1		VIEW3	485
486	DO 2290 IPH=1,LUCK		VIEW3	486
487	IPH=1		VIEW3	487
488	DO 2290 JPH= IPH,LUCK		VIEW3	488
489	IF PHCU(IPH)=PHCU(JPH)	2290,2290,2300	VIEW3	489
490	TEMP= PHCU(IPH)		VIEW3	490
491	PHCU(IPH) = PHCU(JPH)		VIEW3	491
492	PHCU(JPH) = TEMP		VIEW3	492
493	TEMP= PHCU(IPH)		VIEW3	493
494	PHCU(IPH)= PHCU(JPH)		VIEW3	494
495	PHCU(JPH) = TEMP		VIEW3	495
496	CONTINUE		VIEW3	496
497	LOCK= 1		VIEW3	497
498	PHMA(LOCK) = PHCU(11)		VIEW3	498
499	PHMA(LOCK) = PHCU(11)		VIEW3	499
500	JG= 2		VIEW3	500
501	IF JG=LUCK	2320,2320,2330	VIEW3	501
502	CALL TEST2(PHMA(LOCK),PHMA(LOCK),PHCU(JG),IFP)		VIEW3	502
503	IF IFP-11	2340,2340,2350	VIEW3	503
504	CALL TEST2(PHMA(LOCK),PHMA(LOCK),PHCU(JG),IFP)		VIEW3	504
505	IF IFP-11	2360,2360,2360	VIEW3	505
506	PHMA(LOCK) = PHCU(JG)		VIEW3	506
507	JG=JG+1		VIEW3	507
508	GO TO 2370		VIEW3	508
509	LOCK=LOCK+1		VIEW3	509
510	PHMA(LOCK) = PHCU(JG)		VIEW3	510
511	PHMA(LOCK) = PHCU(JG)		VIEW3	511
512	GO TO 2360		VIEW3	512
513	ICINE=0		VIEW3	513
514	J1=1		VIEW3	514

515	2398	PHILL(1)=PHIL	VIEW\$	515
	2400	IF (JI-LOCK) 2410,2410,2400	VIEW\$	516
		PHIU(1)= PHIU	VIEW\$	517
		ICIN=1	VIEW\$	518
		GO TO 2270	VIEW\$	519
520	2410	IF (PHIMA(JI)-PHIL) 2440,2440,2430	VIEW\$	520
	2440	IF (PHAMA(JI)-PHIL) 2460,2450,2450	VIEW\$	521
	2450	IF (PHAMA(JI)-PHIU) 2460,2450,2450	VIEW\$	522
	2460	JI=JI+1	VIEW\$	523
		GO TO 2390	VIEW\$	524
525	2430	IF (PHIMA(JI)-PHIU) 2432,2431,2431	VIEW\$	525
	2431	PHIU(1)= PHIU	VIEW\$	526
		ICIN=1	VIEW\$	527
		GO TO 2470	VIEW\$	528
	2432	PHIU(1)= PHIMA(JI)	VIEW\$	529
		ICIN= 1	VIEW\$	530
530	2470	IF (PHAMA(JI)-PHIU) 2480,2270,2270	VIEW\$	531
	2480	ICIN= ICIN+1	VIEW\$	532
		PHILL(1)= PHAMA(JI)	VIEW\$	533
		IF (JI-LOCK) 2490,2500,2500	VIEW\$	534
535	2490	JI= JI+1	VIEW\$	535
	2510	IF (PHIU-PHIMA(JI)) 2500,2500,2510	VIEW\$	536
		PHIU(1)= PHIMA(JI)	VIEW\$	537
		GO TO 2470	VIEW\$	538
	2500	PHIU(1)= PHIU	VIEW\$	539
540	2270	C = R2+2 + R1+2 + (V2-Y1)+2	VIEW\$	540
		O = 2. *R2+21	VIEW\$	541
		CMD = C - O	VIEW\$	542
		SPEC=0.0	VIEW\$	543
		IF (CMD-1.0E-5) 7670,7070,99	VIEW\$	544
545	7070	IF (R1) 7130,7130,7090	VIEW\$	545
	7090	SPEC=1.0	VIEW\$	546
		GI=0.0	VIEW\$	547
		GO TO 7145	VIEW\$	548
	99	CPD=C+O	VIEW\$	549
550	7130	IF (CPD) 7130,7130,7140	VIEW\$	550
		GO TO 409	VIEW\$	551
	7140	O1=CPD/CMD	VIEW\$	552
		Q2 = CMD/CPD	VIEW\$	553
		Q1 = SORT(Q1)	VIEW\$	554
		Q2 = SORT(Q2)	VIEW\$	555
555		Q3 = 2. *C/(CPD + CMD+2)	VIEW\$	556
		Q4 = 2. * O/(CPD + CMD+2)	VIEW\$	557
		E120=0.0	VIEW\$	558
560	7145	GO 150 JA=1,ICIN	VIEW\$	559
		PHIU = PHIU(JA)	VIEW\$	560
		PHIL = PHILL(JA)	VIEW\$	561
		IF (SPEC) 7150,7150,7160	VIEW\$	562
	7150	IF (PHIU -PIE) 100,110,110	VIEW\$	563
	100	SU2 = SIN(PHIU/2.0)	VIEW\$	564
565		CU2 = COS(PHIU/2.0)	VIEW\$	565
		TU2 = SU2/CU2	VIEW\$	566
		ATU2 = SU1 *TU2	VIEW\$	567
		AU = ATAN(ATU2)	VIEW\$	568
		OSU = TU2/11.+ O1*TU2*TU2)	VIEW\$	569
570		GO TO 170	VIEW\$	570

110	AU = PI/2.	VIEW5	572
120	QSU=0.9	VIEW5	573
130	IF(PHIL) 135,135,138	VIEW5	574
575	SL2 = SIN(PHIL/2.)	VIEW5	575
	CL2 = COS(PHIL/2.)	VIEW5	576
	IL2 = SL2/CL2	VIEW5	577
	AL = 501*IL2	VIEW5	578
	AL = ATAN(AL/2)	VIEW5	579
	OSL = TL2/IL1 + 01*TL2*IL2	VIEW5	580
580	GO TO 140	VIEW5	581
135	AL=0.0	VIEW5	582
140	OSL=0.0	VIEW5	583
	EL1 = 502*03*(AU - AL) + 04*(05U-QSL)	VIEW5	584
	EL2 = 502*04*(AU - AL) + 01*(05U-QSL)	VIEW5	585
585	EL4 = 1.70*21*(PHIU - PHIL) + (03*(2.0*0 - C*CI/D*21)*522*(AU -	VIEW5	586
	1 AL) + (03*CI/D)*(05U-QSL)	VIEW5	587
	CI1 = 91*22*CI*2	VIEW5	588
	CI2 = 92*41*31*(Y2-Y1) - 81*82*31*81 - 81*82*32*32 - 81*42*82*(Y2-Y1)	VIEW5	589
	CI3 = 81*82*81*82 - 82*41*82*(Y2-Y1) - 81*42*81*(Y2-Y1) - 81*42*(Y2-Y1)	VIEW5	590
590	1	VIEW5	591
	EL2 = CI1*EL1 + CI2*EL2 + CI3*EL1 + EL20	VIEW5	592
	GO TO 150	VIEW5	593
7160	CI=CI+AB8(B1)*(PHIU-PHIL)/12.*PIE*RI	VIEW5	594
151	CONTINUE	VIEW5	595
595	IF(SECCL) 293,293,409	VIEW5	596
299	IF(92) 313,313,310	VIEW5	597
300	CI = 2.*92*EI20/PIE	VIEW5	598
	GO TO 409	VIEW5	599
310	CI=2.*92*EI20/PIE+AB5(B2)11	VIEW5	600
410	GO TO(410,420,430)1,MM	VIEW5	601
410	CL=CI	VIEW5	602
	MM=2	VIEW5	603
	IF(92) 414,415,414	VIEW5	604
414	P2=RA*OP2/2.	VIEW5	605
	GO TO 406	VIEW5	606
414	V2=YK+DY2/2.	VIEW5	607
	GO TO 405	VIEW5	608
420	MM=3	VIEW5	609
	IF(82) 424,426,424	VIEW5	610
424	P2=RA*OP2/1.5+0.5*CI1	VIEW5	611
	GO TO 406	VIEW5	612
424	V2=YK+DY2/(1.5+0.5*CI1)	VIEW5	613
	GO TO 405	VIEW5	614
430	MM=1	VIEW5	615
	IF(82) 434,436,434	VIEW5	616
434	R=R+IDR2/1.5+0.5*CI+0.8*GH+5.*GR1	VIEW5	617
	GO TO 400	VIEW5	618
434	R = R+IDV2/1.8+1*15.*GL+8.*GH+5.*GR1	VIEW5	619
620	CONTINUE	VIEW5	620
440	IF(SH40) 450,450,510	VIEW5	621
450	IF(91) 452,454,452	VIEW5	622
452	GO TO(470,440,490)1,LL	VIEW5	623
454	GO TO (472,452,492)1,LL	VIEW5	624
625	RL = R*RI/435(91)	VIEW5	625
470	VI = VJ/0.1/2.	VIEW5	626
		VIEW5	627
		VIEW5	628

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630	672	688	692	698	702	708	712	718	722	728	732	738	742	748	752	758	762	768	772	778	782	788	792	798	802	808	812	818	822	828	832	838	842	848	852	858	862	868	872	878	882	888	892	898	902	908	912	918	922	928	932	938	942	948	952	958	962	968	972	978	982	988	992	998	1002	1008	1012	1018	1022	1028	1032	1038	1042	1048	1052	1058	1062	1068	1072	1078	1082	1088	1092	1098	1102	1108	1112	1118	1122	1128	1132	1138	1142	1148	1152	1158	1162	1168	1172	1178	1182	1188	1192	1198	1202	1208	1212	1218	1222	1228	1232	1238	1242	1248	1252	1258	1262	1268	1272	1278	1282	1288	1292	1298	1302	1308	1312	1318	1322	1328	1332	1338	1342	1348	1352	1358	1362	1368	1372	1378	1382	1388	1392	1398	1402	1408	1412	1418	1422	1428	1432	1438	1442	1448	1452	1458	1462	1468	1472	1478	1482	1488	1492	1498	1502	1508	1512	1518	1522	1528	1532	1538	1542	1548	1552	1558	1562	1568	1572	1578	1582	1588	1592	1598	1602	1608	1612	1618	1622	1628	1632	1638	1642	1648	1652	1658	1662	1668	1672	1678	1682	1688	1692	1698	1702	1708	1712	1718	1722	1728	1732	1738	1742	1748	1752	1758	1762	1768	1772	1778	1782	1788	1792	1798	1802	1808	1812	1818	1822	1828	1832	1838	1842	1848	1852	1858	1862	1868	1872	1878	1882	1888	1892	1898	1902	1908	1912	1918	1922	1928	1932	1938	1942	1948	1952	1958	1962	1968	1972	1978	1982	1988	1992	1998	2002	2008	2012	2018	2022	2028	2032	2038	2042	2048	2052	2058	2062	2068	2072	2078	2082	2088	2092	2098	2102	2108	2112	2118	2122	2128	2132	2138	2142	2148	2152	2158	2162	2168	2172	2178	2182	2188	2192	2198	2202	2208	2212	2218	2222	2228	2232	2238	2242	2248	2252	2258	2262	2268	2272	2278	2282	2288	2292	2298	2302	2308	2312	2318	2322	2328	2332	2338	2342	2348	2352	2358	2362	2368	2372	2378	2382	2388	2392	2398	2402	2408	2412	2418	2422	2428	2432	2438	2442	2448	2452	2458	2462	2468	2472	2478	2482	2488	2492	2498	2502	2508	2512	2518	2522	2528	2532	2538	2542	2548	2552	2558	2562	2568	2572	2578	2582	2588	2592	2598	2602	2608	2612	2618	2622	2628	2632	2638	2642	2648	2652	2658	2662	2668	2672	2678	2682	2688	2692	2698	2702	2708	2712	2718	2722	2728	2732	2738	2742	2748	
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685	578	LP = 3	PHI1 = PHI1 + .5 * CXL * DPHI1	VIEW3	686
		LV = 1		VIEW3	687
		GO TO 77		VIEW3	688
690	580	DO 590 NM = 1, NYL		VIEW3	689
		NM = 3 * NM - 2		VIEW3	690
		NM1 = 3 * NM - 1		VIEW3	691
		NM2 = 3 * NM		VIEW3	692
695	582	1 * (DPHI1/8, 1) * (F1(NM, 1) * F1(NM, 3) * F1(NM2, 1) + F1(NM2, 3))	VIEW3	693	
		2 * (DPHI1/6, 1) * (F1(NM1, 1) + F1(NM1, 3) + F1(NM2, 1) + F1(NM2, 3))	VIEW3	694	
		IF (N1) 582, 589, 582	VIEW3	695	
		FF = FF + C * DPHI	VIEW3	696	
		GO TO 590	VIEW3	697	
708	589	FF = FF + C * DPHI	VIEW3	698	
		CONTINUE	VIEW3	699	
		LV = 1	VIEW3	700	
		LP = 1	VIEW3	701	
705	607	PHI1 = PHI1 + (1 - C * XL * DPHI1)	VIEW3	702	
		IF (ABS(PHI1 - PHI1) - 1, 0E-2) 630, 630, 607	VIEW3	703	
	607	IF (PHI1 - PHI1) 77, 630, 630	VIEW3	704	
	620	F1(J, K) = FF * 2 * PI * E / A(J)	VIEW3	705	
		F1(K, J) = F1(J, K) * A(J) / A(K)	VIEW3	706	
		GO TO 642	VIEW3	707	
710	630	F1(J, K) = FF * DUCI / A(J)	VIEW3	708	
		F1(K, J) = FF * DUCI / A(K)	VIEW3	709	
	642	IF (COUNT - 4) 642, 643, 643	VIEW3	710	
	643	COUNT = 3	VIEW3	711	
		COUNT = 1	VIEW3	712	
715	644	GO TO 641	VIEW3	713	
		CALL TEST(F1(J, K), DIV, COUNT, R, COUNT, R)	VIEW3	714	
	644	IF (COUNT) 644, 644, 5300	VIEW3	715	
		IF (F1(J, K) * LT, 0.0) F1(J, K) = 0.0	VIEW3	716	
		IF (F1(J, K) * LT, 0.0) F1(K, J) = 0.0	VIEW3	717	
720		NODE = NODE + 1	VIEW3	718	
		NODE = NODE + 1	VIEW3	719	
		FFSR(NODE1, NODE2) = F1(J, K)	VIEW3	720	
		FFSR(NODE2, NODE1) = F1(K, J)	VIEW3	721	
725	15800	CONTINUE	VIEW3	722	
		AR1(NODE1) = A(J) / 144.0	VIEW3	723	
	15800	CONTINUE	VIEW3	724	
	15800	IF (PRINT, EQ, 0) GO TO 670	VIEW3	725	
		WRITE(6, 15001)	VIEW3	726	
730	15001	FORMAT(14, 26X, 26H SYSTEM INTERNAL VIEW FACTORS, //)	VIEW3	727	
		DO 16001 I = 1, NTOT	VIEW3	728	
		DO 16001 J = 1, NTOT	VIEW3	729	
		IF (CLINEI, GE, 500) GO TO 15002	VIEW3	730	
	15004	WRITE(6, 652) I, J, FFSR(I, J), J, FFSR(J, I)	VIEW3	731	
	650	FORMAT(14X, 2MF(1, 12, 14), 12, 3M) = , F7.5, 10F, 2MF(1, 12, 14), 12, 3M) = , F7.5	VIEW3	732	
		1)	VIEW3	733	
		LINE1 = LINE1 + 1	VIEW3	734	
		GO TO 16002	VIEW3	735	
740	15802	WRITE(6, 15001)	VIEW3	736	
		LINE1 =	VIEW3	737	
		GO TO 15004	VIEW3	738	
	15800	CONTINUE	VIEW3	739	
			VIEW3	740	
			VIEW3	741	
			VIEW3	742	

```

745 LINE7=LINE7+1
      ARE2=ARE1(IJ*144,8)
      WRITE(6,15005) I,ARE2
15005 FORMAT(28X,5MAREAT,12,3H)=.FT,2,0M,50. IN,0//1
      LINE7=LINE7+2
16001 CONTINUE
      670 IF(IKKKI.EQ.0) GO TO 671
      DO 572 I=1,NTOT
        PUNCH 673, IFFSR(I,I),I=1,NTOT)
        ARE2=ARE1(IJ*144,8)
        672 PUNCH 673, ARE2
        673 FORMAT(8F17,5)
        IF(ISTOP11.EQ.3) STOP
      671 CONTINUE
      END

```

```

      VIEW$ 743
      VIEW$ 744
      VIEW$ 745
      VIEW$ 746
      VIEW$ 747
      VIEW$ 748
      VIEW$ 749
      VIEW$ 750
      VIEW$ 751
      VIEW$ 752
      VIEW$ 753
      VIEW$ 754
      VIEW$ 755
      VIEW$ 756
      VIEW$ 757

```

	SUBROUTINE ARCCOSICS,ANG,ITA)	ARCCOS	2
	PIEI = 3.141592653589793	ARCCOS	3
	TABSTICS) - 1.0	ARCCOS	4
	IFIT) 67.6601.6602	ARCCOS	5
	IFICS) 6603.6603.6606	ARCCOS	6
	ANG = PIEI	ARCCOS	7
	GO TO 70	ARCCOS	8
	ANG=2.0	ARCCOS	9
	GO TO 70	ARCCOS	10
10	6602 IF(ABS(PI-1.0E-5)) 6603,6604,6605	ARCCOS	11
	NO SOLUTION	ARCCOS	12
	ITA=2	ARCCOS	13
	RETURN	ARCCOS	14
	IFICS) 6720,6710,6720	ARCCOS	15
15	5710 ANG = PIEI/2.	ARCCOS	16
	GO TO 70	ARCCOS	17
	6720 TP2PI=SQRT(1.-CS**2)/CS	ARCCOS	18
	ANG=ATAN(TP2PI)	ARCCOS	19
	IF(TP2PI) 60,70,70	ARCCOS	20
20	60 ANG = ANG+ PIEI	ARCCOS	21
	A SOLUTION WAS FOUND	ARCCOS	22
	ITA=1	ARCCOS	23
	RETURN	ARCCOS	24
	END	ARCCOS	25

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SUBROUTINE QUAD(A,B,C,RP1,RI1,RR2,RI2,IOR)

IF(A*B*(A-1-BE-4) 5,5,30

IF(A*B*(B-1-BE-4) 10,10,15

NO SOLUTION

5

10

RETURN

ONE REAL SOLUTION

RR1=-C/B

IOR=2

RETURN

DISC = B*B-A*A+C

IF(DISC) 40,30,60

COMPLEX ROOTS

IOR=3

RR1 = -B/(2.*A)

RI1 = C.5*SQR((-DISC))/A

RR2= RP1

RI2 = -RI1

RETURN

IDENTICAL ROOTS

IOR = 2

RR1 = -B/(2.*A)

RETURN

TWO REAL ROOTS

IOR = 1

RR1 = 0.5*(-B+SQR(DISC))/A

RR2 = 0.5*(-B-SQR(DISC))/A

RETURN

END

QUAD 2
QUAD 3
QUAD 4
QUAD 5
QUAD 6
QUAD 7
QUAD 8
QUAD 9
QUAD 10
QUAD 11
QUAD 12
QUAD 13
QUAD 14
QUAD 15
QUAD 16
QUAD 17
QUAD 18
QUAD 19
QUAD 20
QUAD 21
QUAD 22
QUAD 23
QUAD 24
QUAD 25
QUAD 26
QUAD 27
QUAD 28
QUAD 29
QUAD 30

[illegible]

59	C	223	ONE SOLUTION IC3=3 R01=0 RETURN	CUBIC	59
60				CUBIC	60
61				CUBIC	61
62				CUBIC	62
63				CUBIC	63
64				CUBIC	64
65				CUBIC	65
66				CUBIC	66
67				CUBIC	67
68				CUBIC	68
69				CUBIC	69
70				CUBIC	70
71				CUBIC	71
72				CUBIC	72
73				CUBIC	73
74				CUBIC	74
75				CUBIC	75
76				CUBIC	76
77				CUBIC	77
78				CUBIC	78
79				CUBIC	79
80				CUBIC	80
81				CUBIC	81
82				CUBIC	82
83				CUBIC	83
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96				CUBIC	96
97				CUBIC	97
98				CUBIC	98
99				CUBIC	99
100				CUBIC	100
101				CUBIC	101
102				CUBIC	102
103				CUBIC	103
104				CUBIC	104
105				CUBIC	105
106				CUBIC	106
107				CUBIC	107
108				CUBIC	108

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	SUBROUTINE TEST1(R1T,R2T,PM1OT,PM1T,X1T,Z1T,TEST1)	TEST1	2
	DEMO= R2T+2*R1T+2-2.*R2T+R1T+COS(PM1OT)	TEST1	3
	IF (DEMO) 20,20,10	TEST1	4
5	PM1Z= PM1T+PM1OT	TEST1	5
10	XZ= R1T+R2T+SIN(PM1OT)*(R2T*SIN(PM1Z)-R1T*SIN(PM1T))/DEMO	TEST1	6
	ZZ= R1T+R2T+SIN(PM1OT)*(R2T*COS(PM1Z)-R1T*COS(PM1T))/DEMO	TEST1	7
	XZT=R2T+COS(PM1Z)	TEST1	8
	ZZT=R2T+SIN(PM1Z)	TEST1	9
	D1F= SQRT((X1T-XZT)**2+(Z1T-ZZT)**2)	TEST1	10
11	DZ= SQRT((X2T-XZT)**2+(Z2T-ZZT)**2)	TEST1	11
	D1Z= SQRT((X1T-XZT)**2+(Z1T-ZZT)**2)	TEST1	12
	IF (A1)SID1F-D1Z) -1,DE-03) 11,11,12	TEST1	13
	01F=01Z	TEST1	14
12	IF (A3)D2F-D1Z) -1,DE-03) 13,13,14	TEST1	15
13	DZ= D1Z	TEST1	16
14	IF (A5-D1Z) 15,15,20	TEST1	17
15	IF (D2F-D1Z) 25,25,20	TEST1	18
	SOLUTION IS NOT VALID FOR THIS PROBLEM	TEST1	19
20	TEST1 = 2	TEST1	20
	RETURN	TEST1	21
	SOLUTION IS VALID FOR THIS PROBLEM	TEST1	22
25	TEST1 = 1	TEST1	23
	RETURN	TEST1	24
	END	TEST1	25

				TEST2	2
				TEST2	3
				TEST2	4
				TEST2	5
				TEST2	6
				TEST2	7
				TEST2	8
				TEST2	9
				TEST2	10
				TEST2	11
				TEST2	12
				TEST2	13
				TEST2	14
				TEST2	15
				TEST2	16
				TEST2	17
				TEST2	18


```

SUBROUTINE TEST2(YU,YD,YF,IFYF)
  YUD=ABS(YD-YU)
  YFD=ABS(YD-YF)
  YFU=ABS(YU-YF)
  IF(ABS(YUD-YFD)-1.0E-03) 1,1,2
  1 YFD=YUD
  2 IF(ABS(YUD-YFU)-1.0E-03) 3,3,4
  3 YFU=YUD
  4 IF(YFD-YUD) 5,5,10
  5 IF(YFU-YUD) 15,15,10
  IF IS NOT A VALID SOLUTION FOR THIS PROBLEM
  10 IF YE=2
  RETURN
  IF IS A VALID SOLUTION FOR THIS PROBLEM
  IFYF = 1
  RETURN
  END
  
```

	SUBROUTINE FINDITV,YF,I,NPS,NVU1		FINDIT	
	DIMENSION YF(10,20)		FINDIT	2
	DO 100 J=1,NPS		FINDIT	3
	IF(Y-YF(I,J)) 10,40,50		FINDIT	4
5	IF(J-1) 20,20,30		FINDIT	5
	NVU=0		FINDIT	6
	GO TO 119		FINDIT	7
	NVU=J-1		FINDIT	8
	GO TO 110		FINDIT	9
10	NVU=J		FINDIT	10
	GO TO 110		FINDIT	11
	IF(J-NPS)100,60,60		FINDIT	12
	NVU=J		FINDIT	13
	GO TO 113		FINDIT	14
15	CONTINUE		FINDIT	15
	RETURN		FINDIT	16
	END		FINDIT	17
			FINDIT	18

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```

SUBROUTINE CODE(NY1,NY2,NPS,ICODE)
  IF(NY1) 18,19,15
  IF(NY2) 20,21,25
  BOTH Y1 AND Y2 ARE UPSTREAM OF THE SHADOWING BODY
  5      ICODE=9
  RETURN
  25  IF(NY2-NPS) 30,35,35
  Y1 IS UPSTREAM AND Y2 IS DOWNSTREAM OF THE SHADOWING BODY
  35  ICODE=1
  RETURN
  19  Y1 IS UPSTREAM AND Y2 IS WITHIN Y BAND OF BODY
  30  ICODE=2
  RETURN
  45  IF(NY1-NPS) 40,45,45
  IF(NY2) 50,50,55
  Y1 IS WITHIN Y BAND OF BODY AND Y2 IS UPSTREAM OF IT
  50  ICODE=3
  RETURN
  55  IF(NY2-NPS) 60,65,65
  Y1 IS WITHIN Y BAND OF BODY AND Y2 IS DOWNSTREAM OF IT
  65  ICODE=4
  RETURN
  20  Y1 IS WITHIN Y BAND OF BODY AND Y2 IS ALSO WITHIN THAT BAND
  60  ICODE=5
  RETURN
  45  IF(NY2-NPS) 75,70,70
  BOTH Y1 AND Y2 LIE DOWNSTREAM OF THE SHADOWING BODY
  70  ICODE=8
  RETURN
  35  IF(NY2) 80,80,85
  Y1 IS DOWNSTREAM OF BODY AND Y2 IS WITHIN THE Y BAND OF THE BODY
  85  ICODE=6
  RETURN
  35  Y1 IS DOWNSTREAM OF BODY AND Y2 IS UPSTREAM OF IT
  80  ICODE=7
  RETURN
  END

```

		SUBROUTINE CANSEE(Y1,R1,Y2,R2,VF,RF,K1,KIL,JJ,ISSE)			
		DIMENSION VF(13,20),RF(10,20)			
		IO=0			
5		JD=0		CANSEE	2
		KICK=1		CANSEE	3
		KSE=K1		CANSEE	4
		R2T=R2		CANSEE	5
		RJT=RF(JJ,KK)		CANSEE	6
		RJT=RF(JJ,KK+1)		CANSEE	7
		VOT=VF(JJ,KK)		CANSEE	8
		VOT=VF(JJ,KK+1)		CANSEE	9
		GO TO 10		CANSEE	10
		PUT=RF(JJ,KK)		CANSEE	11
		PUT=RF(JJ,KK+1)		CANSEE	12
		POT=-RF(JJ,KK+1)		CANSEE	13
		VOT=VF(JJ,KK)		CANSEE	14
		VOT=VF(JJ,KK+1)		CANSEE	15
		VDEN=(R2T-R1)/(V2-Y1)-(RDT-RDT)/(VDT-YDT)		CANSEE	16
		IF(ABS(VDEN)-1.0E-03) 200,200,70		CANSEE	17
		VDT=1-RDT/VDT-2DT/VDT/(VDT-VDT)-(R1+Y2-R2T+Y1)/(V2-Y1)		CANSEE	18
		V1=Y2/VDEN		CANSEE	19
		IF(ABS(V1)-1.0E-3) 200+200,60		CANSEE	20
		IF(ABS(V2-Y1)-1.0E-3) 200,200,50		CANSEE	21
		CALL TEST2(VOT,VOT,V1,L1V1)		CANSEE	22
		IF(L1V1-1) 55,65,200		CANSEE	23
		CALL TEST2(Y1,Y2,Y1,LARCV1)		CANSEE	24
		IF(LARCV1-1) 67,67,200		CANSEE	25
		IF(KICK-2) 120,125,130		CANSEE	26
		KSE=K1		CANSEE	27
		KICK=2		CANSEE	28
		IO=1		CANSEE	29
		R2T=-R2		CANSEE	30
		GO TO 30		CANSEE	31
		JD=1		CANSEE	32
		KICK=3		CANSEE	33
		KSE=K1		CANSEE	34
		GO TO 50		CANSEE	35
		JD=JD+1		CANSEE	36
		GO TO 155		CANSEE	37
		IF(KX-KIL) 135,140,140		CANSEE	38
		KSE=K1		CANSEE	39
		IF(KICK-2) 30,30,50		CANSEE	40
		IF(KICK-2) 145,150,155		CANSEE	41
		KICK=2		CANSEE	42
		R2T=-R2		CANSEE	43
		KSE=K1		CANSEE	44
		GO TO 30		CANSEE	45
		KICK=3		CANSEE	46
		KSE=K1		CANSEE	47
		GO TO 50		CANSEE	48
		IF(L1) 150,150,155		CANSEE	49
		IF(JD) 170,170,175		CANSEE	50
		KSE=K1		CANSEE	51
		VOT=VF(JJ,KK)		CANSEE	52
		VOT=VF(JJ,KK+1)		CANSEE	53
		PUT=RF(JJ,KK)		CANSEE	54
		CALL TEST2(V1,Y2,VOT,IFV)		CANSEE	55
		IF(IFV-1) 201,201,195		CANSEE	56
		KSE=K1		CANSEE	57
				CANSEE	58

```

60      C      193,190,228
      THE BODY CAUSES NO SHADOWING
      ISEE=1
      RETURN
      201      RC= (Y2-YUT)*R1/(Y2-V1)
      RHO= R2*(YU1-Y1)/(Y2-Y1)
      X1= RC+PHO
      Y2= RC-RHO
      IF1 ABS(UT-Y1)-1.0E-03) 193,195,205
      IF1 ABS(X2+PUT)-1.0E-03) 195,195,210
      205      IF(X1-PUT) 220,220,230
      210      IF(X2+PUT) 220,220,240
      230      IF(X2+PUT) 220,220,240
      70      C THE FRUSTUM SHADOWS WITH ITS OUTSIDE SURFACE BUT SHADOWING DOES NOT E
      C FOR PH12= 100 DEGREES AS IT DOES FOR ISEE=2
      240      ISEE= 5
      RETURN
      75      C THE BODY CAUSES SHADOWING WITH ITS OUTSIDE SURFACE
      175      ISEE= 2
      RETURN
      165      IF(JDI) 100,100,105
      C THE BODY CAUSES SHADOWING WITH ITS INSIDE SURFACE
      180      ISEE=3
      RETURN
      00      THE BODY CAUSES COMPLETE SHADOWING
      105      ISEE= 4
      RETURN
      END

```

	SUBROUTINE BODY(V1,V2,R1,R2,VFU,BFU,VFO,RFO,PHIO,PHIL,IOM)	BODY	2
	EF= (RFU*VFO-RFO*VFU)/(VFO-VFU)	BODY	3
	FF= (RFO-RFU)/(VFO-VFU)	BODY	4
	FC= EF*FF*V1	BODY	5
5	RC= EF*FF*V2	BODY	6
	IF (ABS(PC1-R1)-1,DE-31,10,12,20	BODY	7
10	IF (ABS(PC2-R2)-1,DE-31,10,12,20	BODY	8
15	IF (ABS(PC3-R3)-1,DE-31,10,12,20	BODY	9
	C 30TH POINTS 1 AND 2 LIE ON THE SHADING BODY SHADING TAKEN CARE OF E.	BODY	10
20	IF (R1-ABS(PC1)) 9830,22,22	BODY	11
25	IF (R2-ABS(PC2)) 9832,24,24	BODY	12
	AF = -1*(RFO-RFU)/SQRT(VFO-VFU)*2*(RFO-RFU)*2	BODY	13
	BF = 1*(VFO-VFU)/SQRT(VFO-VFU)*2*(RFO-RFU)*2	BODY	14
	CF = 8*(V2-V1)*2*(V1-R2)*2-1*(R2-V1)*2	BODY	15
	CE = 8*(V1+V2)*R2*2	BODY	16
	CF = 8*(R2*2+R1*2)+AF*FF*(V2-V1)*2	BODY	17
	CE = 2*(R2*2+R1*2)	BODY	18
	CF = 2*(R2*2+R1*2)*2-1*(R2*2+R1*2)	BODY	19
	CE = 2*(R2*2+R1*2)*2-1*(R2*2+R1*2)	BODY	20
	CF = 2*(R2*2+R1*2)	BODY	21
	CE = 2*(V1+V2)*R2*2	BODY	22
	CF = 2*(V1+V2)*R2*2	BODY	23
	CE = 2*(V1+V2)*R2*2	BODY	24
	CF = 2*(V1+V2)*R2*2	BODY	25
	CE = 2*(V1+V2)*R2*2	BODY	26
	CF = 2*(V1+V2)*R2*2	BODY	27
	CE = 2*(V1+V2)*R2*2	BODY	28
	CF = 2*(V1+V2)*R2*2	BODY	29
	CE = 2*(V1+V2)*R2*2	BODY	30
	CF = 2*(V1+V2)*R2*2	BODY	31
	CE = 2*(V1+V2)*R2*2	BODY	32
	CF = 2*(V1+V2)*R2*2	BODY	33
	CE = 2*(V1+V2)*R2*2	BODY	34
	CF = 2*(V1+V2)*R2*2	BODY	35
	CE = 2*(V1+V2)*R2*2	BODY	36
	CF = 2*(V1+V2)*R2*2	BODY	37
	CE = 2*(V1+V2)*R2*2	BODY	38
	CF = 2*(V1+V2)*R2*2	BODY	39
	CE = 2*(V1+V2)*R2*2	BODY	40
	CF = 2*(V1+V2)*R2*2	BODY	41
	CE = 2*(V1+V2)*R2*2	BODY	42
	CF = 2*(V1+V2)*R2*2	BODY	43
	CE = 2*(V1+V2)*R2*2	BODY	44
	CF = 2*(V1+V2)*R2*2	BODY	45
	CE = 2*(V1+V2)*R2*2	BODY	46
	CF = 2*(V1+V2)*R2*2	BODY	47
	CE = 2*(V1+V2)*R2*2	BODY	48
	CF = 2*(V1+V2)*R2*2	BODY	49
	CE = 2*(V1+V2)*R2*2	BODY	50
	CF = 2*(V1+V2)*R2*2	BODY	51
	CE = 2*(V1+V2)*R2*2	BODY	52
	CF = 2*(V1+V2)*R2*2	BODY	53
	CE = 2*(V1+V2)*R2*2	BODY	54
	CF = 2*(V1+V2)*R2*2	BODY	55
	CE = 2*(V1+V2)*R2*2	BODY	56
	CF = 2*(V1+V2)*R2*2	BODY	57
	CE = 2*(V1+V2)*R2*2	BODY	58
	CF = 2*(V1+V2)*R2*2	BODY	59

A-186

9862	DED=C3-C4*RR1		800Y	59
	IF(AS(DED).LE.1.0E-5)	GO TO 9830	800Y	60
	VF=(C1-C2*RR1)/DED		800Y	61
68	CALL TEST2(VF,VF,VF,IFV)		800Y	62
	IF(IFY - 1) 9863, 9863, 9830		800Y	63
	CALL TEST2(Y1,Y2,YE,ALOU1)		800Y	64
	IF(LOU1-1) 520,520,9830		800Y	65
65	523	CALL CHECK(PHIO,PHI1,Y1,R1,Y2,R2,VF,AF,BF,EF,FF,IG0)	800Y	66
	IF(IG0-1) 9F50,9850,9830		800Y	67
	C A VALID SOLUTION HAS BEEN FOUND.		800Y	68
	9858	ION=2	800Y	69
	RETURN		800Y	70
70	C NO VALID SOLUTION WAS FOUND.		800Y	71
	9830	ION=3	800Y	72
	RETURN		800Y	73
	END		800Y	74

A-188

		SUBROUTINE CHECK(PHI0,PHI1,VA,RI,V2,R2,VFAF,BF,EF,FF,IGOI)	CHECK	2
		PHI2=PHI1+PHI0	CHECK	3
		X1=R1*COB(PHI1)	CHECK	4
		X2=R2*COB(PHI2)	CHECK	5
5		XF=X1+VF-Y11*(X2-X1)/(V2-V1)	CHECK	6
		Z1=R1*SIN(PHI1)	CHECK	7
		Z2=R2*SIN(PHI2)	CHECK	8
		ZF=X1+VF-Y11*(Z2-Z1)/(V2-V1)	CHECK	9
		BF=EF+EFFV	CHECK	10
10		RCFS=XF**2+ZF**2	CHECK	11
		IF(RCFS) 10,10,20	CHECK	12
		GO TO 2	CHECK	13
		NO BLUCKAGE INDICATED BY THIS SOLUTION	CHECK	14
15		GO TO 2	CHECK	15
		RETURN	CHECK	16
		RCF=5021(RCFS)	CHECK	17
		IF(ABS(REF)-1.0E-03) 30,30,40	CHECK	18
		THE SOLUTION IS AN EXTRANEIOUS SOLUTION FOR THIS PROBLEM	CHECK	19
		GO TO 2	CHECK	20
		RETURN	CHECK	21
20		CANS=(R2-X1)*BF*VF/RFAF+(V2-V1)*(Z2-Z1)*BF*ZF/RF	CHECK	22
		IF(ABS(CANS)-1.0E-03) 60,60,50	CHECK	23
		THE SOLUTION IS AN EXTRANEIOUS SOLUTION FOR THIS PROBLEM	CHECK	24
		GO TO 2	CHECK	25
		RETURN	CHECK	26
25		THE SOLUTION IS THE CORRECT SOLUTION TO THE PROBLEM	CHECK	27
		GO TO 1	CHECK	28
		RETURN	CHECK	29
		END	CHECK	30

	SUBROUTINE RING(Y1,P1,Y2,R2,YF,R2,YF,RF,PHI,LOU)		
	Q2=(Y2-YF)*P1/(Y2-Y1)		RING
	RM0= P2*(YF-Y1)/(Y2-Y1)		RING
	IF (PF-(FC-RM0)) < .1E-20		RING
5	C THE CONE OF VISION DOES NOT INTERSECT THE SHADOWING FRUSTUM FOR THIS Y		RING
	R THIS APPLIES TO OUTSIDE SHADOWING ONLY.		RING
	LOU=2		RING
	RETURN		RING
10	YF= 0.5*(XC+RF+PF/PC-RM0*PH0/R0)		RING
	ZFS= RF**2-XF**2		RING
15	IF (ZFS) 30,40,40		RING
	C THE CONE OF VISION COMPLETELY SURROUNDS THE SHADOWING FRUSTUM FOR THIS RING		RING
	C FOR OUTSIDE SHADOWING OF THE CONE OF VISION LIES INSIDE THE SHADOWING		RING
	C FRUSTUM FOR THIS YF FOR INSIDE SHADOWING		RING
	LOU= 1		RING
	RETURN		RING
	Y2R= R1*(Y2-Y1)*(XF-R1)/(YF-Y1)		RING
	CS= X2E/R2		RING
	CALL ARCCOS(CS,P41,IDA)		RING
20	IF (IDA-1) 50,50,60		RING
	C SOMETHING IS WRONG WITH THE SOLUTION OBTAINED FOR X2R.		RING
	LOU=3		RING
	RETURN		RING
	C A SOLUTION FOR RING SHADOWING HAS BEEN FOUND.		RING
25	LOU= 4		RING
	RETURN		RING
	END		RING

		SUBROUTINE PICMAT(PHIS,LIBRY,LLIM,PHAM)			
DIMENSION PHIS(20)		PICMAX	2		
IF(LLIM-1) 1295,1290,1095		PICMAX	3		
LIBRY=LIBRY+1		PICMAX	4		
PHAM=PHIS(1)		PICMAX	5		
GO TO 1297		PICMAX	6		
1095 LAB-Y = LIB-Y + 1		PICMAX	7		
PHAM=PHIS(1)		PICMAX	8		
DO 10 I=1, L		PICMAX	9		
IF(PHAM-D-LLIM)		PICMAX	10		
PHAM=PHIS(1)		PICMAX	11		
1098 PHAM=PHIS(1)		PICMAX	12		
1097 CONTINUE		PICMAX	13		
1295 RETURN		PICMAX	14		
END		PICMAX	15		

		TESTN	
	SUBROUTINE TESTING FT, DIV, KOUNTIR, COUNTIR	2	
	DIMENSION DIV(2)	3	
	IF(KOUNTIR) 2, 2, 10	4	
5	2 FT1=FT	5	
	3 DO 5 I=1, 2	6	
	5 DIV(I)=DIV(I)+DIV(I)	7	
	KOUNTIR=1	8	
	COUNTIR=COUNTIR+1	9	
	RETURN	10	
10	10 IF(ABS(FT1-FT))=0.001, 5, 6, 6	11	
	6 FT1=FT	12	
	6 FT1=FT	13	
	15 KOUNTIR=0	14	
	COUNTIR=0	15	
15	RETURN	16	
	END	17	

	OVERLAY(TEMP,13,0)			TAS193	2
	PROGRAM TAS19			TAS193	3
	COMMON /TAX/ TF(80),N			TAS193	4
5	COMMON /PRINT/ PRINT1, PRINT2, PRINT3, PRINT4, PRINT5, PRINT6, PRINT7, PRINT8, PRINT9, PRINT10			TAS193	5
	INTEGER PRINT1,PRINT2,PRINT3,PRINT4,PRINT5,PRINT6,PRINT7,PRINT8, PRINT9,PRINT10			TAS193	6
	COMMON /TAIL/ NFILL1(122),EIR(80)			TAS193	7
10	COMMON F			TAS193	8
	DIMENSION F (80,80)			TAS193	9
	DIMENSION FA (80,80)			TAS193	10
	DIMENSION C (80,80)			TAS193	11
15	DIMENSION SMAT (20,80)			TAS193	12
	DIMENSION SMAT (8,80)			TAS193	13
	DIMENSION SMAT (20,80)			TAS193	14
	EQUIVALENCE (F,FA)			TAS193	15
	EQUIVALENCE (F,C)			TAS193	16
20	EQUIVALENCE (F,SMAT)			TAS193	17
	EQUIVALENCE (F,SMAT)			TAS193	18
	EQUIVALENCE (F,SMAT)			TAS193	19
	DIMENSION P (80)			TAS193	20
	DIMENSION P (80)			TAS193	21
25	DIMENSION P (80)			TAS193	22
	DIMENSION P (80)			TAS193	23
	DIMENSION P (80)			TAS193	24
	DIMENSION P (80)			TAS193	25
30	DIMENSION P (80)			TAS193	26
	DIMENSION P (80)			TAS193	27
	DIMENSION P (80)			TAS193	28
	DIMENSION P (80)			TAS193	29
	DIMENSION P (80)			TAS193	30
	DIMENSION P (80)			TAS193	31
	DIMENSION P (80)			TAS193	32
	DIMENSION P (80)			TAS193	33
	DIMENSION P (80)			TAS193	34
35	DIMENSION P (80)			TAS193	35
	DIMENSION P (80)			TAS193	36
	DIMENSION P (80)			TAS193	37
	DIMENSION P (80)			TAS193	38
	DIMENSION P (80)			TAS193	39
	DIMENSION P (80)			TAS193	40
40	DIMENSION P (80)			TAS193	41
	DIMENSION P (80)			TAS193	42
	DIMENSION P (80)			TAS193	43
	DIMENSION P (80)			TAS193	44
	DIMENSION P (80)			TAS193	45
45	DIMENSION P (80)			TAS193	46
	DIMENSION P (80)			TAS193	47
	DIMENSION P (80)			TAS193	48
	DIMENSION P (80)			TAS193	49
	DIMENSION P (80)			TAS193	50
50	DIMENSION P (80)			TAS193	51
	DIMENSION P (80)			TAS193	52
	DIMENSION P (80)			TAS193	53
	DIMENSION P (80)			TAS193	54
	DIMENSION P (80)			TAS193	55
55	DIMENSION P (80)			TAS193	56
	DIMENSION P (80)			TAS193	57
	DIMENSION P (80)			TAS193	58

```

CALL      SCRIP (NDIM,F,M,EIR,A,1.0,
1      S1,S2,NX2,NX3,BUFFER)
CALL WRTIT4      IF,N,NX2,NX3,3,BUFFER)
68      DO 509 INEX=L,15
          RPN=ND 2
          IF (LINDEX=EQ,1) GO TO 505
          CALL DINVRT (NDIM,SMAT ,N,ALPHA,1,S1,S2)
65      DO 508 I=1,N
          IF (I=ALPHA(I))-460.
          506      F (I)=ALPHA(I)
          505      IEND=1
          DO 506 I=1,N
          DO 507 J=1,N
          500      SMAT(I,J)=C.
          DO 501 I=1,N
          501      ALPHA(I)=-(ABS(P(I)))
          75      IF (CT(I),LT,(-499.1)) GO TO 503
          DO 502 J=1,N
          502      SMAT(I,J)=CRODEL(I,J)
          503      ALPHA(I)=C(I)*N63.
          CONTINUE
          DO 510 I=1,N
          READ (2) (BUFFER(J),J=1,NX3)
          DO 504 J=1,N
          IF (CT(I),GT,(-499.1)) GO TO 504
          IF (I=EQ,1) GO TO 506
          85      J=J+NX2
          SMAT(I,J)=SMAT(I,I)-BUFFER(J)-BOLTZ*BUFFER(J)*%0*(I(I)*%3)
          SMAT(I,J)=      BUFFER(J)+BOLTZ*BUFFER(J)*%0*(I(I)*%3)
          ALPHA(I)=ALPHA(I)-BOLTZ*BUFFER(J)*%30*(I(I)*%4)-(I(J)*%4)
          504      CONTINUE
          OTOTAL(I)=-(ABS(P(I)))
          90      DO 506 J=1,N
          J3=J+NX2
          IF (IBUFFER(J3)+BUFFER(J))      J,ER,(0.1) GO TO 506
          OC=BUFFER (J)*C(I(I)      )-C(I(I)      )
          OK=BUFFER(J3)*C(I(I)*%3)-(I(I)*%3)*BOLTZ
          OTOTAL(I)=OTOTAL(I)+OC+OK
          95      CONTINUE
          IF (CT(I),GT,(-499.1)) GO TO 510
          IF (ABS(OTOTAL(I)),GT,RELIG) IEND=2
          100      CONTINUE
          IF (IEND=EQ,1) GO TO 300
          509      CONTINUE
          300      DO 310 I=1,N
          310      F(I)=F(I)+%60.5
          105      AN13      FORMAT(14,29X,'SYSTEM NODE TEMPERATURES',/2)
          1014      FORMAT(15X,'NODE NO. ',/2,'/29X,'TEMPERATURE=',F7.2,' DEG. R.',/1)
          IF (POINT=EQ, 0) GO TO 200
          WRITE(6,IC13)
          LIMCT=4
          DO 201 I=1,N
          IF (LIMIT,LE, 56) GO TO 203
          WRITE(5,IC13)
          LIMCT=4
          201      WRITE(6,1014) I,F(I)

```

A-194

TAS135	59
TAS135	60
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TAS135	110
TAS135	111
TAS135	112
TAS135	113
TAS135	114
TAS135	115

115

LINECT=LINECT+3

201 CONTINUE

200 CONTINUE

END

TAS103 116

TAS104 117

TAS105 118

TAS106 119

FUNCTION CROCEL(I,J)
IF (I.NE.J) GO TO 1
CROCEL=1.
RETURN
1 CROCEL=0.
RETURN
END

CROCEL 2
CROCEL 3
CROCEL 4
CROCEL 5
CROCEL 6
CROCEL 7
CROCEL 8

A-196


```

SUBROUTINE MATPOS (NDIM,A,M)
  DIMENSION A(NDIM,NDIM)
  DO 1 I=1,M
    DO 1 J=1,M
      A(I,J)=ABS(A(I,J))
1 CONTINUE
  RETURN
  END

```

```

2 MATPOS
3 MATPOS
4 MATPOS
5 MATPOS
6 MATPOS
7 MATPOS
8 MATPOS
9 MATPOS

```

SUBROUTINE MATSYM (NDIM,F,N)		
DIMENSION F(NDIM,NDIM)		
1	MM=N-1	MATSYM 2
2	DO 3 I=1,MM	MATSYM 3
3	IP=I+1	MATSYM 4
4	DO 5 J=IP,N	MATSYM 5
5	IF (F(I,J).EQ.(0.0)) GO TO 2	MATSYM 6
6	1 F(I,I)=F(I,J)	MATSYM 7
7	GO TO 3	MATSYM 8
8	2 IF (F(I,J).EQ.(0.0)) GO TO 3	MATSYM 9
9	3 CONTINUE	MATSYM 10
10	RETURN	MATSYM 11
11	END	MATSYM 12
12		MATSYM 13
13		MATSYM 14
14		MATSYM 15

```

SUBROUTINE DINVRT (NDIM,A,NIN ,B,MIN ,S1,S2)
  DIMENSION A(NDIM,NDIM),B(NDIM,2)
  DIMENSION S1(2),S2(2)
  INTEGER Z1,Z2,S1
  EQUIVALENCE (IPDM,JRCM), (ICOLM,JCOLM), (AMAX,I,SWAP)
  N=NIN
  M=MIM
  DO 20 J=1,M
    S1(J)=0
    DO 550 I=1,N
      Z1=I+N
      Z2=Z1+N
      AMAX=0.0
      DO 15 J=1,N
        IF (S1(J).EQ.1) GO TO 105
        DO 100 K=1,N
          IF (S1(K)-1) 00,100,740
          IF (ABS(AMAX)-ABS(S1(J,K))) 80,100,108
          80 IFDM=J
          85 IFDM=K
          ICOLM=K
          AMAX=A(J,K)
          100 CONTINUE
          105 CONTINUE
          S1(ICOLM)=S1(I2COLM)+1
          IF (IFDM.EQ.ICOLM) GO TO 260
          DO 230 L=1,M
            SWAP=A(I2COLM,L)
            A(I2COLM,L)=A(ICOLM,L)
            A(I2COLM,L)=SWAP
          200 A(ICOLM,L)=SWAP
          IF (M.LE.0) GO TO 260
          DO 250 L=1,M
            SWAP=B(I2COLM,L)
            B(I2COLM,L)=B(ICOLM,L)
            B(I2COLM,L)=SWAP
          250 B(ICOLM,L)=SWAP
          S1(I2)=ICOLM
          S2(I)=A(ICOLM,ICOLM)
          A(ICOLM,ICOLM)=1.0
          DO 350 L=1,M
            A(ICOLM,L)=A(ICOLM,L)/S2(I)
          350 A(ICOLM,L)=A(ICOLM,L)/S2(I)
          IF (M.LE.0) GO TO 340
          DO 370 L=1,M
            B(ICOLM,L)=B(ICOLM,L)/S2(I)
          370 B(ICOLM,L)=B(ICOLM,L)/S2(I)
          DO 550 L=1,N
            IF (L1.EQ.ICOLM) GO TO 550
            T=A(L1,ICOLM)
            A(L1,ICOLM)=0.0
            DO 450 L=1,M
              A(L1,L)=A(L1,L)-A(ICOLM,L)*T
            450 A(L1,L)=A(L1,L)-A(ICOLM,L)*T
            DO 530 L=1,M
              B(L1,L)=B(L1,L)-B(ICOLM,L)*T
            530 B(L1,L)=B(L1,L)-B(ICOLM,L)*T
            550 CONTINUE
            DO 710 I=1,N
              L=N+1-I
              L1=L+N
              L2=L1+N

```

```

IF (S1(L1),EQ,S1(L2)) GO TO 710
JROM=S1(L1)
JCOLUM=S1(L2)
DO 705 K=1,N
SNAP=AK(JROM)
AK(JROM)=AK(JCOLUM)
AK(JCOLUM)=SNAP
705 CONTINUE
710 CONTINUE
760 RETURN
END

```

DINVT	59
DINVT	60
DINVT	61
DINVT	62
DINVT	63
DINVT	64
DINVT	65
DINVT	66
DINVT	67
DINVT	68
DINVT	69

A-200

	SUBROUTINE WRIT14	(MATRIX,M,NX2,NX3,MATNO,BUFFER)	WRIT14	2
	REAL MATRIX(80,80),	BUFFER(248)	WRIT14	3
	REIND 2		WRIT14	4
5	REIND 4		WRIT14	5
	DO 7 I=1,M		WRIT14	6
	GO TO (1,2,3) MATNO		WRIT14	7
	1 DO 4 J=1,N		WRIT14	8
	4 BUFFER(J)=MATRIX(I,J)		WRIT14	9
10	WRITE(2) (BUFFER(J),J=1,M)		WRIT14	10
	GO TO 7		WRIT14	11
	2 READ(2) (BUFFER(J), J=1,M)		WRIT14	12
	DO 5 J=1,N		WRIT14	13
	J2=J+N		WRIT14	14
15	5 BUFFER(J2)=MATRIX(I,J)		WRIT14	15
	WRITE(4) (BUFFER(J),J=1,NX2)		WRIT14	16
	GO TO 7		WRIT14	17
	3 READ(4) (BUFFER(J), J=1,NX2)		WRIT14	18
	DO 6 J=1,N		WRIT14	19
	J3=J+NX2		WRIT14	20
20	6 BUFFER(J3)=MATRIX(I,J)		WRIT14	21
	WRITE(2) (BUFFER(J),J=1,NX3)		WRIT14	22
	7 CONTINUE		WRIT14	23
	RETURN		WRIT14	24
	END		WRIT14	25

	SUBROUTINE FEOTIT (NOIM,N,M)	FEOTIT	2
	COMMON /ALL/ NFILE(135), A(6)	FEOTIT	3
	COMMON /PLN/ 2(1500)	FEOTIT	4
5	DIMENSION F (50,50)	FEOTIT	5
	DIMENSION FA (80,80)	FEOTIT	6
	EQUIVALENCE (F(150),F(1,1))	FEOTIT	7
	DO 5 I=1,N	FEOTIT	8
	DO 5 J=1,N	FEOTIT	9
	FEOTIT=0.	FEOTIT	10
10	DO 6 I=1,M	FEOTIT	11
	FEOTIT=0.	FEOTIT	12
	DO 6 J=1,N	FEOTIT	13
	FEOTIT=FEOTIT	FEOTIT	14
	FEOTIT=FEOTIT	FEOTIT	15
15	DO 6 I=1,M	FEOTIT	16
	DO 6 J=1,N	FEOTIT	17
	FEOTIT=FEOTIT	FEOTIT	18
	FEOTIT=FEOTIT	FEOTIT	19
	FEOTIT=FEOTIT	FEOTIT	20
20	IF (A(I),EQ,0.) GO TO 9	FEOTIT	21
	DO 8 J=1,N	FEOTIT	22
	FEOTIT=FEOTIT	FEOTIT	23
	FEOTIT=FEOTIT	FEOTIT	24
	FEOTIT=FEOTIT	FEOTIT	25
25	FEOTIT=FEOTIT	FEOTIT	26

A-202

	SUBROUTINE CEDIT (NDIM,M)				
	COMMON C			CE01T	2
	DIMENSION C(80,93)			CE01T	3
	COMMON /HTPACK/ INT(80),MT(80), IM,			CE01T	4
5	DO 4 I=1,M			CE01T	5
	DO 3 J=1,N			CE01T	6
	6 C(I,J)=0.			CE01T	7
	DO 110 I=1,IM			CE01T	8
	I9=INT(I)/100			CE01T	9
10	I8=INT(I)-I9*100			CE01T	10
	C(I9,I8)=MT(I1)			CE01T	11
	100 C(I9,I8)=MT(I1)			CE01T	12
	CALL MATPOS (NDIM,C,M)			CE01T	13
	CALL MATSYM (NDIM,C,M)			CE01T	14
15	RETURN			CE01T	15
	END			CE01T	16

	SUBROUTINE SCRIPT (NDIM,F,N,E,A,BOLIZ,	S1,S2,NX2,NY3,BUFFER)	SCRIPT	
	DIMENSION F(100,80)	(60)	SCRIPT	2
	DIMENSION E	(100)	SCRIPT	4
	DIMENSION A	(100)	SCRIPT	5
5	DIMENSION S1	(240)	SCRIPT	6
	DIMENSION S2	(80)	SCRIPT	7
	DIMENSION BUFFER(240)		SCRIPT	8
	DO 1 I=1,N		SCRIPT	9
	DO 1 J=1,N		SCRIPT	11
10	F(I,J)=CODEL(I,J)-((I-E(I))*F(I,J))		SCRIPT	11
	CALL DWRITE (NDIM,F,N,E,S1,S2)		SCRIPT	12
	K=4102		SCRIPT	13
	REWRITE		SCRIPT	14
	DO 6 I=1,N		SCRIPT	15
15	READ(4) (BUFFER(I),J=1,NX2)		SCRIPT	16
	DO 7 J=1,N		SCRIPT	17
	S2(J)=C		SCRIPT	18
	DO 7 K=1,N		SCRIPT	19
	K2=K+N		SCRIPT	20
20	S2(J)=S2(J)+BUFFER(K2)*F(I,J)		SCRIPT	21
	CONTINUE		SCRIPT	22
	WRITE(2) (S2(J),J=1,N)		SCRIPT	23
	CONTINUE		SCRIPT	24
	REWRITE 2		SCRIPT	25
25	DO 130 I=1,N		SCRIPT	26
	READ(2) (S2(J),J=1,N)		SCRIPT	27
	DO 130 J=1,N		SCRIPT	28
	F(I,J)=S2(J)		SCRIPT	29
	CONTINUE		SCRIPT	30
30	DO 11 I=1,N		SCRIPT	31
	PARF=E(I)*A(I)*BOLIZ		SCRIPT	32
	DO 11 J=1,N		SCRIPT	33
	F(I,J)=F(I,J)+E(J)*PARF		SCRIPT	34
	CONTINUE		SCRIPT	35
35	END		SCRIPT	36

A-204

	OVERLAY(RHP,14,0)	TAILS	2
	PROGRAM TAIL	TAILS	3
	COMMON/T/ TNA(20),KSC,NAS,NWL,NPLOT	TAILS	4
	CALL OVERLAY(RHP,12,1)	TAILS	5
S	CALL TAIL1	TAILS	6
	CALL OVERLAY(RHP,12,2)	TAILS	7
C	CALL TAIL2	TAILS	8
	END	TAILS	9

60	1.46X, "OFF-AXIS ANGLE",	
	2 F4.1, "DISC.", /, 47X, "TARGET ALTITUDE", F7.1, " FT.", /, 47X,	PLOT1 59
	3 "SENSOR ALTITUDE", F7.1, " FT.", /, 47X, "TARGET TO SENSOR RANGE",	PLOT1 60
	4 F7.1, " FT.", /, 47X, "MICRONS",	PLOT1 61
7	FORMAT(15,1MI,16(10)-----1)	PLOT1 62
2	FORMAT(12,11F7.3,1X1, /, 55X, "RADIANI INTENSITY", /, 55X, "WAIT/SIF	PLOT1 63
	1RADIANI",	PLOT1 64
63	300 RETURN	PLOT1 65
	END	PLOT1 66
		PLOT1 67

Line	Code	Statement	Line
1	OVERLAY	COMMON/PLM/3(1500)	1
2	PROGRAM	TITLE	2
3	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	3
4	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	4
5	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	5
6	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	6
7	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	7
8	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	8
9	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	9
10	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	10
11	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	11
12	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	12
13	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	13
14	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	14
15	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	15
16	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	16
17	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	17
18	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	18
19	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	19
20	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	20
21	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	21
22	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	22
23	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	23
24	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	24
25	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	25
26	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	26
27	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	27
28	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	28
29	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	29
30	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	30
31	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	31
32	COMMON	/ALL/ N,NH,NV,N,ISURF(50),MODE(55),JSURF(5,2),N(15),NTOTL,	32

[illegible]

[illegible]

60	YAN=ST YAP=CT ZAN=3.0 GO 7 I= NAF,NAL IF (IOUTI) 612,612, 610 IF (YS1II) -YCOR2 1.200.612,612	REOI 59 REOI 60 REOI 61 REOI 62 REOI 63 REOI 64 REOI 65 REOI 66 REOI 67 REOI 68 REOI 69 REOI 70 REOI 71 REOI 72 REOI 73 REOI 74 REOI 75 REOI 76
65	GO TO 628 SHAD=0.0 TAU=THI)*PIE/100.0 CT=CEITAU ST=CHITAU DJ= (PZ2II)-YS1II)/NDIV(I) DVS= (YS2II)-YS1II)/NDIV(I) YB=YS1II)-5*DV3 NAB=NDIV(I) FAB=0.0 D43=SQRT(CS3*2 + DV8**2) R3B=SI1II) - 0.5*OR3 YBN = - ST GO 25 ISR= 1,NAB YB=Y3*DV5 RS9=RS4+OR2 QA=QMI*RC3*DMA PHI=-.5*DPHI GO 5 J = 1,NDIV PHI=PHI+DPHI SP= SIN(PHI) CP= COS(PHI) KB=RS8*CP ZB=RS8*SP XBN=CT*CP ZBN=CT*SP DX=Y3-YA DY=Y3-YA DZ=Z3-ZA R2=OX*OY*OY*OZ*OZ IF(R2) 4,4,16 R1 = SORT(R2) ACOS= (DX*YAN+OY*YAN+OZ*ZAN)/R1 BCOS= (DX*XBN+OY*YBN+OZ*ZBN)/R1 IF (ACOS) 41,41,2 IF (ABS(TH(I))-90.) 43,4,4 F1=J.C GO TO 212 IF(ACOS) 47,47,3 IF (ABS(TH(I))-90.) 43,4,4 OYB=0.0 IF(OY) 19,24,19 OY=1.CE-3*DM3 OYB=OY YB=YA+OY*F XV= (XA*YB-YA*XV)/OY ZV= (ZA*YB-YA*ZV)/OY GO 116 K = 1, NF RCII = REAIK) + (RER(K)-REAIK))*(YS1II)-YFA(K))	REOI 59 REOI 60 REOI 61 REOI 62 REOI 63 REOI 64 REOI 65 REOI 66 REOI 67 REOI 68 REOI 69 REOI 70 REOI 71 REOI 72 REOI 73 REOI 74 REOI 75 REOI 76 REOI 77 REOI 78 REOI 79 REOI 80 REOI 81 REOI 82 REOI 83 REOI 84 REOI 85 REOI 86 REOI 87 REOI 88 REOI 89 REOI 90 REOI 91 REOI 92 REOI 93 REOI 94 REOI 95 REOI 96 REOI 97 REOI 98 REOI 99 REOI 100 REOI 101 REOI 102 REOI 103 REOI 104 REOI 105 REOI 106 REOI 107 REOI 108 REOI 109 REOI 110 REOI 111 REOI 112 REOI 113 REOI 114 REOI 115
68		
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110		

115	115	IF (ABS12 = PFAIK) + (RFBK) - RFAIK) * (VS211) - VFAIK) / (VFBK) - VFAIK)	REOIT	116
	116	IF (ABS12C11-RS1111) - 1.0E-3) 110,118,208	REOIT	117
	117	IF (ABS12C12-RS2111) - 1.0E-3) 100,108,208	REOIT	118
	118	GO TO 116	REOIT	119
120	200	DF = RFRK) - RFAIK)	REOIT	120
		DF = VFAIK) - VFAIK)	REOIT	121
125		RV = (RFAIK) * VFBK) - VFAIK) * RFAIK) / DF	REOIT	122
		AF = (VFAIK) * VFBK) - VFAIK) * RFAIK) / DF	REOIT	123
		3F = 2. * (10 * XV / DV + 0.2 * Y / DV - DF * RW / DV)	REOIT	124
		CF = Y * XV + 2 * YZ - X * RV	REOIT	125
		DF = 8 * CF - 4 * AF * CF	REOIT	126
		IF (DF) 116,111,11	REOIT	127
130	11	DF12 = SCRT(CF)	REOIT	128
		VFI11 = 2.5 * (1 - 3 * DF12) / AF	REOIT	129
		VFI12 = 2.5 * (1 - 3 * DF12) / AF	REOIT	130
		DO 15 L=1,2	REOIT	131
		IF (VFI1) - YB) 15,13,13	REOIT	132
	13	IF (VFI1) - VFAIK) 15,13,13	REOIT	133
	14	IF (VFI1) - VFAIK) 15,13,13	REOIT	134
	15	CONTINUE	REOIT	135
135	116	CONTINUE	REOIT	136
	1060	IF (SWD) 1 57,1057,1069	REOIT	137
		DO 3000 IANG = 1,10000	REOIT	138
		SANG = SIN(THET(IANG))	REOIT	139
		CANG = COS(THET(IANG))	REOIT	140
		IF (ABS1SANG) - 1.0E-4) 1120,1120,1130	REOIT	141
		IF (THET(IANG) - 1.5708) 1121,1121,1122	REOIT	142
		SANG = 0.0000000	REOIT	143
		CANG = 1.0000000	REOIT	144
		GO TO 1123	REOIT	145
145	1122	SANG = 0.0000000	REOIT	146
	1123	IF (Z3 - ZA) 11,10,3000,1140	REOIT	147
	1140	YPP = YA - (YB - YA) * ZA / (ZB - ZA)	REOIT	148
		XPP = XA - (XB - XA) * ZA / (ZB - ZA)	REOIT	149
150	1142	IF (THET(IANG) - 0.01) 1142,1142,1144	REOIT	150
	1144	IF (XPP) 3000,3000,1310	REOIT	151
	1133	IF (ABS1SANG) - 0.9999) 1150,1150,1150	REOIT	152
	1150	IF (THET(IANG) - PIE) 1151,1151,1152	REOIT	153
	1151	SANG = 1.0000000	REOIT	154
		CANG = 0.0000000	REOIT	155
		GO TO 1153	REOIT	156
	1152	SANG = -1.0000000	REOIT	157
		CANG = 0.0000000	REOIT	158
160	1153	IF (X3 - XA) 1170,3000,1170	REOIT	159
	1170	YPP = YA - XA * YB - YAI / (XB - XA)	REOIT	160
		ZPP = ZB - XA * ZB - ZAI / (XB - XA)	REOIT	161
		XPP = 0.0	REOIT	162
165		IF (SANG) 1172,1172,1174	REOIT	163
	1174	IF (ZPP) 3000,3000,1310	REOIT	164
	1172	IF (XPP) 1310,3000,3000	REOIT	165
	1160	IF (X3 - XA) 1160,1190,1190	REOIT	166
	1190	IF (Y3 - YAI) 1200,1210,1220	REOIT	167
	1200	IF (ZB - ZA) 1230,3000,1230	REOIT	168
	1230	ZPP = XA * SANG / CANG	REOIT	169
		YPP = YA + (YB - YAI) * (ZPP - ZAI) / (ZB - ZAI)	REOIT	170
170			REOIT	171
			REOIT	172

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175	1231	IF (SANG) 1231,1231,1232	REDI	173
	1231	IF (ZPP) 1233,3000,3000	REDI	174
	1231	IF (CANG) 1234,1234,1235	REDI	175
	1234	IF (VPI) 1310,3000,3000	REDI	176
	1234	IF (VPP) 3000,3000,1310	REDI	177
	1232	IF (VPI) 3000,3000,1233	REDI	178
	1232	IF (ZB -ZAI) 1240,3000,1240	REDI	179
180	1240	ZPP = YA*SANG/CANG	REDI	180
		YPP = YA	REDI	181
		YPP = YA	REDI	182
		GO TO 1238	REDI	183
	1180	IF (YB -YAI) 1250,1260,1250	REDI	184
	1250	IF (Z3 -ZAI) 1270,1280,1270	REDI	185
	1270	DEAI = (YB -YAI)*SANG/CANG - (ZB -ZAI)	REDI	186
		IF (END) 1290,3000,1290	REDI	187
	1290	YPP = (ZAI*Y3 -ZB*YAI)/GENO	REDI	188
		YPP = YA + (Y3 -YAI)*YPP-XAI/IXB-XAI	REDI	189
190		ZPP = ZA + (ZB -ZAI)*(YPP -XAI)/(X3-XAI)	REDI	190
		GO TO 1238	REDI	191
	1280	XPO = ZA*CANG/SANG	REDI	192
		YPO = YA + (XPP -YAI)*(Y3 -YAI)/(X3 -XAI)	REDI	193
		ZPP = ZA	REDI	194
		GO TO 1239	REDI	195
195	1260	IF (ZB -ZAI) 1270,1300,1270	REDI	196
	1300	YPP = YA	REDI	197
		ZPO = ZA	REDI	198
		XPO = ZA*CANG/SANG	REDI	199
200		GO TO 1238	REDI	200
	1310	RPP = SPT(YPP*2*ZPP*2)	REDI	201
		AA = (RCOR1 -RCOR2)/(YCOR2 -YCOR1)	REDI	202
		CC = (RCOR2*YCOR1 -RCOR1*YCOR2)/(YCOR2 -YCOR1)	REDI	203
		DIST = DIS(AA,CC,YPP,RPP)	REDI	204
205		IF (DIST) 3000,1335,1320	REDI	205
	1320	AA = (RCOR1 -RCOR3)/(YCOR3 -YCOR1)	REDI	206
		CC = (RCOR3*YCOR1 -RCOR1*YCOR3)/(YCOR3 -YCOR1)	REDI	207
		DIST = DIS(AA,CC,YPP,RPP)	REDI	208
		IF (DIST) 1325,1335,3000	REDI	209
210	1325	AA = (PCOR4 -RCOR1)/(YCOR1 -YCOR4)	REDI	210
		CC = (PCOR4*YCOR1 -RCOR1*YCOR4)/(YCOR1 -YCOR4)	REDI	211
		DIST = DIS(AA,CC,YPP,RPP)	REDI	212
		IF (DIST) 3000,1335,1310	REDI	213
215	1338	AA = (RCOR3 -RCOR2)/(YCOR2 -YCOR3)	REDI	214
		CC = (RCOR2*YCOR3 -RCOR3*YCOR2)/(YCOR2 -YCOR3)	REDI	215
		DIST = DIS(AA,CC,YPP,RPP)	REDI	216
		IF (DIST) 1335,1335,3000	REDI	217
220	1335	IF (YPP -YB) 3000,4,4	REDI	218
	1335	CONTINUE	REDI	219
	1857	FI = ACOS(BCOS*OA /PIE*R2)	REDI	220
		GO TO 5	REDI	221
	4	FI=0.0	REDI	222
	5	FAR = FAR + FI	REDI	223
	212	YB = Y3 - DYNP	REDI	224
225	25	UNIMIN	REDI	225
		FAR=2.0*FAR	REDI	226
		IF (PI*TA -FO, 0) GO TO 20001	REDI	227
		IF (LINEF .CL. 981 CALL RITE(LINEF))	REDI	228

239	WRITE(1,10000) MODE(1),FAB	PEO1	230
	LINEF=LINEF+1	PEO1	231
	20001 LLELL+1	PEO1	232
	FEIN,ALLD=FA3*1.DES	PEO1	233
	7 CONTINUE	PEO1	234
235	30 CONTINUE	PEO1	235
	RETURN	PEO1	236
	END	PEO1	237

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FUNCTION DISUAL,CCI,VPPI,PPPI

OFU-SOPT/ARI*2,1,0)

COA-AA1/OEO

SIA=1,0/OEO

PP = - 1,0 CCI/OEO

DIS = VPPI*COA +PPPI*SIA -PP

RETURN

END

DIS 2
DIS 3
DIS 4
DIS 5
DIS 6
DIS 7
DIS 8
DIS 9

SUBROUTINE RIECTIME
MPTG(5,1)
FORMAT(1,25,"SYSTEM EXTERNAL VIEW FACTORS-")
LINE=4
RETURN
END

RIE
RIE
RIE
RIE
RIE
RIE
RIE

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7

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		SUBROUTINE VECANG(X1,X2,Y1,X2,Y2,VECT,THETA,NTOT1)		VECANG	2
		DIMENSION XL(1),Y1(1),Y2(1),Y2(1),VECT(1),THETA(1)		VECANG	3
		DO 1 I=1,NTOT1		VECANG	4
		IF(X2(1).NE.X1(1)) GO TO 2		VECANG	5
5		IF(VECT(1).GT.0.0) GO TO 3		VECANG	6
		THETA(1)=90.0		VECANG	7
		GO TO 1		VECANG	8
	3	THETA(1)=0.0		VECANG	9
		GO TO 1		VECANG	10
10	2	IF(Y2(1).NE.Y1(1)) GO TO 4		VECANG	11
		IF(VECT(1).GT.0.0) GO TO 5		VECANG	12
		THETA(1)=180.0		VECANG	13
		GO TO 1		VECANG	14
15	5	THETA(1)=3.0		VECANG	15
		GO TO 1		VECANG	16
	4	THETA(1)=((ABS(Y2(1))-Y1(1))/ABS(X2(1))-X1(1)))*.14159		VECANG	17
		IF(Y1(1).GT.Y2(1)) GO TO 6		VECANG	18
		IF(VECT(1).GT.0.0) GO TO 7		VECANG	19
		THETA(1)=180.0+THET		VECANG	20
20		GO TO 1		VECANG	21
	7	THETA(1)=THET		VECANG	22
		GO TO 1		VECANG	23
	6	IF(VECT(1).GT.0.0) GO TO 8		VECANG	24
		THETA(1)=180.0-THET		VECANG	25
25		GO TO 1		VECANG	26
	8	THETA(1)=THET		VECANG	27
	1	CONTINUE		VECANG	28
		RETURN		VECANG	29
		END		VECANG	30

	OVERLAY/PH,16,21	TAIL2	2
	PROGRAM TAIL2	TAIL2	7
	COMMON/PLM/08(500)	TAIL2	4
	COMMON/ALL/ M,N,N,N,N,N,ISURF(50),MODE(5),JSURF(5,2),X(15),NTOT1,	TAIL2	5
5	NO,INP(10), AREA(80)	TAIL2	6
	COMMON /TAIL/ NF,YFAC(30),WF(30),RFAC(30),RFB(30),TPL,FW(50)	TAIL2	7
	COMMON /WZ/ TW(80)	TAIL2	8
	COMMON/CG/ MMS,MMS,S,MMS,4(6)	TAIL2	9
	COMMON /PRINT/ PRINT1, PRINT2, PRINT3, PRINT4, PRINT5,	TAIL2	10
	PRINT6, PRINT7, PRINT8, PRINT9, PRINT10,	TAIL2	11
10	* DIMENSION FE(3,53),	TAIL2	12
	Y2(55), VEC(155), YF(16,20), PF(10,20)	TAIL2	13
	COMMON/T/ THA(20),NST,NAS,NAL,NPLOT	TAIL2	14
	INTERF PRINT1,PRINT2,PRINT3,PRINT4,PRINT5,PRINT6,PRINT7,PRINT8,	TAIL2	15
15	PRINT9,PRINT10	TAIL2	16
	EQUIDISTANCE (0,1),FE(1), (0,1),FE(1), (0,3),FE(1), (1,1),	TAIL2	17
	(1,2),FE(1), (1,1), (0,3),FE(1), (2,1), (0,6),FE(1), (0,8),FE(2),	TAIL2	18
	VECT(1),	TAIL2	19
	(0,1),FE(1), (1,1), (0,3),FE(1), (2,1), (0,6),FE(1), (0,8),FE(2),	TAIL2	20
20	CALL F(0,1),F(1),NAS,THA,AREA,F,FE,EM,TW,0,NAL,NPLOT1	TAIL2	21
	END	TAIL2	21

	SUBROUTINE REDI(M,N,ANG,TM,AR,F,FE,RH,T,OG,NML,NPLOT)	REDI	2
	DIMENSION FE(30,50),OG(1),F(50,50),AR(1),RH(1),LL(50),ERI(20),	REDI	3
	1ML(50),P(4),U(4),AM(5,50),F(50,50)	REDI	4
5	DIMENSION TH(30),T(80)	REDI	5
	COMMON /PRINT/ PRINT1, PRINT2, PRINT3, PRINT4, PRINT5,	REDI	6
	PRINT6, PRINT7, PRINT8, PRINT9, PRINT0,	REDI	7
	INTEGER PRINT1, PRINT2, PRINT3, PRINT4, PRINT5, PRINT6, PRINT7, PRINT8,	REDI	8
	PRINT9, PRINT0	REDI	9
10	1, PRINT9, PRINT0	REDI	10
	COMMON /OUT/ AREAR(20),TMAK(20),ANG(20),ITOT	REDI	11
	COMMON /EE/ BAND1,BAND2, 504(20)	REDI	12
	DATA ERI/20*IM /	REDI	13
	DATA P/ .1719274, .1260726, .1260726, .1719274,	REDI	14
	DATA U/- .4315642, -.1699305, .1699305, .4315642	REDI	15
	DATA S0/0.02/	REDI	16
15	DO 210 I=1,N	REDI	17
231	RM(I)=1.0-CH(I)	REDI	18
	CI=1.187*(1.0**0)/3.41276	REDI	19
	C2=25.0	REDI	20
	RE=630.	REDI	21
30	RS=DEFEV/14.	REDI	22
	CF=1./(10.**5)	REDI	23
	NS=N	REDI	24
	READ(5,49) BAND1,BAND2	REDI	25
25	FO, MAT(2,10,5)	REDI	26
281	DO 2 I=2,NS	REDI	27
	IP=I-1	REDI	28
	DO 1 J=1,IP	REDI	29
30	1 F(I,J)=AR(I)*F(J,IP)/AR(I)	REDI	30
	2 CONTINUE	REDI	31
	DO 3 I=1,NS	REDI	32
	IF(I-J) 4,5,4	REDI	33
	4 DJJ=J.	REDI	34
	GO TO 3	REDI	35
35	5 DJJ=I.	REDI	36
	3 AM(I,J)=OIJ-RH(I)*F(I,J)	REDI	37
	CALL MINV (AM,N,50,LLL,PLL)	REDI	38
	DO 4 J=1,NS	REDI	39
40	ONL=1.0-RH(J)	REDI	40
	DO 6 I=1,NS	REDI	41
6	AM(I,J)=AM(I,J)*ONEN	REDI	42
	DO 10 I=1,NANG	REDI	43
	DO 95 J=1,NS	REDI	44
	ERI(J)=0.	REDI	45
45	DO 9 K=1,NS	REDI	46
9	ERI(J)=ERI(J)+FE(I,K)*AM(I,K,J)	REDI	47
95	ERI(J)=CF* ERI(J)	REDI	48
18	CONTINUE	REDI	49
	DO 120 I=1,NANG	REDI	50
50	GBAX=0.0	REDI	51
	ML=1.0	REDI	52
	DO 21 M=1,NML	REDI	53
	GBL=J.0	REDI	54
	DO 14 J=1,NS	REDI	55
55	VI=0.0	REDI	56
	DO 94 ID=1,4	REDI	57
	X(15)=C(100)+ML	REDI	58

Line	Code	Statement	MINV
5	10	10 SUBROUTINE MINV(A,N,M,L,M)	2
	11	11 DIMENSION A(I),L(I),M(I)	3
	12	12 N=N	4
	13	13 DO 15 K=1,N	5
	14	14 M=NK+M	6
	15	15 L(K)=K	7
	16	16 M(K)=K	8
	17	17 K=NK+K	9
	18	18 SIGA=A(I,K)	10
	19	19 DO 20 J=1,N	11
	20	20 I=K+J	12
	21	21 DO 21 I=K,N	13
	22	22 I=I+1	14
	23	23 IF(I)S(I,G)=ABS(A(I,J))	15
	24	24 SIGA=A(I,J)	16
	25	25 L(K)=I	17
	26	26 M(K)=J	18
	27	27 CONTINUE	19
	28	28 J=L(K)	20
	29	29 IF(J-K) 35,35,25	21
	30	30 KI=K-M	22
	31	31 DO 31 I=1,K	23
	32	32 KI=KI+M	24
	33	33 HOLD=A(K,I)	25
	34	34 JI=KI-K+J	26
	35	35 A(K,I)=A(J,I)	27
	36	36 A(J,I)=HOLD	28
	37	37 I=K(I)	29
	38	38 IF(I-K) 45,45,38	30
	39	39 JP=K+I-1	31
	40	40 DO 40 J=1,N	32
	41	41 JK=N+J	33
	42	42 JI=JP+J	34
	43	43 HOLD=A(I,K)	35
	44	44 A(J,K)=A(J,I)	36
	45	45 A(J,I)=HOLD	37
	46	46 IF(I-GAI) 45,45,46	38
	47	47 DO 55 I=1,N	39
	48	48 IF(I-K) 50,55,50	40
	49	49 IK=N+I	41
	50	50 A(I,K)=A(I,K)/(I-GAI)	42
	51	51 CONTINUE	43
	52	52 DO 65 I=1,N	44
	53	53 IK=N+I	45
	54	54 IJ=I-NM	46
	55	55 DO 65 J=1,N	47
	56	56 IJ=IJ+M	48
	57	57 IF(I-K) 60,65,68	49
	58	58 IF(J-K) 62,65,62	50
	59	59 A(I,J)=A(I,K)*A(K,J)*A(I,J)	51
	60	60 CONTINUE	52
	61	61 K=N+M	53
	62	62 DO 70 J=1,N	54
	63	63 KI=K+M	55
	64	64 DO 70 J=1,N	56
	65	65 IF(J-K) 70,75,70	57
	66	66 A(I,K)=A(I,K)/SIGA	58

```

75 CONTINUE
  A ( K K ) = 1. / 81 GA
60 CONTINUE
  K=N
180 K=(K-1)
  IF(K) 150,150,185
105 I=L(K)
  IF(I-K) 120,128,188
188 J=NM*(K-1)
  J=NM*(I-1)
  DO 110 J=1,M
    JK=J+J
    HOLD=J(JK)
    JI=J+J
    A(JK)=-A(JI)
110 A(JI)=HOLD
120 J=N(K)
75 IF(J-K) 100,108,125
125 KI=K+NM
  DO 130 I=1,M
    KI=KI+NM
    HOLD=A(KI)
    JI=KI-K+J
    A(KI)=-A(JI)
130 A(JI)=HOLD
  GO TO 100
150 RETURN
85 END

```



```

SUBROUTINE SUMAT1 (TH,Q8,NML,I,IPT,IPLT)
  DIMENSION OB(1)
  COMMON /OUT/ AREA(20),TMAX(20),ANG(20),ITOT
  COMMON /EE/ BAND1,BAND2, SUM(20)
  NMS=1000./BAND2
  NME=1000./BAND1
  DEL=4NE-MNS
  NP=DEL/50.*1
  SS=DEL/NP
  NME-MNS=0.5*SS
  AREA(1)=0.0
  DO 200 L=1,NP
    WN=WN+SS
    200 AREA(L)=AREA(L)+PLANKC(TMAX(L),WN)*SS
    ANG(L)=TH
    IS=(BAND1-1.0)/0.02+1.00000035
    IE=(BAND2-1.0)/0.02+0.00000035
    WL=0.5*(IS+IE)
    OIFF=WL-BAND1
    VAL=0.5*(EO.*OIFF)
    SUM(1) = VAL*OB(1S)
    L=1S+1
    DO 103 LL=L,IE
      103 SUM(LL) = SUM(LL)+OB(LL)
      L=1E+1
      NML=0.9*(L+0.02)
      OIFF=NL-BAND2
      VAL=0.5*(EO.*OIFF)
      SUM(1) = VAL*OB(1S)
      L=1S+1
      SUM(LL) = SUM(LL)+OB(LL)
      AREA(1)=SUM(1)/AREA(1)
      IF(IPT.EQ.0) GO TO 100
      WRITE(6,15) BAND1, BAND2, SUM(1)
      15 FORMAT(1H0,9,*,BANDWIDTH SUMMATION*,5X,*,BANDWIDTH*F6.2,2H -,F6.2,
      15,*,RADIATION*,F8.3,*,W/ST.*)
      103 IF(IPLT.EQ.0 .OR. TH.GT.89.5) RETURN
      WL=0.9*(IS+0.02)
      NP=1E-1S+2
      DO 60 L=1,NP
        LL=L+999
        OB(LL)=WL
        LL=LL+NP
        L=L+1S
        OB(LL)=OB(1S)
        WN=10000./WL
        LL=LL+NP
        SS=10000./ (WL-0.01)-10000./ (WL+0.01)
        OB(LL)=PLANKC(TMAX(L),WN)+AREA(1)*SS
        60 WL=WL+0.02
      CALL PLOT1 (TH,Q8(1000),NP,3,40.0)
      RETURN
    END
  END

```